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# Diagnosability Study of Technological Systems

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**Abstract.** This paper describes an approach to study the diagnosability of technological systems, by characterizing their observable behaviors. Due to the interaction between many components, faults can occur in a technological system and cause hard damages not only to its integrity but also to its environment. Though a diagnosis system is a suitable solution to detect and identify faults, it is first important to ensure the diagnosability of the system: will the diagnosis system always be able to detect and identify any fault, without any ambiguity, when it occurs? In this paper, we present an approach to identify and integrate faults in a model of a technological system. Then we use these models for the diagnosability study of faults by characterizing their observable behaviors.

**Keywords:** faults modeling, diagnosability, model-based diagnosis.

## 1 Introduction

Technological systems are complex systems constituted with many components interacting with each other and combining multiple physical phenomena: thermodynamic, hydraulic, electric, etc. Faults, which are un-observable damages affecting components of a system, can occur due to many causes: wear, dirtying, breakage, etc. Some are serious and must require to stop the system, or to put it in a safety mode; while others have minor impact and should only be reported for being repaired off-board. Thus, it is necessary to achieve on-board the detection of these faults and to identify them the most precisely; this in order to take the appropriate decision. An embedded diagnosis system, completing the controller, is a suitable solution to do this ([1]). However, the problem is then to ensure that this diagnosis system will always be able not only to detect any fault when it occurs (does the fault induce an observable behavior distinct from the normality?), but also to assign a unique listed fault to a divergent observable behavior (do some faults induce the same observable behavior?). This problem is known as diagnosability ([2]).

A way to handle this diagnosability, with respect to a system, is to augment the model of this system (the normal model) with faults (producing faulty models); and to exploit them to characterize observable behaviors of the system, under or not a fault,

by a specific property which will be verified by the diagnosis system. This approach, called diagnosability study of faults, inheres in the analysis process of the diagnosis system. It requires, by definition, all faulty models to produce, for each one, a specific fault characterization according to its observable behaviors. All these faults characterizations will then be used by the embedded diagnosis system to detect and identify faults.

In this paper, we present an approach to study the diagnosability of faults of a technological system by exploiting its observable behaviors. These observable behaviors are obtained by using the normal and all faulty models of the system. In the second part, we present the framework to model a technological system and show how to integrate faults in it. In the third part, we exploit these produced models in order to define observable behaviors of the system in the normal and all faulty cases. In the fourth part, we study diagnosability of faults by producing their characterizations. In the fifth part, we apply this theoretical framework to a practical application: a fuel cell system. Finally, the last part concludes by summarizing results and outlining interesting directions for future works.

## 2 System and Faults Modeling

In order to study faults diagnosability of a system, it is necessary to get the normal model and all faulty models of the system. In this part, we present the framework to obtain a model of a system and show how to integrate faults into it.

### 2.1 Normal Model of the System

Classical works found in literature for diagnosis ([1], [3] and [4]) are based on a representation of the system in open-loop. But for the majority of industrial applications, the system is inserted in a closed-loop and its controller computes system inputs by taking into account its outputs; this to increase system performances and to maintain them in spite of unknown perturbations affecting it. In this context fault detection and isolation are more difficult because of the contradiction between control objectives and diagnosis objectives. In fact, control objectives are to minimize disturbances or faults effects; whereas diagnosis objectives are precisely to bring out these faults. The considered solution, to take into account this problem, is to model the system with its controller in closed-loop. Fig. 1 below represents the complete structure of the system: the system and its controller in closed-loop.

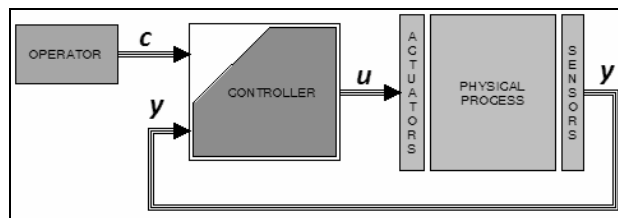


Fig. 1. Complete structure of the system

We model a controlled system with two parts: the controller and the system itself composed of the physical process, actuators and sensors. We consider a continuous model in discrete time  $T$  with a state space representation, described by the set (1) of equations:

$$\begin{aligned} x(t+1) &= f(x(t), \theta, u(t), d(t)), x(0) = x_{init} \\ y(t) &= g(x(t), \theta, u(t), d(t)) \\ a(t+1) &= h(c(t), a(t), y(t)), a(0) = a_{init} \\ u(t) &= k(c(t), a(t), y(t)) \end{aligned} \quad (1)$$

where the two first equations model the system and the two other ones model the controller (more precisely its control laws). Variables  $u$ ,  $x$ ,  $\theta$ ,  $d$  and  $y$  are respectively input, state, parameter, disturbance and output vectors of the system;  $c$  and  $a$  are respectively order (from the operator) and state vectors of the controller. We denote by  $V = \{c; a; u; x; y; d\}$  the set of all variables of the model, with respective domains of values  $C$ ,  $A$ ,  $U$ ,  $X$ ,  $Y$  and  $D$ , and by  $V_{Obs} = \{c; u; y\}$  the set of observable variables.

## 2.2 Faults Modeling

Faults in the system can cause failures or malfunctions, resulting in serious damages not only to the system integrity but also to its environment. It is therefore important to identify and classify all potential faults of the system in order to ensure their integration in the model.

