

Optimization of Fault Detection Performance for a Class of Nonlinear Systems

Denis Efimov, Ali Zolghadri

► **To cite this version:**

Denis Efimov, Ali Zolghadri. Optimization of Fault Detection Performance for a Class of Nonlinear Systems. International Journal of Robust and Nonlinear Control, Wiley, 2012, 22 (17), pp.1969-1982. <10.1002/rnc.1802>. <hal-00745300>

HAL Id: hal-00745300

<https://hal.inria.fr/hal-00745300>

Submitted on 25 Oct 2012

HAL is a multi-disciplinary open access archive for the deposit and dissemination of scientific research documents, whether they are published or not. The documents may come from teaching and research institutions in France or abroad, or from public or private research centers.

L'archive ouverte pluridisciplinaire **HAL**, est destinée au dépôt et à la diffusion de documents scientifiques de niveau recherche, publiés ou non, émanant des établissements d'enseignement et de recherche français ou étrangers, des laboratoires publics ou privés.

Optimization of Fault Detection Performance for a Class of Nonlinear Systems

Denis Efimov, Ali Zolghadri

Abstract— The problem of observer design for fault detection in a class of nonlinear systems subject to parametric and signal uncertainties is studied. The design procedure includes formalized optimization of observer free parameters in terms of trade-offs for fault detection performance and robustness to external disturbances and model uncertainties. The technique makes use of some monotonicity conditions imposed on the estimation error dynamics. Efficiency of the proposed approach is demonstrated through the Oscillatory Failure Case in aircraft control surface servo-loops.

I. MOTIVATIONS AND PROBLEM SETTING

Model-based Fault Detection and Isolation (FDI) in dynamical systems has been an active research area during the last three decades (see [12] for a recent survey). Different design and evaluation tools to enhance the robustness of FDI schemes against small parameter variations and other disturbances have been proposed ([7], [9]). An important focus has been on the use of observer-based schemes. In the linear case, it has been shown that any linear fault detection filter can be transformed into an observer-based form [6], providing a unified framework for analysis and implementation [8], [10], [15], [26], [27]. From an estimation point of view, the problem of optimal noise filtering for stochastic linear systems has many solutions [14], [22]. For nonlinear systems, a general framework does not exist, although numerical or suboptimal solutions are available [1], [16], [20]. Typically, the observer design problem is solvable if the system model can be transformed into a canonical form that may be a hard assumption to satisfy in many applications [4], [17].

Usually various linear approximations are used to optimize the fault detection performance of a nonlinear observer. In this paper, a formal approach is developed for nonlinear fault detection observer design, together with a procedure for parameter tuning. For the latter, the design is made under monotonicity assumption [23] for the estimation error dynamic. In this case, using an appropriate linear parameter varying (LPV) transformation [21], [5], [13], the design of minorant and majorant monotone linear systems is possible, whose solutions form an envelope for the original system trajectories. Solving an optimization problem for the minorant and majorant systems (the solution is straightforward due to their linearity), it is possible to obtain a suboptimal solution for the original nonlinear system. This solution could be the locally optimal one when the system solutions converge to the minorant or majorant flows. The optimization problem is formulated in the presence of uncertain parameters and disturbances. The goal is to maximize robustness with respect to disturbances and sensitivity with respect to faults.

In some applications the faulty signal is known to belong to a specific class of signals. Such *a priori* available information simplifies the process of searching the solution, since specific techniques can be used for the design of observer gains. For example, the early and robust detection of Oscillatory Failure Case (OFC) in aircraft control surface servo-loops is an important practical problem [11]. An OFC is a harmonic function of time with unknown frequency and unknown amplitude

The authors are with University of Bordeaux, IMS-lab, Automatic control group, 351 cours de la libération, 33405 Talence, France, {[Denis.Efimov](mailto:Denis.Efimov@ims-bordeaux.fr); [Ali.Zolghadri](mailto:Ali.Zolghadri@ims-bordeaux.fr)}@ims-bordeaux.fr (the present place of work of the first author is Non-A project at INRIA - LNE, Parc Scientifique de la Haute Borne, 40 avenue Halley, Bât. A Park Plaza, 59650 Villeneuve d'Ascq, France).

This work was performed in the framework of the European ADDSAFE project (<http://addsafe.deimos-space.com>): Grant agreement №: FP7-233815.

that can be propagated through the control loop to the control surface and could produce unacceptable structural loads and vibrations [11], [2]. The research work presented in this paper is originally motivated by the above application.

