



HAL
open science

Zirconia-spinel composites. Part II: mechanical properties

Olivier Quénard, Christophe Laurent, Alain Peigney, Abel Rousset

► **To cite this version:**

Olivier Quénard, Christophe Laurent, Alain Peigney, Abel Rousset. Zirconia-spinel composites. Part II: mechanical properties. *Materials Research Bulletin*, 2000, vol. 35, pp. 1979-1987. 10.1016/S0025-5408(00)00409-8 . hal-00949036

HAL Id: hal-00949036

<https://hal.science/hal-00949036>

Submitted on 19 Feb 2014

HAL is a multi-disciplinary open access archive for the deposit and dissemination of scientific research documents, whether they are published or not. The documents may come from teaching and research institutions in France or abroad, or from public or private research centers.

L'archive ouverte pluridisciplinaire **HAL**, est destinée au dépôt et à la diffusion de documents scientifiques de niveau recherche, publiés ou non, émanant des établissements d'enseignement et de recherche français ou étrangers, des laboratoires publics ou privés.



Open Archive TOULOUSE Archive Ouverte (OATAO)

OATAO is an open access repository that collects the work of Toulouse researchers and makes it freely available over the web where possible.

This is an author-deposited version published in : <http://oatao.univ-toulouse.fr/>
Eprints ID : 10981

To link to this article : doi:10.1016/S0025-5408(00)00409-8
URL : [http://dx.doi.org/10.1016/S0025-5408\(00\)00409-8](http://dx.doi.org/10.1016/S0025-5408(00)00409-8)

To cite this version : Quénard, Olivier and Laurent, Christophe and Peigney, Alain and Rousset, Abel Zirconia–spinel composites. Part II: mechanical properties. (2000) Materials Research Bulletin, vol. 35 (n° 12). pp. 1979-1987. ISSN 0025-5408

Any correspondence concerning this service should be sent to the repository administrator: staff-oatao@listes-diff.inp-toulouse.fr

Zirconia–spinel composites. Part II: mechanical properties

O. Quénard, Ch. Laurent*, A. Peigney, A. Rousset

*CIRIMAT, UMR CNRS 5085/LCMIE, Centre Interuniversitaire de Recherche et d'Ingénierie des Matériaux,
Université Paul-Sabatier, 31062 Toulouse Cedex 4, France*

Abstract

The mechanical properties (fracture strength, fracture toughness, and Vickers microhardness) of MgAl_2O_4 and x wt% ZrO_2 - MgAl_2O_4 ($1 \leq x \leq 30$) hot-pressed materials were measured at room temperature. Two kinds of materials, which were prepared from either ball-milled or attrited powders, were investigated. Compared with an unreinforced spinel, a twofold (or greater) increase in both strengthening and toughening was measured for materials with the highest zirconia content (30 wt%). It was found that dispersing only 1 wt% of zirconia in the spinel produced a marked increase in the Vickers microhardness. The total zirconia content appears to be a key parameter. © 2001 Elsevier Science Ltd. All rights reserved.

Keywords: A. Oxides; A. Composites; C. Electron microscopy; D. Microstructure, D. Mechanical properties

1. Introduction

The field of applications of the spinel MgAl_2O_4 is limited by its poor mechanical properties at room temperature [1–8]. The dispersion of micrometric ZrO_2 particles as a discrete second phase is a well-known method for the enhancement of the mechanical properties of ceramics [9]. Several reinforcement mechanisms have been identified, including microcracking, owing to the transformation upon cooling from the sintering temperature of tetragonal ZrO_2 (t- ZrO_2) particles into monoclinic ZrO_2 (m- ZrO_2) particles (denoted hereafter as the t \rightarrow m transformation), stress-induced t \rightarrow m transformation, compressive

* Corresponding author. Tel.: +33-561-55-61-22; Fax: +33-561-55-61-63.

E-mail address: laurent@iris.ups-tlse.fr (Ch. Laurent).

surface stresses, crack branching, and crack deflection. However, most studies have dealt with $\text{ZrO}_2\text{-Al}_2\text{O}_3$ composites [9], and only a few with $\text{ZrO}_2\text{-MgAl}_2\text{O}_4$ composites [10–12].