By using methodologies of safety engineering ([5] and [4]), an identification of all important faults of the system can be made. Thanks to faults analysis techniques, such as Failure Mode and Effects Analysis or Fault Tree Analysis, we can identify most of potential faults which could occur in the system; and analyze their causes and impacts. Therefore, the set  $\Gamma = \{F_0, F_1, \dots, F_k\}$  of potential faults, that must be taken into account by a diagnosis system, is identified and defined during this safety analysis, where to simplify the presentation, the fault  $F_0$  represents the normal case.

Potential faults can be classified in order to ensure their integration in the model. Various classifications of faults can be found in literature ([1], [4] and [6]); but all of them differentiate the behavior of the fault and its effects on the system ([7]). Fault behavior is characterized by its occurrence time (randomly, at a specific time or from a specific event), its appearance (abruptly or progressively) and its form (permanent, transient or intermittent). Fault effects consist in its location inside the system and its disturbance induced. For our purpose, we do not consider faults occurring in the controller. Thus, there are sensor faults (perturbing the output vector  $y$ ), actuator faults (perturbing the input vector  $u$ ) and faults in the process (perturbing the state vector  $x$  or the parameter vector  $\theta$ ). The disturbance can be additive, multiplicative, sinusoidal or limitative.

Thus, for a fault  $F \in \Gamma \setminus \{F_0\}$  and a time instant  $t_n \in T$ , the faulty model of the system under  $F$  is obtained by considering the set of equations (1) where the considered disturbed variable  $v$  is replaced by its disturbance  $v_F = dist(t, v(t), flt(t, t_n))$ , with  $flt$  the fault behavior and  $t_n \in T$  its occurrence time. For example with a sensor fault  $F$ , represented by  $y_F(t) = dist(t, y(t), flt(t, t_n))$ , the faulty model of the system is described by the set (2) of equations:

$$\begin{aligned}
 x(t+1) &= f(x(t), \theta, u(t), d(t)), x(0) = x_{init} \\
 y(t) &= dist(t, g(x(t), \theta, u(t), d(t)), flt(t, t_n)) \\
 a(t+1) &= h(c(t), a(t), y(t)), a(0) = a_{init} \\
 u(t) &= k(c(t), a(t), y(t))
 \end{aligned} \tag{2}$$

### 3 Observable Behaviors

By adding faults in the model of the system, we have produced all faulty models requested for the diagnosability study. We can now exploit them to characterize observable behaviors in the normal and all faulty cases. A behavior of the system represents its way of operation, according to an instruction (a sequence of orders) from the operator. An observable behavior is therefore obtained from the behavior by restricting it to the only observable variables. Observable means visible from an external observer, such as a diagnosis system for example.

#### 3.1 System Behaviors

A behavior of the system is represented by the set of values of variables during its operation and according to an instruction from the operator. This operation can be under the presence, or not, of a fault. A behavior is therefore specified according to an instruction and a fault.

An instruction is the evolution of orders from the operator during the time. Formally, it is a sequence  $cs$  from a temporal window  $I_{cs} \subseteq T$ , assumed beginning from the time instant 0, to the domain  $C$ . In the following, we consider a set  $Cons$  of instructions the most representative, i.e.: providing all operation ranges of the system. Thus, though each instruction  $cs$  is defined from its own temporal window  $I_{cs}$ , we assume that all instructions are defined from a same temporal window  $I = \max\{I_{cs}\}$ , by extending any instruction  $cs$ , where  $I_{cs} \subset I$ , with its last value  $cs(\max(I_{cs}))$ .

For a vector  $v = (v_1, \dots, v_n)$  and for an index  $i \in \{1, \dots, n\}$ , we denote by  $p_i(v) = v_i$  the  $i$ -th element of  $v$ . For a set  $E$ , constituted by a direct product  $E = E_1 \times \dots \times E_n$ , for a subset  $G \subseteq E$  and for indexes  $i_1, \dots, i_k \in \{1, \dots, n\}$  with  $k \leq n$ ; the projection of  $G$  onto the  $E_{i_1} \times \dots \times E_{i_k}$  is the set  $\text{Pr}_{E_{i_1} \times \dots \times E_{i_k}}(G) = \{(p_{i_1}(v), \dots, p_{i_k}(v)) \in E_{i_1} \times \dots \times E_{i_k} \mid v \in G\}$ .

**Normal Behaviors.** For an instruction  $cs \in Cons$ , the normal behavior of the system, according to  $cs$ , is the set  $B(cs, F_0)$  of vectors of data  $(t, v(t)) \in I \times C \times A \times U \times X \times Y \times D$ , ordered by time  $t$ , with  $v(t) = (c(t), a(t), u(t), x(t), y(t), d(t))$ . This set of data vectors satisfies the following:

- Existence and uniqueness in time: for any time instant  $t \in I$ , it exists a unique vector  $v(t) \in C \times A \times U \times X \times Y \times D$  such as  $(t, v(t)) \in B(cs, F_0)$ .
- Construction according to the instruction  $cs$ : for any time instant  $t \in I$ ,  $p_1(v(t)) = cs(t)$ .
- Satisfaction of system equations in normal case: for any time instant  $t \in I$ ,
  - $p_4(v(t+1)) = f(p_4(v(t)), \theta, p_3(v(t)), p_6(v(t)))$  and  $p_4(v(0)) = x_{init}$
  - $p_5(v(t)) = g(p_4(v(t)), \theta, p_3(v(t)), p_6(v(t)))$