In this work we will consider the following model of a nonlinear system:

$$\dot{\mathbf{x}} = \mathbf{A}\mathbf{x} + \mathbf{G}\mathbf{F}(\mathbf{H}\mathbf{x}, \mathbf{u} + \mathbf{f}, \boldsymbol{\theta}) + \mathbf{S}\mathbf{v}, \quad \mathbf{y} = \mathbf{C}\mathbf{x} + \mathbf{d}, \quad (1)$$

where $\mathbf{x} \in \mathbb{R}^n$, $\mathbf{u} \in \mathbb{R}^m$, $\mathbf{y} \in \mathbb{R}^p$ are the system state, input and output; $\mathbf{v} \in \mathbb{R}^v$, $\mathbf{d} \in \mathbb{R}^p$ are the state and the output disturbances; $\mathbf{f} \in \mathbb{R}^m$ is the faulty signal (unknown portion of the input); $\boldsymbol{\theta} \in \mathbb{R}^q$ is the vector of unknown parameters; the matrices \mathbf{A} , \mathbf{G} , \mathbf{H} , \mathbf{S} , \mathbf{C} are known and constant having appropriate dimensions; the function $\mathbf{F}: \mathbb{R}^{l+m+q} \rightarrow \mathbb{R}^g$ is continuously differentiable. The matrices \mathbf{G} and \mathbf{H} are introduced to take into account more accurately the influence of nonlinearity on the system behavior. For simplicity of presentation, the signal \mathbf{f} is considered to act on the control signal as additive disturbance. However the approach can be applied to multiplicative faults also. Assume that all input signals \mathbf{u} , \mathbf{f} , \mathbf{v} and \mathbf{d} are (Lebesgue) measurable and essentially bounded, i.e.

$$\|\mathbf{f}\| = \text{ess sup}_{t \geq 0} |\mathbf{f}(t)| < +\infty.$$

The objective is to design an observer for (1) using the available noisy measurements \mathbf{y} and the input \mathbf{u} , and ensuring robustness with respect to the parametric $\boldsymbol{\theta}$ and the signal \mathbf{v} , \mathbf{d} uncertainties. Moreover, for fault detection it is required to find the observer gains maximizing sensitivity of the output estimation error with respect to \mathbf{f} and robustness with respect to \mathbf{v} and \mathbf{d} .

Note that, if the fault detection problem is not of interest, then \mathbf{f} can be considered as an additional unknown input.

Two solutions of this problem are presented below. One is based on LMIs verification (Section 4), another utilizes the monotone systems routine for analysis and optimization (Section 5).

The proposed routine for observer gains optimization manages the design trade-off in terms of robustness and performance. The choice of the observer gains plays a key role in the overall observer design and a general formalized methodology is required for their selection. Typically, the observer design approaches guarantee the estimation error stability and without such a procedure, the observer could behave very poorly and the fault detection specifications will not be satisfied. An important contribution of this paper is to include this problem as an integral part for design nonlinear fault detection observers.

The paper is organized as follows. Preliminaries are given in Section 2. The observer equations are introduced in Section 3. Stability conditions based on LMIs are presented in Section 4 (the optimization possibilities of this approach are also discussed). An alternative approach for the observer stability analysis and the new optimization technique are given in Section 5. In Section 6 the overall approach is illustrated through its application to oscillatory failure detection in aircraft control surface servo-loops.

II. PRELIMINARIES

This section introduces some basic notions about monotone systems and LPV representation of nonlinearities.

A. LPV representation of nonlinear functions

For any two vectors \mathbf{p} and \mathbf{p}' of the same dimension define $L(\mathbf{p}, \mathbf{p}') = \{\lambda\mathbf{p} + (1-\lambda)\mathbf{p}', 0 \leq \lambda \leq 1\}$ (the line connecting the points \mathbf{p} and \mathbf{p}'). Since the vector valued function \mathbf{F} in (1) is continuously differentiable, then according to the Mean