Claussen and Rühle [10] reported that the fracture strength of MgAl_2O_4 increases from 200 to 500 MPa upon the dispersion of 25 wt% ZrO_2 , with 60% of the total ZrO_2 content being in the metastable tetragonal form and 40% in the monoclinic form. Fujita et al. [11] prepared dense specimens (relative density $\geq 95\%$) by conventional sintering or hot pressing of powders of spinel and a 24 wt% $\text{ZrO}_2\text{-spinel}$ composite synthesized by the powder mixing and alkoxides routes. In these materials, the spinel is alumina rich ($\text{MgO}:\text{Al}_2\text{O}_3$ ratio equal to 3:4). The matrix grain size is close to 2 μm in both the sintered (ex-alkoxide) spinel and $\text{ZrO}_2\text{-spinel}$ materials, and the average size of the ZrO_2 particles is 0.5 μm . The fracture strength and the fracture toughness of the composite (400 MPa and 6.3 $\text{MPa}\cdot\text{m}^{1/2}$) are about twice those measured for the unreinforced spinel (230 MPa and 3.1 $\text{MPa}\cdot\text{m}^{1/2}$). For the hot-pressed (expowder mixing) materials, the matrix grain size is close to 4–5 μm in the spinel and much smaller (1.2 μm) in the composite. The fracture strength increases from 200 MPa for the spinel to 340 MPa for the composite. These authors [11] proposed that the improvement of the mechanical properties was due to the stress-induced $t \rightarrow m$ transformation, higher densification by ZrO_2 addition, and inhibition of the matrix grain growth. Hyun and Song [12] prepared a 20 wt% $\text{ZrO}_2\text{-spinel}$ sintered composite (relative density = 97.8%) consisting of a spinel matrix (grain size = 1.5–2 μm) containing 1–2 μm cubic ZrO_2 (c- ZrO_2) agglomerates made up of much smaller primary grains. The fracture strength and the fracture toughness of the composite were equal to 390 MPa and 1.98 $\text{MPa}\cdot\text{m}^{1/2}$, respectively. The absence of toughening with respect to a spinel produced by the same process was attributed to the presence of c- ZrO_2 rather than t- ZrO_2 particles.

The present authors have reported in a companion paper [13] the synthesis of MgAl_2O_4 and x wt% $\text{ZrO}_2\text{-MgAl}_2\text{O}_4$ ($1 \leq x \leq 30$) powders by the urea combustion route, and the subsequent preparation of dense materials by hot pressing. The aim of the present work is to investigate the mechanical properties (fracture strength, fracture toughness, and Vickers microhardness) of these materials.

2. Experimental

MgAl_2O_4 and x wt% $\text{ZrO}_2\text{-MgAl}_2\text{O}_4$ ($x = 1, 5, 10, 20,$ and 30) composite powders were prepared by the urea combustion route [13]. For each composition, the so-obtained powders were separated into two parts, which were ground either by ball milling or by attrition. These powders were uniaxially hot pressed in graphite dies at 1500°C in a primary vacuum. The hot-pressed specimens (20 mm in diameter and 2 mm thick) were ground to a finish finer than 6 μm with diamond suspensions, and a final polish was made using “colloidal” silica (0.05 μm). Relative densities were calculated from the mass and dimensions of the hot-pressed composites. For the sake of brevity, the materials issued from the hot pressing of ball-milled and attrited powders will be denoted BM0, BM1, ..., BM30 and A0, A1, ..., A30, respectively, the number reflecting the ZrO_2 weight content. The specimens were observed by scanning electron microscopy (SEM). The Vickers microhardness was measured by indentation during 20 s using a 3 N load. The values given for H_v are the average of 10

Table 1

Some characteristics of the ZrO₂-MgAl₂O₄ hot-pressed specimens

Specimen ^a	d _r	t-ZrO ₂	∅ _s	∅ _z	σ _f	K _{IC}	H _v
BM0	96.2	—	1.4	—	259	3.3	1444
BM1	96.5	100	0.8	n-m ^b	300	3.0	1561
BM5	95.7	84	0.8	0.19	329	3.2	1584
BM10	98.3	89	0.8	0.25	294	3.0	1587
BM20	96.9	87	0.8	0.36	355	4.8	1559
BM30	96.7	48	0.8	0.44	578	6.6	1575
A0	95.5	—	0.3	—	243	2.3	1494
A1	95.7	100	0.3	n-m	234	2.8	1632
A5	96.6	88	0.3	0.35	376	3.1	1617
A10	95.8	89	n-m	0.37	445	3.4	1560
A20	96.4	60	0.2	0.42	489	4.0	1590
A30	94.8	19	n-m	0.44	506	6.6	1505

d_r: relative density; t-ZrO₂: proportion (%) of tetragonal zirconia with respect to the total amount of ZrO₂; ∅_s and ∅_z: average size (μm) of the spinel grains and of the ZrO₂ particles, respectively; σ_f: fracture strength (MPa); K_{IC}: fracture toughness (MPa·m^{1/2}); H_v: Vickers microhardness.

