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A Multiscale Approach to Predict Classical Losses in Soft Magnetic Composites

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This paper presents the application of a finite element multiscale method, based on the homogenization technique, to the prediction of classical losses in soft magnetic composite materials. The experimental results, obtained for a wide range of frequencies and for various toroidal samples with different cross sections, are explained by using the considered model. It has been found that the classical losses are influenced by the dimensions of the sample, as well as by the conductivity and the length of the random contacts between the grains.

Index Terms — Composite materials, numerical analysis, multiscale problem, classical losses.

I. INTRODUCTION

SOFT MAGNETIC Composites (SMC) appear as very promising in many industrial applications, as for example in high speed electrical machines [1]. Indeed, their granular structure leads to a significant reduction of the classical loss contribution, which, however, can become important at the frequency increase [2]. Moreover, unlike conventional laminated materials, SMC exhibit isotropic magnetic properties, which can make them suitable in machines with 3D flux paths, such as axial flux machines [3]. They also possess isotropic thermal properties [4], which is an important feature for loss dissipation.

An accurate loss prediction is essential for a reliable optimization of electrical machines using such materials. Since the classical loss gives the most important contribution in high frequency applications, this paper focuses on a modeling approach for the computation of eddy currents in SMC materials.

SMC are composed of grains made of a magnetic material (often pure iron). The grains are resin-insulated from each other and then compressed under high pressure. During the compaction, random contacts can appear between grains, as pointed out in [5]. These random contacts are responsible for a SMC bulk conductivity, which is much lower than the one of the grains, but not negligible, giving rise to eddy current circulation at macroscopic scale (sample size).

A model for computing the SMC equivalent permeability taking into account the grain contacts has been proposed in [6]. Here, a micrograph image is exported to an electromagnetic finite element software and used to deduce an equivalent permeability, which is found in good agreement with the measurements. Such an approach could be extended also to eddy current computations, but it is

limited to very small samples because of the huge number of mesh elements required for a reliable discretization. Other authors have analyzed so small samples that the effects of current paths flowing from grain to grain at the sample scale are negligible [7]. Only the microscopic eddy currents flowing at the grain scale have been taken into account, considering rectangular grains. However, this simplifying assumption is usually not verified in electrical machine applications, where non negligible intergrain currents are present. Therefore, in [8] the classical loss contribution has been evaluated by introducing a loss decomposition into two terms: the first one is due to the eddy currents at the grain scale, the second one is related to the eddy currents at the macroscopic scale and linked to the bulk resistivity. However, this loss summation is not straightforward from a mathematical point of view.

This paper proposes the use of a method based on a multi-scale homogenization technique [9], successfully applied to different non-homogeneous materials, such as ferrites [10]. The main difficulty encountered here is to model the random contacts between grains using the homogenization method. In the first part of the paper, the experimental evidence of the macroscopic eddy currents is shown. Then, the idealized model of the contacts between grains, to be used in the homogenization process, is introduced. The last part of the paper presents the comparison between the experimental results and the model.

II. EXPERIMENTS

The presence of macroscopic eddy currents flowing from grain to grain at the sample scale is put in evidence in this section. This evidence is based on the remark that only the macroscopic eddy current term, unlike the loss contributions at the grain scale (hysteresis, excess, and local eddy currents), can be responsible for a dependence of the specific loss on the sample size and shape. The analysis presented in

[7] shows that a toroid with a square cross section $S = 5 \times 5$ mm² seems to be small enough to neglect macroscopic eddy currents. Indeed, when decreasing the section to 2.5×2.5 mm², a negligible change in the specific loss has been observed. Here, the analysis is centered on toroids with cross sections greater than 5×5 mm², where not negligible macroscopic eddy currents are expected.

A. Description of the experimental set-up

The considered SMC are produced by the Swedish company Höganäs in bulk cylindrical shape (diameter: 80 mm, height: 20 mm), under the reference "Prototyping" [11]. Since these blocks can be quite easily cut, they are well suitable for making toroids of different cross sections, as the ones investigated in this paper and represented in Fig. 1. The first section (toroid A: $S_A = 5 \times 5$ mm²) is considered as the reference case [7], having assumed that the eddy currents are confined at the grain scale. Two larger samples are also considered: toroid B ($S_B = 10 \times 10$ mm²) and toroid C ($S_C = 10 \times 20$ mm²). The external diameter D_{ext} of the toroids is always set at its maximal value (i.e. the external diameter of the blocks, equal to 80 mm), in order to ensure a uniform flux density distribution throughout the entire cross section.