3.  $p_2(v(t+1)) = h(p_1(v(t)), p_2(v(t)), p_3(v(t)))$  and  $p_2(v(0)) = a_{init}$
4.  $p_3(v(t)) = k(p_1(v(t)), p_2(v(t)), p_3(v(t)))$

**Faulty Behaviors.** A characteristic of faults behaviors, defined in the above part, is the occurrence time (randomly, at a specific time, or from a specific event). In the following, we only consider faults occurring at a specific time; in fact our focus is only to ensure diagnosability of a fault when it occurs, not to predict its occurrence. Thus, for each fault  $F \in \Gamma \setminus \{F_0\}$  and each instruction  $cs \in Cons$ , we consider a set  $\Omega_{(F,cs)}$  of time occurrence  $t_n \in I$  of the fault  $F$  according to the instruction  $cs$ .

Therefore, for an instruction  $cs \in Cons$  and a fault  $F \in \Gamma \setminus \{F_0\}$  occurring at a time instance  $t_n \in \Omega_{(F,cs)}$ , the faulty behavior of the system  $B(cs, F, t_n)$  is defined as the normal one above where points (c) is replaced with the satisfaction of system equations in the considered faulty case.

### 3.2 Observable Behaviors of the System

An observable behavior of the system represents its visible, from an external observer, way of operation according to an instruction from the operator. It is obtained by projecting the behavior, according to the considered instruction, onto the set of observable variables.

In addition, detection and isolation of a fault require, for industrial applications, to be made in bounded time  $b$  after the fault occurrence. This bound can be assumed more than the response time  $\delta$  of the system. Thus, as a behavior could be defined for a fault occurring at the time instant  $t_n = \max(I)$ , it could not consider onto the time interval  $[t_n, t_n + b]$  as it is not defined. Therefore, for any fault  $F \in \Gamma \setminus \{F_0\}$  and any instruction  $cs \in Cons$ , we only consider time occurrences  $t_n \in \Theta_{(F,cs)} = \Omega_{(F,cs)} \cap [0; \max(I) - b]$ .  $F_0$  can be considered as a fault always occurring at the time instant  $t_n = 0$ ; thus,  $\Theta_{(F_0,cs)} = \{0\}$  for any instruction  $cs \in Cons$ .

For a faulty behavior  $B(cs, F, t_n)$ , according to an instruction  $cs \in Cons$  and under a fault  $F \in \Gamma \setminus \{F_0\}$  occurring at a time instance  $t_n \in \Theta_{(F,cs)}$ , the underlying faulty observable behavior  $ObsB(cs, F, t_n)$  is the projection of  $B(cs, F, t_n)$  onto the direct product  $I \times C \times U \times Y$  of observable variables:  $ObsB(cs, F, t_n) = \text{Pr}_{I \times C \times U \times Y}(B(cs, F, t_n))$ .

For a normal behavior  $B(cs, F_0)$ , according to an instruction  $cs \in Cons$ , and the time instant  $t_n \in \Theta_{(F_0,cs)} (= \{0\})$ , the underlying normal observable behavior  $ObsB(cs, F_0, t_n)$  is the projection of  $B(cs, F_0)$  onto the direct product  $I \times C \times U \times Y$  of observable variables:  $ObsB(cs, F_0, t_n) = \text{Pr}_{I \times C \times U \times Y}(B(cs, F_0))$ . The parameter  $t_n$ , which is always equal to 0, is added to harmonize with the notation of faulty observable behaviors  $ObsB(cs, F, t_n)$ .

An observable behavior is defined according to an instruction  $cs \in Cons$ , a fault  $F \in \Gamma$  and an occurrence time  $t_n \in \Theta_{(F,cs)}$  ( $t_n = 0$  for  $F_0$ ). Therefore the set of observable behaviors, according to the set  $Cons$  of instructions and under a fault  $F \in \Gamma$ , is the union of all observable behaviors for all instructions  $cs$  of  $Cons$  and all occurrence time  $t_n \in \Theta_{(F,cs)}$  of  $F$ :  $ObsBeh_{Cons}(F) = \bigcup_{cs \in Cons} \bigcup_{t_n \in \Theta_{(F,cs)}} \{ObsB(cs, F, t_n)\}$ . Finally, the set of observable behaviors, according to the set  $Cons$  of instructions, is the union of all sets of observable behaviors for all faults:  $ObsBeh_{Cons} = \bigcup_{F \in \Gamma} ObsBeh_{Cons}(F)$ . We also

define the time domain  $Tdom(ob)$  of an observable behavior  $ob \in ObsBeh_{Cons}$  as  $I$  and a set  $J = [b; \max(I)] \subset I$ .

## 4 Diagnosability Study of the System

Intuitively a fault  $F \in \Gamma \setminus \{F_0\}$  is said diagnosable if observable behaviors of the system under this fault are not the same that observable behaviors of the system under another fault  $F' \in \Gamma \setminus \{F\}$ . This other fault can be  $F_0$ , or another one  $F' \in \Gamma \setminus \{F_0; F\}$ , which expresses the two ideas: the fault detectability and the fault isolability.