^a BM and A denote specimens issued from hot-pressing of ball-milled and attrited powders, respectively, and the number indicates the ZrO₂ content in wt%.

^b n-m: not measured.

measurements. The transverse fracture strength (σ_f) was determined by the three-point bending test on parallelepipedic specimens (1.6 × 1.6 × 18 mm³) machined with a diamond saw. The fracture toughness (K_{IC}) was measured by the SENB method on similar specimens notched using a diamond wire 0.1 mm in diameter. The calibration factor proposed by Brown and Srawley [14] was used to calculate the SENB toughness from the experimental results. Crosshead speed was fixed at 0.1 mm/min. The values given for σ_f and K_{IC} are the average of measurements on 10 and 6 specimens, respectively.

3. Results and discussion

It has been shown [13] that the matrix of the BM specimens is the stoichiometric spinel, whereas that of the A materials is an alumina-rich spinel, the formula of which could be Mg_{0.91}□_{0.03}Al_{2.06}O₄. Because it is expected that the effects of the nonstoichiometry are negligible at room temperature [7,15], the oxide in the A materials will be considered as being MgAl₂O₄ in the following. The microstructural characteristics of the specimens [13] are listed in Table 1. Both t-ZrO₂ and m-ZrO₂ are present in the composites, except in BM1 and A1, in which only t-ZrO₂ was detected. The proportion of t-ZrO₂ slightly decreases to a value close to 85% for BM5, BM10, and BM20, and sharply decreases upon further addition of ZrO₂ (48% for BM30). A similar evolution is observed for the A composites, but it is noteworthy that the sharp decrease of the t-ZrO₂ proportion takes place for a lower ZrO₂ content (60% for A20). SEM observations [13] have shown that the spinel grains are larger in the BM composites than in the A specimen, and that the presence of ZrO₂ particles inhibits the growth of the matrix grains upon hot pressing only in the BM composites (∅_s in Table

1). The ZrO_2 particles are homogeneously dispersed at the grain boundaries or grain junctions of the matrix. For both the BM and A specimens, their average size ($\bar{\mathcal{O}}_z$ in Table 1) increases with the total ZrO_2 content, but the values are generally higher for the A materials because the gathering of the ZrO_2 particles is easier when the matrix grains are smaller. The $t \rightarrow m$ phase transformation occurs for the larger ZrO_2 particles upon cooling from the hot-pressing temperature. Thus, the increasing proportion of $m\text{-ZrO}_2$ upon the increase in the total amount of ZrO_2 , and when comparing BM20 to A20 and BM30 to A30, reflects the growth of the ZrO_2 particles. The hypothesis that polishing could have provoked the $t \rightarrow m$ phase transformation of ZrO_2 particles located at the surface of the materials was ruled out, because it has been verified that the proportion of $m\text{-ZrO}_2$ is similar in the unground, 6 μm -ground, and silica-polished specimens.

The evolution of H_v vs. the ZrO_2 content is different for the BM and A composites (Fig. 1 and Table 1). Indeed, H_v increases from 1444 for BM0 to a value that remains quite constant (in the 1560–1590 range) regardless of the ZrO_2 content of the BM specimens (Fig. 1a). ZrO_2 particles at the matrix grain junctions could minimize the matrix grain slide and thus account for the higher Vickers microhardness, even for a very low zirconia content (1 wt%). H_v for A0 is close to that measured for BM0 (1494 vs. 1444, respectively), indicating that the matrix grain size has little influence on the microhardness of the present spinel materials. The presence of 1 wt% ZrO_2 leads to a strong increase in microhardness ($H_v = 1632$ for A1), but, contrary to what is observed for the BM specimens, H_v decreases from 1632 to 1505 upon a further increase in ZrO_2 content (Fig. 2b). Because this decrease is very important for the composite with the lesser amount of $t\text{-ZrO}_2$ (A30, which has a microhardness similar to that of A0), it is proposed that the decrease is caused by the increase in the density of microcracks, which are generated by the volume expansion of the zirconia particles that undergo the $t \rightarrow m$ transformation upon cooling from the hot-pressing temperature.