Value Theorem, for any $\mathbf{h}, \mathbf{h}' \in \mathbf{HX}$, $\mathbf{u}, \mathbf{u}' \in \mathcal{U} \cup \mathcal{F}$, $\boldsymbol{\theta}, \boldsymbol{\theta}' \in \boldsymbol{\Omega}$ there exist $\boldsymbol{\eta}_j^h \in L(\mathbf{h}, \mathbf{h}')$, $\boldsymbol{\eta}_j^u \in L(\mathbf{u}, \mathbf{u}')$, $\boldsymbol{\eta}_j^\theta \in L(\boldsymbol{\theta}, \boldsymbol{\theta}')$, $j = \overline{1, g}$ such that

$$\mathbf{F}(\mathbf{h}, \mathbf{u}, \boldsymbol{\theta}) - \mathbf{F}(\mathbf{h}', \mathbf{u}', \boldsymbol{\theta}') = \Delta_x(\mathbf{h} - \mathbf{h}') + \Delta_u(\mathbf{u} - \mathbf{u}') + \Delta_\theta(\boldsymbol{\theta} - \boldsymbol{\theta}'),$$

$$\Delta_{x,j} = \left. \frac{\partial F_j(\boldsymbol{\xi}, \mathbf{v}, \mathbf{q})}{\partial \boldsymbol{\xi}} \right|_{\boldsymbol{\xi}=\boldsymbol{\eta}_j^x, \mathbf{v}=\boldsymbol{\eta}_j^v, \mathbf{q}=\boldsymbol{\eta}_j^q}, \Delta_{\theta,j} = \left. \frac{\partial \mathbf{F}(\boldsymbol{\xi}, \mathbf{v}, \mathbf{q})}{\partial \mathbf{q}} \right|_{\boldsymbol{\xi}=\boldsymbol{\eta}_j^x, \mathbf{v}=\boldsymbol{\eta}_j^v, \mathbf{q}=\boldsymbol{\eta}_j^q}, \Delta_{u,j} = \left. \frac{\partial F_j(\boldsymbol{\xi}, \mathbf{v}, \mathbf{q})}{\partial \mathbf{v}} \right|_{\boldsymbol{\xi}=\boldsymbol{\eta}_j^x, \mathbf{v}=\boldsymbol{\eta}_j^v, \mathbf{q}=\boldsymbol{\eta}_j^q}, j = \overline{1, g},$$

where the symbols $\Delta_{x,j}$, $\Delta_{u,j}$, $\Delta_{\theta,j}$ denote the j -th row of the corresponding matrix.

The application of this technique gives an *exact* equivalent LPV representation of a nonlinear function. It is not a linearization around a single point (or around a trajectory) since the above expression is an equality. The LPV approach allows us to transform nonlinear models to linear ones depending on unknown parameters Δ_x , Δ_u and Δ_θ . Therefore, the complexity of the nonlinear model (1) can be replaced with enlarged parametric uncertainty of a linear one. This tool will be applied in the next section to analyze the estimation error dynamics of the observer.

B. Monotone system theory

The system

$$\dot{\mathbf{x}} = \mathbf{f}(t, \mathbf{x}), \mathbf{x} \in X, t \geq 0$$

with the solution $\mathbf{x}(t, \mathbf{x}_0)$ for the initial condition $\mathbf{x}(0) = \mathbf{x}_0$ is called *monotone*, if $\mathbf{x}_0 \leq \boldsymbol{\xi}_0 \Rightarrow \mathbf{x}(t, \mathbf{x}_0) \leq \mathbf{x}(t, \boldsymbol{\xi}_0)$ for all $t \geq 0$ [23] (for the vectors \mathbf{x}_0 , $\boldsymbol{\xi}_0$ the inequality $\mathbf{x}_0 \leq \boldsymbol{\xi}_0$ is understood elementwise). The system is called *cooperative* if $\partial f_i(t, \mathbf{x}) / \partial x_j \geq 0$ for all $1 \leq i \neq j \leq n$, $t \in R$ and $\mathbf{x} \in X$ [23]. Cooperative systems form a subclass of monotone ones. A matrix \mathbf{A} with dimension $n \times n$ is called Metzler if $A_{i,j} \geq 0$ for all $1 \leq i \neq j \leq n$. Note that for the cooperative stable system (the matrix \mathbf{A} is Metzler and Hurwitz)

$$\dot{\mathbf{s}}(t) = \mathbf{A}\mathbf{s}(t) + \mathbf{r}(t), \mathbf{s} \in R^n, \mathbf{r} \in R^n, t \geq 0$$

the properties $\mathbf{s}(0) \geq 0$, $\mathbf{r}(t) \geq 0$ for all $t \geq 0$ imply $\mathbf{s}(t) \geq 0$ for $t \geq 0$ and, conversely, $\mathbf{s}(0) \leq 0$, $\mathbf{r}(t) \leq 0$ for all $t \geq 0$ ensures $\mathbf{s}(t) \leq 0$ for $t \geq 0$.

III. ROBUST OBSERVER EQUATIONS

This section is based on the following assumption.