It is also important to give some details about the cutting procedure. Indeed, some authors [12] have pointed out the fact that a mechanical abrasion could create conductive paths on the material surface. This could introduce criticalities in our experiments: if the four faces of the toroid are made conductive by the cutting abrasion, a fictitious closed electrical turn would be created on the toroid surface. This is another reason why the toroids have an external diameter equal to the external diameter of the blocs $D_{ext} = 80$ mm. This choice ensures that at least the external face has not undergone any abrasion, therefore making impossible the formation of a closed conductive turn around the toroids.

Fig. 1. Scheme of the toroidal sample and of the different cross sections considered in the analysis.

The experimental loss measurement is carried out as follows. The toroid is wound by two windings. The primary winding is supplied under AC conditions with a linear power amplifier. The current flowing in this primary winding is measured using a resistive sensor. This allows to deduce the applied magnetic field, which is, according to Ampere's law, proportional to the current. The mean flux density over the toroid cross section is measured by the integration of the voltage given by a secondary winding. Then, the B - H curve is deduced, and the area of the cycle gives the total specific loss per cycle W_{tot} . A feedback loop permits to get a perfect sinusoidal polarization in the toroid, assumed to be equal to the magnetic flux density (frequency f , peak value J_p).

B. Loss results in the different toroids

The total specific energy loss per cycle $W_{tot}(J_p, f)$ measured in the considered toroids are given in Fig. 2. The dependence of the specific loss on the toroid cross section due to macroscopic eddy current patterns is well evident.

Fig. 2. Total measured loss $W_{tot}(J_p, f)$ versus frequency f for $J_p = 0.5$ T (a) and $J_p = 1$ T (b).

C. Assumption of no skin effect for the loss separation

The loss separation has been carried out following the approach described in [7]. Starting from the assumption of only local eddy currents in toroid A, a model of eddy currents at the scale of the single grain has been developed. The hysteresis and excess losses, which are local per definition, have been extracted. Then, we assume that, under the same excitation conditions (frequency f and polarization peak value J_p), the excess and hysteresis losses in toroids B and C are equal to the ones in toroid A, in spite of the presence of macroscopic eddy currents which change the classical loss. Therefore, the classical loss contribution in toroids B and C is computed by subtracting hysteresis and excess loss obtained in toroid A from the total measured loss.

This procedure is valid if we assume that the macroscopic eddy current patterns do not modify the local magnetic flux density in the toroid. In other terms, the skin effect at the sample scale must be negligible. To verify this assumption experimentally the local magnetic flux density in the cross section of toroid C has been measured, by drilling two holes in the toroid, as represented in Fig. 3. An internal coil between the two holes allows us the measurement of the internal magnetic flux density $B_{int}(t)$, while an external winding enables the detection of the external field $B_{ext}(t)$. The skin effect due to macroscopic eddy current patterns is negligible if these internal and external magnetic flux density components do not differ from the mean field $B(t)$ measured at the secondary winding.

Fig. 3. Scheme of the measurement procedure for the internal and external magnetic flux density components in toroid C.

177 The ratios of the peak values of the local and mean
 178 magnetic flux densities and the phase shift between their first
 179 harmonics are plotted versus frequency for $J_p=1$ T in Fig.
 180 4(a) and in Fig. 4(b), respectively. The amplitude of the ratio
 181 is close to unity, while the phase shift does not exceed 5° , so
 182 that the assumption of negligible skin effect is well justified.

183 Fig. 4. a) Ratios of the peak values of the local magnetic flux densities,
 184 $B_{ext}(t)$ and $B_{int}(t)$, and the mean magnetic flux density $B(t)$. b) Phase shifts
 185 between the first harmonics of the local and mean magnetic flux densities.
 186

187 III. MODELING APPROACH

188 The starting point of the modeling approach is the
 189 application of the mathematical homogenization technique to
 190 infer the physical and geometrical properties of the
 191 equivalent contacts between the grains. For such a purpose,
 192 the 3D random distribution of grains, with possible contacts,
 193 is replaced with a 2D periodic structure represented by the
 194 repetition of an idealized elementary cell. A known
 195 sinusoidal magnetic flux is imposed along the direction
 196 normal to this 2D domain and the electromagnetic field
 197 problem is formulated in terms of an electric vector potential
 198 with homogeneous Dirichlet boundary conditions [13]. The
 199 governing equation is written in the frequency domain
 200 expressing the field quantities as phasors. All the field
 201 problems involved in the adopted approach are solved
 202 through the Finite Element Method.

203 Fig. 5: Scheme of the elementary cell with idealized grain contacts.
 204

205 For the specific application, the elementary square cell ($s =$
 206 $115 \mu\text{m}$) shown in Fig. 5 is adopted, where four regions
 207 connecting the surrounding cells are introduced to simulate
 208 the presence of grain contacts. The idealized square grain is
 209 assumed to have the average dimensions of the actual grains,
 210 observed in the micrograph images.