The fracture strength and fracture toughness measured for BM0 and the BM composites are reported in Table 1 and Fig. 2. For BM1, BM5, and BM10, the fracture strength (Fig. 2a) is only marginally higher than that of BM0 (259 MPa), whereas for BM20 and notably for BM30 it is significantly higher (355 MPa and 578 MPa, respectively). The evolution of the fracture toughness (Fig. 2b) is similar, with no toughening being observed for BM1, BM5, and BM10, while K_{Ic} increases to 4.8 and 6.6 $\text{MPa}\cdot\text{m}^{1/2}$ for BM20 and BM30, respectively. For the A materials (Fig. 3 and Table 1), it is noteworthy that comparable strengthening and toughening are observed at a lower ZrO_2 content than that of the BM specimens. The fracture strength increases from 243 MPa for A0 to 506 MPa for A30 (Fig. 3a), whereas K_{Ic} increases from 2.3 $\text{MPa}\cdot\text{m}^{1/2}$ for A0 to 6.6 $\text{MPa}\cdot\text{m}^{1/2}$ for A30 (Fig. 3b).

The fracture strength of BM0 (255 MPa) is similar to that of A0 (243 MPa). These values are of the order of, but slightly higher than, those reported by other workers [7,10,11]. It is noteworthy that K_{Ic} for BM0 is higher (3.3 $\text{MPa}\cdot\text{m}^{1/2}$) than most values (1.3–2.2 $\text{MPa}\cdot\text{m}^{1/2}$) reported for MgAl_2O_4 [2–5]. The difference could arise from a smaller matrix grain size in the present material (1.4 μm) than in the other materials (2–400 μm), because spinels with a grain size lower than 2 μm have been found to have a fracture toughness close to 3.3 $\text{MPa}\cdot\text{m}^{1/2}$ [7,11]. However, a still lower grain size in A0 (0.3 μm) results in a fracture toughness of only 2.2 $\text{MPa}\cdot\text{m}^{1/2}$. The higher toughness measured for BM0 could result from

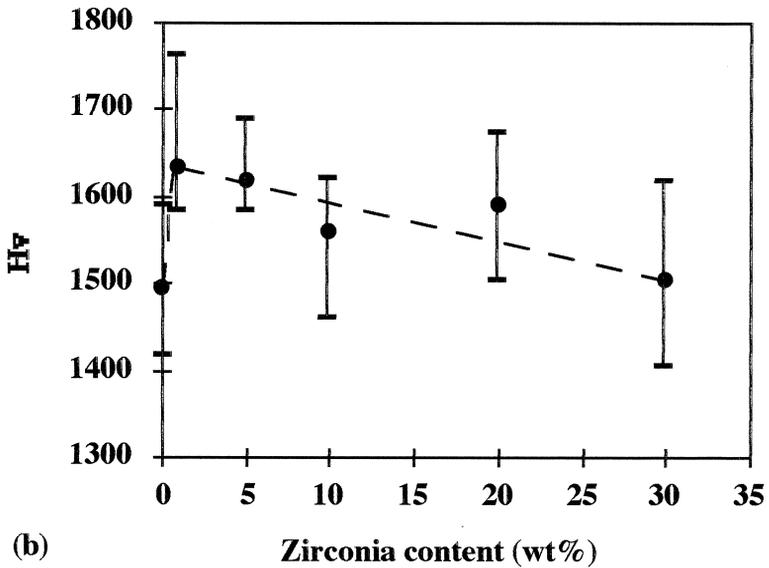
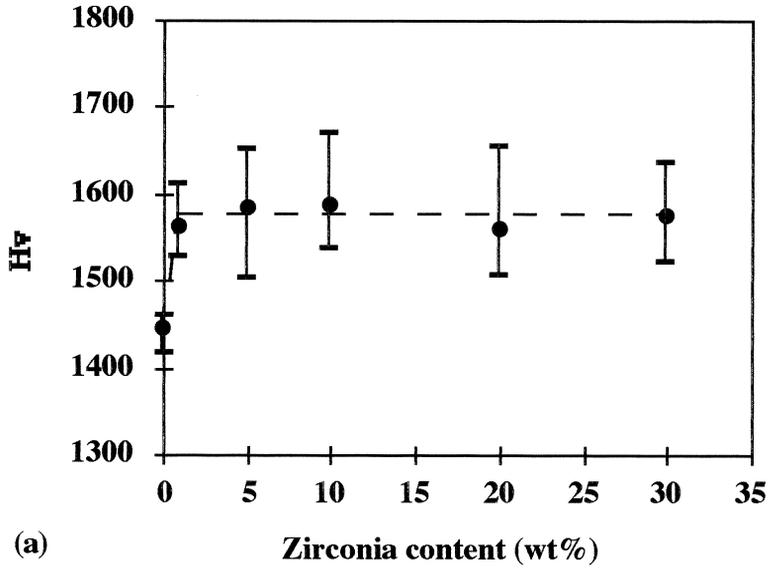