The diagnosability study inheres in the analysis process of the diagnosis system. In fact, during its operation, the diagnosis system will check if the observed behavior of the system, provided by data of observable variables, satisfies a specific property characterizing the normal operation of the system. If this property is not satisfied, it will search which property, characterizing an abnormal operation, is satisfied. Consequently, the diagnosability study will be made from a set  $\Lambda = (P_F)_{F \in \Gamma}$  of properties characterizing the most precisely observable behaviors of the system under the considered fault.  $\Lambda$  is said a faults characterization.

### 4.1 Faults Characterization

For a fault  $F \in \Gamma$ , its characterization is a property  $P_F$  which must be satisfied at each time instant by at least observable behaviors under this considered fault ( $P_F : ObsBeh_{Cons} \times J \rightarrow \{\text{true}; \text{false}\}$ ). We propose two kinds of faults characterization.

**The Perfect Characterization (PC).** The most natural solution to characterize observable behaviors is to consider them restricted to the temporal windows  $[t - b; t]$ , with  $b$  the bound presented above.

- For the fault  $F_0 \in \Gamma$ , the set of bounded normal observable behaviors is  $ObsBeh_{Cons}^{bd}(F_0) = \bigcup_{cs \in Cons} \bigcup_{t \in J} \{\Pr_{[t-b; t] \times C \times U \times Y}(ObsB(cs, F_0, 0))\}$ .
- For a fault  $F \in \Gamma \setminus \{F_0\}$  the set of bounded faulty observable behaviors is  $ObsBeh_{Cons}^{bd}(F) = \bigcup_{cs \in Cons} \bigcup_{t_n \in \Theta_{(F, cs)}} \bigcup_{t \in [t_n; t_n + b]} \{\Pr_{[t-b; t] \times C \times U \times Y}(ObsB(cs, F, t_n))\}$ .

For a fault  $F \in \Gamma$ , its perfect characterization is the property  $P_F$  defined as follow: for an observable behavior  $ob \in ObsBeh_{Cons}$  and a time instant  $t \in J$ ,  $P_F(ob, t)$  is true iff  $\Pr_{[t-b; t] \times C \times U \times Y}(ob) \in ObsBeh_{Cons}^{bd}(F)$ .

Intuitively, an observable behavior  $ob \in ObsBeh_{Cons}$ , restricted to a temporal window  $[t_i - b; t_i]$ , is an element of the set  $ObsBeh_{Cons}^{bd}(F)$  iff it exists an instruction  $cs \in Cons$ , an occurrence time  $t_n \in \Theta_{(F, cs)}$  of  $F$  and a time instant  $t_d \in [t_n; t_n + b]$ , such as data vectors of  $ob$  (which are restricted to the temporal window  $[t_i - b; t_i]$ ) are equal to data vectors of  $ObsB(cs, F, t_n)$  restricted to the temporal window  $[t_d - b; t_d]$ . I.e., if for any time instant  $k \in [0; b] \subseteq T$ , the data vector  $v(t_i + k)$  of  $ob$  at the time instant  $t_i + k$  is equal to the data vector  $v'(t_d + k)$  of  $ObsB(cs, F, t_n)$  at the time instant  $t_d + k$ .

It is a perfect characterization because it is not possible to specify, in a best way, observable behaviors. In fact, the sets  $ObsBeh_{Cons}^{bd}(F)$ , constructed by restricting

elements of  $ObsBeh_{Cons}(F)$ , are the nominal definitions of observable behaviors of the system under a fault; it is therefore not possible to do it better. Nevertheless, not only the set  $Cons$  of instructions must be the most representative: the set  $C^I$  of all functions from the temporal window  $I$  to the domain  $C$ ; but also all sets  $\Theta_{(F,cs)}$  of occurrence time of faults must be equal to  $J$ .

**The Temporal Formulas Characterization (TFC).** This faults characterization describes how the system operates under a fault thanks to a temporal formula. We will use an adaptation of the metric interval temporal logic ([8]), well adapted to specify bounded real-time properties.

The syntax of temporal formulas is classically defined by induction. The set of terms, representing arithmetic formulas, is built from the set  $V_{Obs}=\{c;u;y\}$  of observable variables of the system, a set  $K$  of constants, arithmetic operators ( $+$ ,  $-$ ,  $\cdot$  and  $\div$ ) and a temporal operator  $V_{[\alpha]}$ , where  $\alpha \in T$  is a positive or negative time instant. Atomic formulas, expressing a comparison (equality or inequality) between two arithmetic formulas, are built from the set of terms and by using comparison operators ( $=$ ,  $\neq$ ,  $<$ ,  $>$ ,  $\geq$  and  $\leq$ ). Temporal formulas are therefore built, recursively, with operators  $\neg$  (not),  $\wedge$  (and)  $G_{[\alpha;\beta]}$  (globally during a temporal window bounded by  $\alpha$  and  $\beta$ ) and  $E_{[\alpha;\beta]}$  (eventually during a temporal window bounded by  $\alpha$  and  $\beta$ ); where  $\alpha, \beta \in T$  are two positive or negative time instants. Classical operators  $\vee$  (or) and  $\Rightarrow$  (implication) and  $\Leftrightarrow$  (equivalent) are built from the above operators  $\neg$  and  $\wedge$ .