211 Both for grain and contacts the relative magnetic
 212 permeability is assumed to be equal to 450, as deduced by a

213 3D analysis. However, the precise value of this parameter
 214 has a limited impact, due to the absence of skin effect shown
 215 in the previous section. The grain is made of pure iron with
 216 an electrical conductivity of 10 MS/m . The non-magnetic
 217 insulating layer has a thickness $l_i = 0.74 \mu\text{m}$ and a high
 218 resistivity ($\rho_i = 10 \text{ M}\Omega\text{m}$). The length and the electrical
 219 conductivity of the contact are chosen, by a trial and error
 220 procedure, to fit the classical loss contribution. Magnetic
 221 fluxes Φ corresponding to uniform magnetic flux densities of
 222 0.5 T and 1 T are imposed along the direction normal to the
 223 sample cross-section.

224 Since the aim is an accurate evaluation of the classical
 225 losses at both grain and sample scales, a multiscale model
 226 able to reconstruct the macroscopic and local distribution of
 227 eddy currents has to be adopted. The mathematical
 228 homogenization approach, based on the multiple scale
 229 expansion theory [13], is suitable for this application. Indeed,
 230 following this technique, the field equation is handled by
 231 searching a solution expressed in an asymptotic form, with a
 232 zero-order term and higher-order correctors. The first term
 233 describes the homogenized solution computed in a
 234 homogenous medium with “average” properties; the other
 235 terms introduce corrections to reproduce the local behavior
 236 of the heterogeneous material. A detailed description of the
 237 mathematical formulation can be found in [9]. As an
 238 example, the effect of the superimposition of the local terms
 239 to the global one is shown in the eddy current distribution
 240 presented in Fig. 6.

241
 242 Fig.6. Distribution of current field lines in the cross section of a SMC toroid,
 243 computed using the homogenization method with second order correctors.

244 IV. RESULT DISCUSSION

245 The first problem for the model development is the
 246 characterization of the contact, starting from the
 247 experimental data. Having fixed the insulating layer
 248 thickness, two parameters have to be identified: the contact
 249 length l_c and its conductivity σ_c . To investigate the influence
 250 of these parameters on the classical loss component, l_c is
 251 varied from $\sim 0.025 \mu\text{m}$ up to $115 \mu\text{m}$ (full contact) and σ_c is
 252 varied in the range between $\sim 20 \text{ S/m}$ and $\sim 100000 \text{ S/m}$.

253 A first analysis, performed keeping constant one of the
 254 two parameters, shows that the increase of the other one
 255 always leads to an increase in the macroscopic eddy currents
 256 and in the classical loss too. However, when the two

parameters are simultaneously modified maintaining their product constant, the classical loss remains practically unchanged in the whole range of contact length. This implies that a single parameter (the product $\sigma_c l_c$) can fully identify the properties of the contact.

The identification process is performed considering the total loss measured in toroid B at 7000 Hz from which the hysteresis and excess losses obtained in toroid A are subtracted to evaluate the classical loss contribution. A value of 2850 S has been determined for the product $\sigma_c l_c$ and adopted in all the simulations carried out in the frequency range from 1 kHz to 10 kHz, where the SMC components usually operate and the influence of eddy currents is better highlighted.

The comparison between the experimental and computed classical losses in toroids B and C are presented in Fig. 7 for two flux values, corresponding respectively to uniform flux densities of 0.5 T and 1.0 T.

Fig. 7. Classical losses W_{clas} as a function of frequency f , for a magnetic flux density of 0.5 T (a) and 1 T (b)

For the both toroids the model provides results in very good agreement with the experiments. The relative error is less than 3% for a magnetic flux density of 0.5 T and it is approximately 6% for 1 T. The errors can be attributed both to the measurement uncertainty and to the approximations intrinsic in a numerical model. The greater errors in the 1 T case can be explained by the higher temperature increase in the sample, consequent to the loss enhancement, which can modify the material properties. For both sections, the influence of macroscopic eddy currents cannot be disregarded and it is responsible of the dependence of the classical losses on the sample size. For toroid A, a good agreement with the numerical model is also found when simulating insulated grains (i.e. the circulation of macroscopic grains is neglected).

V. CONCLUSION

The paper proposes a computational method, based on a multi-scale homogenization technique, for the evaluation of the classical loss component in composite materials. The model takes into account the presence of macroscopic eddy currents, which can flow between grains due to random contacts. The comparison between the experimental and numerical results shows a good agreement for toroids with large cross sections. It has been observed that at the increase of the toroid size the current path, which is mainly local for small cross sections, tends towards a more global distribution.

The proposed model is able to evaluate the increase of the classical loss due to the presence of currents at sample scale for any kind of SMC materials, provided that some measurements are available for the material identification.

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