Fig. 1. Vickers microhardness H_V of the (a) BM and (b) A composites. Bars represent the minimum and maximum values. The dashed lines are guides to the eye.

the mixture of transgranular and intergranular fractures, as revealed by SEM observations presented later in this paper, in contrast to an almost totally intergranular fracture for A0.

The fracture strengths of the BM30 (578 MPa) and A30 (506 MPa) composites are higher than those reported by Claussen and Rühle [10] for a 25 wt% ZrO_2 - $MgAl_2O_4$ specimen (500 MPa) and that reported by Fujita et al. [11] for a 24 wt% ZrO_2 - $MgAl_2O_4$ composite (400 MPa). This could reflect the higher ZrO_2 content (30 wt%) in the present composites. Nevertheless, even for lower ZrO_2 content (10 and 20 wt%), the present A composites

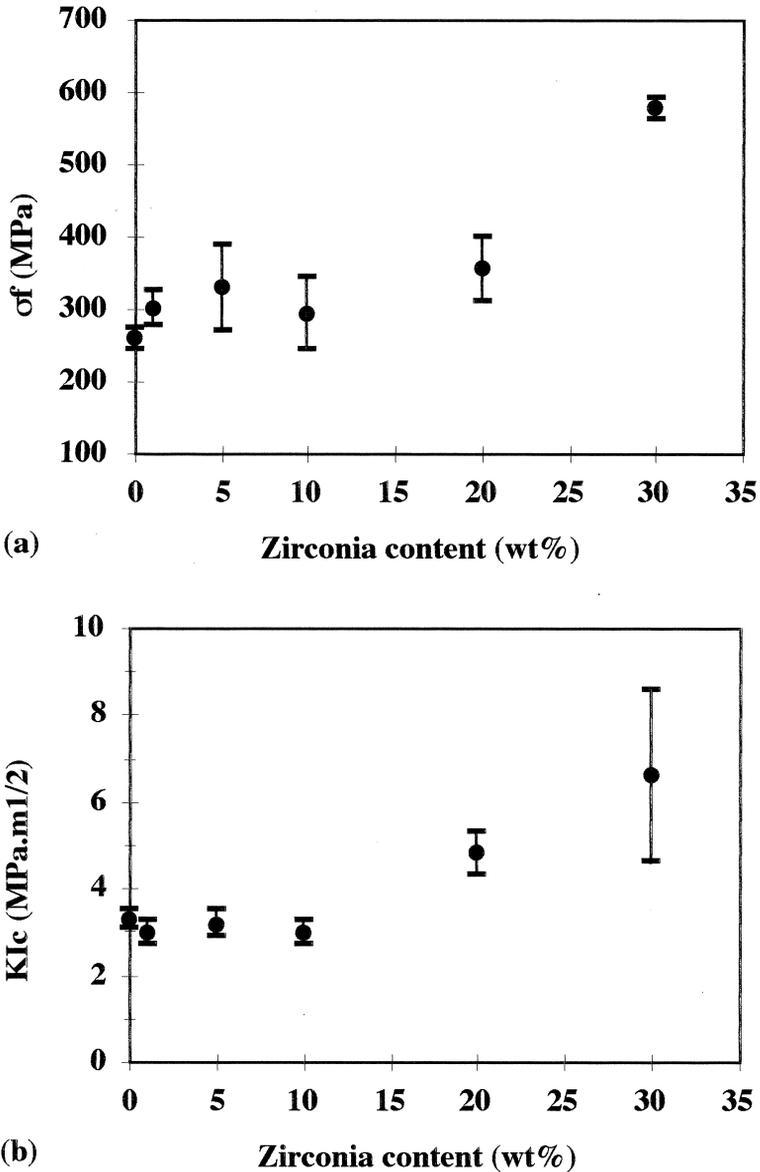


Fig. 2. (a) Fracture strength σ_f and (b) fracture toughness K_{Ic} of the BM composites. Bars represent the minimum and maximum values.