Temporal formulas are interpreted by observable behaviors  $ob \in ObsBeh_{Cons}$  at each time instant  $t \in J$ : the satisfaction of  $\varphi$  by  $ob$  at the time instant  $t$ , denoted by  $(ob, t) \models \varphi$ , is classically defined by induction onto the set of temporal formulas:

- $(ob, t) \models atom$ , iff  $t \in \text{Dom}(atom) = T\text{dom}(ob)$  and  $atom$  is true when all observable variables are replaced by their values from the vector of  $ob$  at the time instant  $t$ . If  $atom$  contains a term of the form  $V_{[\alpha]}v$ , its satisfaction is obtained if  $t+\alpha \in \text{Dom}(atom)$  and by considering the value of  $v$  at the time instant  $t+\alpha$ .
- $(ob, t) \models \neg\varphi$  iff  $t \in \text{Dom}(\varphi)$  and  $(ob, t)$  does not satisfy  $\varphi$ .
- $(ob, t) \models \varphi \wedge \psi$  iff  $t \in \text{Dom}(\varphi) \cap \text{Dom}(\psi)$  and  $(ob, t) \models \varphi$  and  $(ob, t) \models \psi$ .
- $(ob, t) \models G_{[\alpha;\beta]}\varphi$  iff  $[t+\beta; t+\alpha] \subseteq \text{Dom}(\varphi)$  and for all  $t'$  in  $[t+\beta; t+\alpha]$  we have  $(ob, t') \models \varphi$  (if  $[t-\beta; t-\alpha] \not\subseteq \text{Dom}(\varphi)$  the value of  $G_{[\alpha;\beta]}\varphi$  is not defined).
- $(ob, t) \models E_{[\alpha;\beta]}\varphi$  iff  $[t+\beta; t+\alpha] \subseteq \text{Dom}(\varphi)$  and there exists  $t'$  in  $[t+\beta; t+\alpha]$  such that  $(ob, t') \models \varphi$  (if  $[t-\beta; t-\alpha] \not\subseteq \text{Dom}(\varphi)$  the value of  $E_{[\alpha;\beta]}\varphi$  is not defined).

For example, the formula  $\varphi_{ex}: G_{[-3;0]}((c \in [0;1[) \wedge (c - V_{[-0.1]}c = 0))$ , where  $c \in [0;1[$  means  $(0 \leq c) \wedge (c < 1)$ , asserts that since 3 time units, the variable  $c$  is in the interval  $[0;1[$  and has not changed.

*Fault Characterization Formulas.* All data sets  $ObsBeh_{Cons}(F)$  of observable behaviors under a fault are obtained by simulation. By analyzing them, for each fault  $F \in \Gamma$ , a specific temporal formula  $\varphi_F$  is generated.

The normal formula  $\varphi_{Fo}$  consists in checking thresholds of the gap  $|c - y|$  according to changes of orders during the time:



- Firstly,  $\varphi_{F_0}$  is divided into sub-formulas  $\varphi_{F_0}^i$  according to a partition  $C = \bigcup_{i \in E} C_i$  of the domain  $C$ . This partition represents all operating points of the system. Thus, when the order  $c$  is in a part  $C_i$ , the sub-formula  $\varphi_{F_0}^i$  is checked.
- Secondly, each sub-formula  $\varphi_{F_0}^i$  is divided into two sub-formulas: a sub-formula  $\varphi_{F_0}^{i,h}$  for high changes of order; and another  $\varphi_{F_0}^{i,l}$  for low changes. For a high change of order, more than a threshold, the sub-formula  $\varphi_{F_0}^{i,h}$  is checked from the time of the change and during the response time  $\delta$  of the system. Otherwise, for low changes of order less than the threshold, the sub-formula  $\varphi_{F_0}^{i,l}$  is checked.

All faulty formulas are elaborated by taking into account behaviors and effects of faults. Thus, these characteristics are transformed, if it is possible, into temporal formulas describing how the fault disturbs the gap  $|c - y|$  and all observable variables  $u$  and  $y$ .

For a fault  $F \in \Gamma$ , its temporal formula characterization is the property  $P_F$  defined as follow: for an observable behavior  $ob \in ObsBeh_{Cons}$  and a time instant  $t \in J$ ,  $P_F(ob, t)$  is true iff  $(ob, t) \models \varphi_F$ . Temporal formulas are checked, thanks to the ARTiMon<sup>®</sup> tool, from the CEA, LIST ([9]), interfaced to MATLAB/Simulink<sup>®</sup>.

## 4.2 Diagnosability Study

Whatever is the considered faults characterization  $\Lambda = (P_F)_{F \in \Gamma}$ , we can give a general definition of diagnosability. Although we have presented two kinds of such characterizations (PC and TFC); another kind could be used.

**Formal definitions.** Given a faults characterization  $\Lambda = (P_F)_{F \in \Gamma}$ , a fault  $F \in \Gamma$  is said *diagnosable* if it is eligible, detectable and isolable.