exhibit a higher fracture strength (445 and 489 MPa, respectively) than the previously reported [11] 24 wt% ZrO_2 - $MgAl_2O_4$ specimen. The fracture toughness for both BM30 and A30 (6.6 $MPa \cdot m^{1/2}$) are slightly higher than those reported by Fujita et al. [11] (6.3 $MPa \cdot m^{1/2}$).

The observation that the highest reinforcement is achieved with the composites that contain the highest quantity of zirconia but also the lowest proportion of t- ZrO_2 suggests that

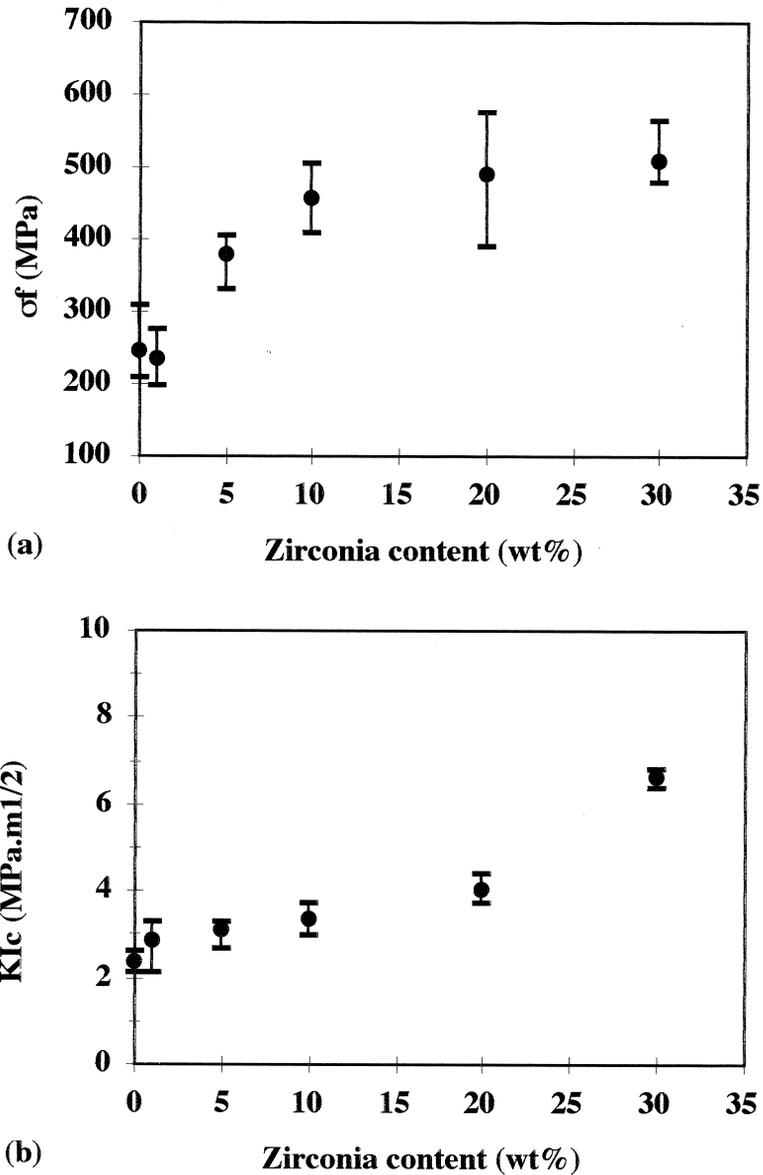


Fig. 3. (a) Fracture strength σ_f and (b) fracture toughness K_{Ic} of the A composites. Bars represent the minimum and maximum values.