- A fault  $F \in \Gamma$  is *eligible* iff for any instruction  $cs \in Cons$  and for any occurrence time  $t_n \in \Theta_{(F,cs)}$  of  $F$  ( $t_n = 0$  for  $F_0$ ), it exists a time instant  $t_e \in [t_n; t_n + b]$  such that for all time instant  $t \in J$  with  $t \geq t_e$ :  $P_F(ObsB(cs, F, t_n), t)$  is true.
- A fault  $F \in \Gamma \setminus \{F_0\}$  is *detectable* iff for any instruction  $cs \in Cons$  and for any occurrence time  $t_n \in \Theta_{(F,cs)}$ , it exists a time instant  $t_d \in [t_n; t_n + b]$  such that for all time instant  $t \in J$  with  $t \geq t_d$ :  $P_{F_0}(ObsB(cs, F, t_n), t)$  is false.
- A fault  $F \in \Gamma \setminus \{F_0\}$  is *isolable* iff for any instruction  $cs \in Cons$  and for any occurrence time  $t_n \in \Theta_{(F,cs)}$ , it exists a time instant  $t_i \in [t_n; t_n + b]$  such that for all time instant  $t \in J$  with  $t \geq t_i$ :  $P_F(ObsB(cs, F, t_n), t)$  is false for any other fault  $F' \in \Gamma \setminus \{F_0; F\}$ .

**Analysis According to the Kind of Characterization.** We have defined the diagnosability for any faults characterization  $\Lambda = (P_F)_{F \in \Gamma}$ ; we can therefore point up some remarks.

The diagnosability is defined for all faults  $F \in \Gamma$ ; thus for  $F_0$ , there is just to check its eligibility. Furthermore, this eligibility notion is added because as it is defined for any faults characterization  $\Lambda$ , it could be possible to consider one where some faults are not eligible. Obviously, it is not the case with PC: by definition of all sets  $ObsBeh_{Cons}^{bd}(F)$ , all faults are eligible.

Since the diagnosability is defined by the conjunction of three notions, we could study them independently. But in practical applications for example the isolability study of a fault  $F \in \Gamma \setminus \{F_0\}$  will be considered only if  $F$  is detectable and with respect to other detectable faults  $F' \in \Gamma \setminus \{F_0; F\}$ . In fact, if a fault is not detectable for the diagnosability study, it means that it will not be detected by the diagnosis system when it will occur. This is due to the fact that the diagnosability study inheres in the analysis process of the diagnosis system.

We can observe a useful result: if a fault is not diagnosable with PC, it will not be diagnosable with TFC. In fact, TFC is obtained by exploiting the data sets  $ObsBeh_{Cons}(F)$ , thus it can be considered as a reduction of these sets. TFC is therefore a reduction of PC and its diagnosability requirements are thus stronger.

A brief complexity analysis shows the advantage of using TFC for an embedded diagnosis system.

- Space complexity: first, at each  $t_k$  sample, the diagnosis system has to store the received observable data vector. In addition, it has to keep only previous required data vectors during a temporal window bounded according to the considered faults characterization: the bound  $b$  for PC and  $\beta$  for TFC (the size of the longest temporal window appearing in all formulas). Thus, it is a number  $n_{perf} = \#v \cdot (b/u)$  for PC and  $n_{form} = \#v \cdot (\beta/u)$  for TFC, where  $u$  is the time unit (e.g.:  $u = 0.01$ ) and  $\#v$  is the number of observable variables. Then, the diagnosis system must store all formulas for TFC; whereas all data sets  $ObsBeh_{Cons}^{bd}(F)$  for PC. It means a number of data  $m_{form} = n_{form} + \prod_{F \in \Gamma} (2^{h(F)})$  for TFC and  $m = \sum_{F \in \Gamma} (\sum_{cs \in Cons}(m_{F,cs}))$  for PC (where  $h(F)$  is the level of the formula  $F$ ,  $m_{F_0,cs} = (\#J \cdot n_{perf})$  and  $m_{F,cs} = (\#\Theta_{(F,cs)} \cdot (b/u) \cdot n_{perf})$ ,  $\#J$  is the number of time instants between  $b$  and  $\max(I)$  and  $\#\Theta_{(F,cs)}$  is the number of time occurrences  $F$  according to  $cs$ ).
- Time complexity: for each  $t_k$  sample the embedded diagnosis system must check the real observed behavior of the system during a temporal window of operation, according to the considered faults characterization, against all data of observable behavior previously stored, also according to the kind of faults characterization. This time complexity is therefore proportional to the space complexity.

Therefore, PC could not be exploited by an embedded diagnosis system. First, the diagnosis system should have enough memory to store all these data sets  $ObsBeh_{Cons}^{bd}(F)$  for each fault  $F \in \Gamma$ , and enough computational power to make all comparisons. Second, as we have seen, the set  $Cons$  of instructions must be the most representative: the set  $C^I$  of all functions from  $I \subseteq T$  to  $C$ . Therefore this solution would be unusable for complex system with large ranges of operation. Nevertheless, it is useful during design and development phases of the system to intrinsically ensure the diagnosability of faults identified during the safety analysis.

Finally, TFC is perfectly adapted to be embedded inside a diagnosis system. In fact, conception and development phases are actually more and more accomplished with simulation tools which are able to generate the source code of control laws directly for a controller. We could add the embeddable ARTiMon<sup>®</sup> technology (involved in the diagnosability study), with all temporal formulas, during the source code generation; it will be the embedded diagnosis system completing the controller.