several reinforcement mechanisms occur. The presence of m-ZrO₂ and t-ZrO₂ in the hot-pressed materials indeed points towards both the microcracking and stress-induced t → m transformation mechanisms being active simultaneously. This is in agreement with results obtained on ZrO₂-Al₂O₃ composites [16,17]. The hypothesis that polishing could have provoked the t → m phase transformation of ZrO₂ particles located at the surface of the materials was ruled out, because it has been verified that the proportion of m-ZrO₂ is similar

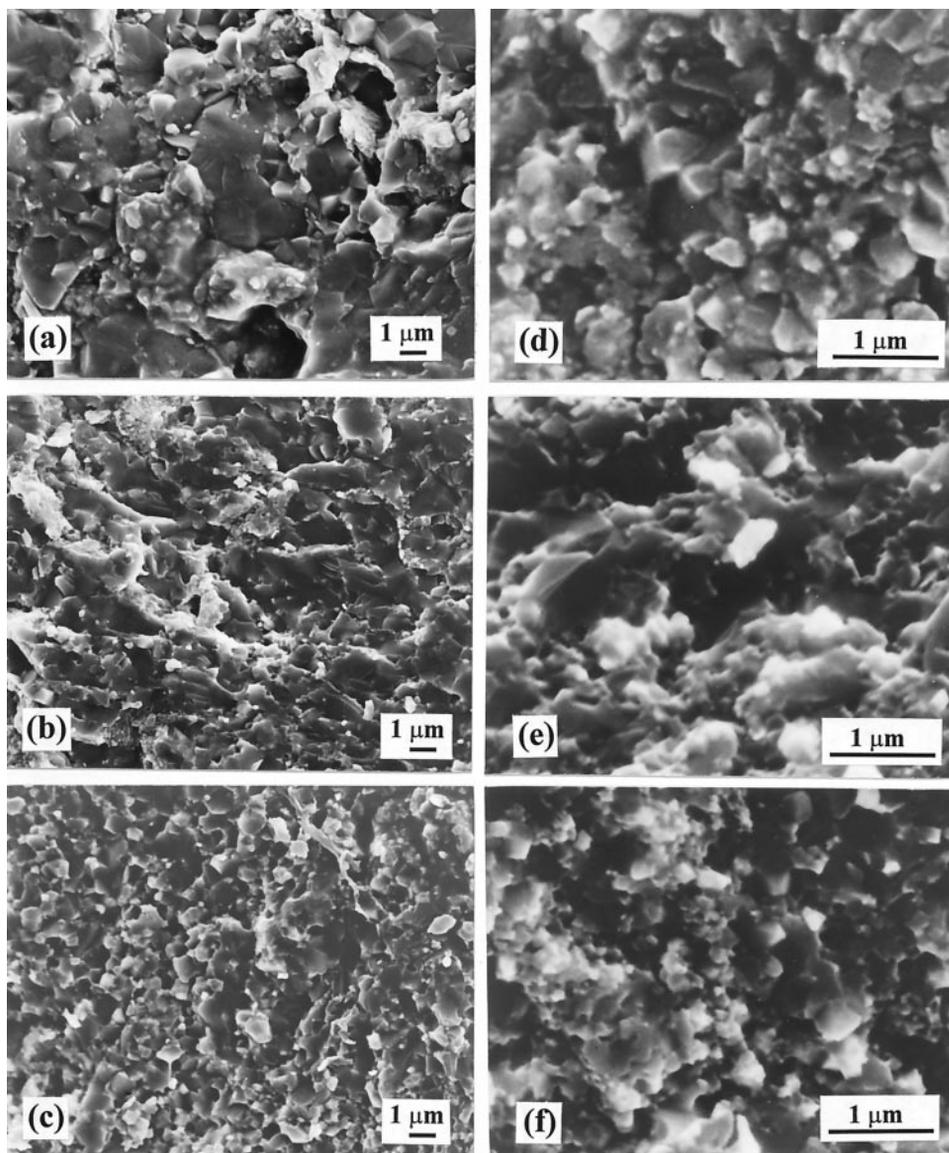


Fig. 4. SEM images of fracture surfaces of (a) BM0, (b) BM5, (c) BM30, (d) A0, (e) A5, and (f) A30.

in the unground, 6 μm -ground, and silica-polished specimens [13]. Thus, it is inferred that there are no compressive surface stresses contributing to the reinforcement.