## 5 Practical Applications

With the above theoretical framework, we have defined the diagnosability study of faults by analyzing their observable behavior obtained by models. By using simulation tools, such as MATLAB/Simulink<sup>®</sup>, we can apply this theoretical framework in practical applications.

First of all, we require a simulation model of the system. Simulation models used in control design could be a first solution; nevertheless, as showed in [10], we have to keep in mind that models needed for diagnosis are not the same that models needed for control. A model for control is generally less complex than a model for diagnosis.

We assume to have a simulation model of the system (the process and its controller) and furthermore we assume the model of the process represents perfectly the real system.

### 5.1 A Simulation Model Example

For example, we consider a part of a simulation model, developed in Matlab/Simulink<sup>®</sup>, of a fuel cell system embedded in an electric vehicle ([7]). The concerned part is the air alimentation line of the fuel cell stack. To summarize, thanks to a compressor at the beginning and a valve at the end of the line, this air line has to provide air to the fuel cell stack at specific mass flow rates and pressures supplied by the global controller of the fuel cell system. This model can be described, in a simplified manner for the system part, by the set (3) of equations:

$$\begin{aligned}
 P(t+1) &= k(Q_{in}(t) - Q_{out}(t)), P(0) = 1 \\
 Q_{in}(t) &= f_{in}(W(t), P(t)) \\
 Q_{out}(t) &= f_{out}(X(t), P(t)) \\
 W(t) &= \alpha_W \cdot u_W(t) \\
 X(t) &= \alpha_X \cdot u_X(t) \\
 y_P(t) &= \lambda_P \cdot P(t) \\
 y_Q(t) &= \lambda_Q \cdot Q_{in}(t)
 \end{aligned} \tag{3}$$

$P$  is the air pressure in the line.  $Q_{in}$  and  $Q_{out}$  are air mass flow rates respectively before and after the stack.  $W$  is the compressor speed rotation and  $X$  is the valve opening.  $u_W$  and  $u_X$  are respectively compressor and valve orders from the air line controller;  $y_P$  and  $y_Q$  are respectively air pressure and air mass flow rate measures.  $k$ ,  $\alpha_W$ ,  $\alpha_X$ ,  $\lambda_P$ ,  $\lambda_Q$  are constants.

These mass flow rate and pressure are controlled according to orders ( $c_Q$  for mass flow rate and  $c_P$  for pressure) supplied by the global controller of the fuel cell system. The supplied mass flow rate order  $c_Q$  is computed, for the most part, according to the electrical power needed by the vehicle controller (the operator). The pressure order  $c_P$  is then deduced from this mass flow rate according to pressure requirements in the stack and in the line. Thus, we can assume the mass flow rate order  $c_Q$  is the main order. Therefore, the set of observable variables of this air line is  $V_{Obs} = \{c_Q; c_P; u_W; u_X; y_Q; y_P\}$ .

All important faults of the air line have been identified and integrated in the simulation model by using an adapted faults library developed in MATLAB/Simulink<sup>®</sup> ([7]). For example, we consider a lock of the compressor  $F_{lock}$  which causes an abrupt decrease of the mass flow rate output of the compressor; and during the fault presence, this mass flow rate output stays equal to 0 gram per second. Within the model, variable  $Q_{in}$  is therefore disturbed by a multiplicative perturbation and is described by  $Q_{in,F_{lock}}(t) = (1 - flt(t,t_n)) \cdot Q_{in}(t)$ , where  $flt$  is the behavior of  $F_{lock}$ , parameterized to occur abruptly at a time instant  $t_n$  and stay permanent (so  $flt(t,t_n) = 0$  before  $t_n$  and 1 after).

## 5.2 Observable Behaviors Obtained by Simulations

We have considered a set  $Cons$  of instructions representing all operation ranges of the air line. By simulating the normal and all faulty models, according to the set  $Cons$  of instructions, we have obtained all data sets  $ObsBeh_{Cons}(F)$  of observable behaviors for all identified faults  $F \in \Gamma$  parameterized according to their behaviors and effects ([7]).

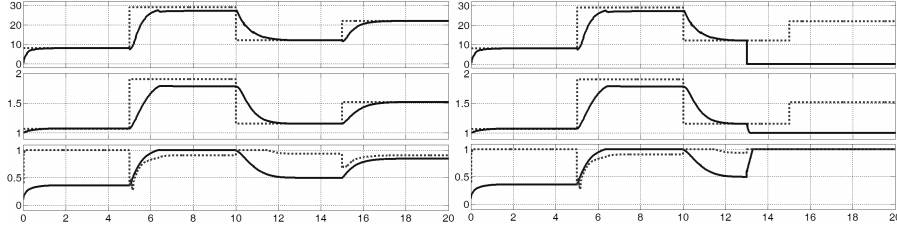
Fig. 2 illustrates two observable behaviors obtained for a random instruction  $cs$  during the temporal window  $[0;20]$ . In the two figures, first and second graphs show the mass flow rate and the pressure in the air line: dotted lines represent orders  $c_Q$  and  $c_P$  whereas plain lines represent measures  $y_Q$  and  $y_P$  from sensors. The third graph shows orders from the air line controller: compressor orders  $u_W$  in plain line and valve orders  $u_X$  in dotted line. Fig. 2 on left shows the normal observable behavior  $ObsB(cs,F_0,0)$  whereas Fig. 2 on right shows the faulty observable behavior  $ObsB(cs,F_{lock},13)$ , for the lock of the compressor occurring at the time instant 13. During the time interval  $[0;13[$ , the air line operates correctly, as the normal behavior; but from the time instant 13, we can see disturbances in all graphs. Mass flow rate measures (first graph) decrease abruptly to 0 gram per second; compressor orders (third graph) are therefore maximal (equal to 1) in order to compensate the difference between orders and measures. Pressure measures (second graph) are thus equal to 1 bar.

## 5.3 Results on the Air Line Model

The diagnosability study of faults in the air line model was achieved with use of the temporal formulas characterization.

For example, the conjunction  $\phi_{F_0}$ , of the two following formulas, characterizes the observable behavior of the air line in the normal case:

$$\begin{aligned} \phi_{F_0}^1: (c_Q \in [0;25]) \Rightarrow & \\ & ( ( G_{[-3;0]}(c - V_{[-0.01]}c = 0) \Rightarrow ( (|c_Q - y_Q| \leq 0.5) \wedge (|c_P - y_P| \leq 0.1) ) ) \\ & \vee ( E_{[-3;0]}(c - V_{[-0.01]}c \neq 0) \Rightarrow ( (|c_Q - y_Q| > 0) \wedge (|c_P - y_P| > 0) ) ) ) \\ \phi_{F_0}^2: (c_Q \in [25;30]) \Rightarrow & \\ & ( ( G_{[-3;0]}(c - V_{[-0.01]}c = 0) \Rightarrow ( (|c_Q - y_Q| \leq 1) \wedge (|c_P - y_P| \leq 0.5) ) ) \\ & \vee ( E_{[-3;0]}(c - V_{[-0.01]}c \neq 0) \Rightarrow ( (|c_Q - y_Q| > 0) \wedge (|c_P - y_P| > 0) ) ) ) \end{aligned}$$



**Fig. 2.** Observable behaviors obtained by simulations (left: normal; right: lock of compressor)

The following formula  $\varphi_{lock}$  characterizes the observable behavior of the air line under the lock of the compressor:

$$\varphi_{lock}: (G_{[-1;0]}((y_Q = 0) \wedge (y_P = 1) \wedge (u_W = 1) \wedge (u_X = 1)))$$

We consider the set of faults  $\Gamma = \{F_0; F_{lock}\}$ , where  $F_0$  is the normal case and  $F_{lock}$  is the lock of the compressor only occurring at the time instant  $t_n = 13$ . We suppose the set *Cons* of instructions is reduced to  $\{cs\}$  and we consider a bound  $b = 5$ . Thus,  $ObsBeh_{\{cs\}} = \{ObsB(cs, F_0, 0); ObsB(cs, F_{lock}, 13)\}$ , with  $\Theta_{(F_0, cs)} = \{0\}$  and  $\Theta_{(F_{lock}, cs)} = \{13\}$ .

Firstly, the normal observable behavior  $ObsB(cs, F_0, 0)$  satisfies the formula  $\varphi_{F_0}$ . Therefore, the fault  $F_0$  is eligible.

Secondly, the faulty observable behavior  $ObsB(cs, F_{lock}, 13)$  satisfies the faulty formula  $\varphi_{lock}$  from the time instant  $t_c = 14, 3 \in [13; 18]$ ; therefore, the fault  $F_{lock}$  is eligible. In addition, from the time instant 13, this faulty observable behavior  $ObsB(cs, F_{lock}, 13)$  does not satisfy the normal formula  $\varphi_0$ ; the fault  $F_{lock}$  is therefore detectable.

Of course, it is just an example. Firstly, the set of instructions is not reduced to only one but contains several ones representing all operation ranges of the system. Moreover, all identified faults have been taken into account with several occurrence times: before or after a change of orders and according the response time  $\delta$  of the system. Furthermore all real temporal formulas obtained are more elaborated.

## 6 Conclusions and Perspectives

In this paper, our goal was to exploit faulty models of a technological system to study faults diagnosability. We have first presented the theoretical framework to define observable behaviors of a system under, or not, a fault. It considers a model of the system with its controller and integrates faults, preliminary identified and classified, in this model. Then, according to a set of instructions representing all operation ranges of the system, we have defined observable behaviors in the normal and all faulty cases. They consist in sets of vectors of observable data ordered by time according to a given instruction of the set of instructions.

The notion of faults diagnosability was defined regardless of a considered faults characterization, describing, the most precisely, how the system operates under or not a fault. Two faults characterizations were proposed. A perfect one, well adapted for

the study during design and development phases of the system, simply considers all sets of data vectors, restricted to temporal windows. The other one uses temporal logic formalism to express the temporal evolution of observable data of the system and is adapted for an embedded diagnosis system.

Finally, for diagnosable faults, their characterization will then be embedded inside the diagnosis system in order to detect and identify faults on line. It could be combined with an embedded model of the system simulated by the controller and temporal formulas could take into account the temporal evolution of the difference between real and model outputs data. These future works will be presented in forthcoming papers.

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