SEM observation of the fractures of the pure MgAl_2O_4 specimens reveals a mixture of intergranular and transgranular fractures in BM0 (Fig. 4a), whereas they are almost totally intergranular in A0 (Fig. 4d). This could indicate that the critical size under which the fractures are totally intergranular ranges between 0.3 and 1.4 μm (the average grain sizes of BM0 and A0, respectively), which is much lower than the 80–100 μm range reported by White and Kelkar [6]. The fractures of the BM composites (Fig. 4b and c) are similar to those

of BM0 (mixed intergranular and transgranular). However, the transgranular character of the fractures is lessened for the higher ZrO₂ content (BM30 in Fig. 4c). In contrast, the fractures of the A composites (Fig. 4e and f) are not totally identical to that of A0, because some degree of transgranular fracturing is observed. Thus, it appears that the dispersion of ZrO₂ particles could induce some transgranular character to the fracturing in the composites with very small matrix grains (0.3 μm for A specimens).

4. Conclusions

The room-temperature mechanical properties (fracture strength, fracture toughness, and Vickers microhardness) of MgAl₂O₄ and x wt% ZrO₂-MgAl₂O₄ (1 ≤ x ≤ 30) hot-pressed materials were investigated. Compared to the unreinforced spinel, a twofold (or greater) increase in both strengthening and toughening is measured for materials with the highest zirconia content (30 wt%). The presence of m-ZrO₂ and t-ZrO₂ in these composites suggests that both the microcracking and stress-induced t → m transformation mechanisms are active simultaneously. While strengthening and toughening are generally only modest for low zirconia contents, it was found that dispersing only 1 wt% of zirconia in the spinel produces a marked increase in the Vickers microhardness. Two kinds of materials were investigated—those prepared from ball-milled powders, and those prepared from attrited powders. Differences in matrix grain sizes and in the proportions of tetragonal and monoclinic zirconia between one series of specimens and the other could explain some differences observed in the fracture behavior (transgranular, intergranular, or mixed) and in the mechanical properties. However, the total zirconia content appears to be a key parameter.

References

- [1] H. Palmour III, D.M. Choi, L.D. Barnes, R.D. McBrayer, W.W. Krieger, *Mater Sci Res* 1 (1963) 158.
- [2] R.L. Stewart, R.C. Bradt, *J Am Ceram Soc* 63 (1980) 619.
- [3] R.L. Stewart, M. Isawa, R.C. Bradt, *J Am Ceram Soc* 64 (1981) C-22.
- [4] M. Sakai, R.C. Bradt, A.S. Kobayashi, *J Ceram Soc Jpn Int Ed* 96 (1988) 510.
- [5] A. Gosh, K.W. White, M.G. Jenkins, A.S. Kobayashi, R.C. Bradt, *J Am Ceram Soc* 74 (1991) 1624.
- [6] K.W. White, G.P. Kelkar, *J Am Ceram Soc* 75 (1992) 3440.
- [7] C. Baudin, R. Martinez, P. Pena, *J Am Ceram Soc* 78 (1995) 1857.
- [8] R.W. Rice, C.C.M. Wu, *J Mater Sci Lett* 14 (1995) 723.
- [9] J. Wang, R. Stevens, *J Mater Sci* 24 (1989) 3421.
- [10] N. Claussen, M. Rühle, in: *Advanced Ceramics Vol. 3, Science and Technology of Zirconia*, American Ceramics Society, Westerville, OH, 1981, p. 137.
- [11] M. Fujita, H. Yoshimatsu, A. Osaka, Y. Miura, *J Ceram Soc Jpn Int Ed* 103 (1994) 81.
- [12] S.H. Hyun, W.S. Song, *J Mater Sci* 31 (1996) 2457.
- [13] O. Quénard, Ch. Laurent, A. Peigney, A. Rousset, *Mater Res Bull* 35 (12) (2000) in press.
- [14] W.F. Brown, J.E. Srawley, *ASTM Spec Tech Pub* 410, ASTM, Philadelphia, PA, USA, 1966.
- [15] B. Hallstedt, *J Am Ceram Soc* 75 (1992) 1497.
- [16] S. Hori, M. Yoshimura, S. Somiya, *J Am Ceram Soc* 69 (1986) 169.
- [17] M. Rühle, N. Claussen, A.H. Heuer, *J Am Ceram Soc* 69 (1986) 195.