Assumption 1. Let the compact sets $\mathcal{X} \subset \mathbb{R}^n$, $\mathcal{U} \subset \mathbb{R}^m$, $\mathcal{F} \subset \mathbb{R}^m$, $\mathcal{V} \subset \mathbb{R}^r$, $\mathcal{D} \subset \mathbb{R}^p$ and $\boldsymbol{\Omega} \subset \mathbb{R}^q$ be given such that for almost all $t \geq 0$:

$$\mathbf{x}(t) \in \mathcal{X}, \mathbf{u}(t) \in \mathcal{U}, \mathbf{f}(t) \in \mathcal{F}, \mathbf{v}(t) \in \mathcal{V}, \mathbf{d}(t) \in \mathcal{D} \text{ and } \boldsymbol{\theta} \in \boldsymbol{\Omega}. \quad \square$$

Such constraints are rather common in nonlinear observer design theory stating that the system (1) has bounded inputs and the state, and the admissible bounds on the system trajectories and inputs are known.

Consider the following Luenberger type observer for (1):

$$\begin{aligned} \dot{\mathbf{z}} = \mathbf{Z}(\mathbf{z}, \mathbf{y}, \mathbf{u}) = & \mathbf{A}\mathbf{z} + \mathbf{G}\mathbf{F}[\mathbf{H}\mathbf{z} + \mathbf{L}_2(\mathbf{y} - \mathbf{C}\mathbf{z}), \mathbf{u} + \\ & + \mathbf{L}_3(\mathbf{y} - \mathbf{C}\mathbf{z}), \boldsymbol{\theta}^* + \mathbf{L}_4(\mathbf{y} - \mathbf{C}\mathbf{z})] + \mathbf{L}_1(\mathbf{y} - \mathbf{C}\mathbf{z}), \end{aligned} \quad (2)$$

where $\mathbf{z} \in \mathbb{R}^n$ is an estimate of the state \mathbf{x} ; \mathbf{L}_i , $i = \overline{1,4}$ are the observer gains to be designed, $\boldsymbol{\theta}^* \in \boldsymbol{\Omega}$ is a supporting fixed value for the vector of unknown parameters. In (2) the output injection term is introduced for all arguments of the nonlinear function \mathbf{F} . The gain \mathbf{L}_1 is standard, it is used to ensure stability of the pure linear part of the estimation error $\mathbf{e} = \mathbf{x} - \mathbf{z}$ dynamics. The gain \mathbf{L}_2 has been proposed in [3] in order to improve robustness abilities of (2) and to relax restrictiveness of the LMIs used for the observer design. The gains \mathbf{L}_3 , \mathbf{L}_4 have been introduced in [2] to improve robustness of the system with respect to \mathbf{v} , \mathbf{d} , $\boldsymbol{\theta}$ and sensitivity with respect to \mathbf{f} . These gains have to be assigned to guarantee (or to find a trade-off) the system stability and performance, to satisfy the required estimation and fault detection specifications.

To apply the LPV technique below, the observer (2) has to be equipped with a projection algorithm ensuring that $\mathbf{z}(t)$ belongs to the set \mathcal{X} for all $t \geq 0$:

$$\dot{\mathbf{z}} = \text{proj}_{\mathcal{X}}\{\mathbf{Z}(\mathbf{z}, \mathbf{y}, \mathbf{u})\}, \quad (3)$$

the equations of the projection algorithm can be found in [19] (smooth projection).

From (1), (2) the estimation error \mathbf{e} dynamics can be given by:

$$\begin{aligned} \dot{\mathbf{e}} = & \mathbf{A}\mathbf{x} + \mathbf{G}\mathbf{F}(\mathbf{H}\mathbf{x}, \mathbf{u} + \mathbf{f}, \boldsymbol{\theta}) + \mathbf{S}\mathbf{v} - \mathbf{A}\mathbf{z} - \mathbf{G}\mathbf{F}[\mathbf{H}\mathbf{z} + \\ & + \mathbf{L}_2(\mathbf{y} - \mathbf{C}\mathbf{z}), \mathbf{u} + \mathbf{L}_3(\mathbf{y} - \mathbf{C}\mathbf{z}), \boldsymbol{\theta}^* + \mathbf{L}_4(\mathbf{y} - \mathbf{C}\mathbf{z})] - \\ & - \mathbf{L}_1(\mathbf{y} - \mathbf{C}\mathbf{z}) = (\mathbf{A} - \mathbf{L}_1\mathbf{C})\mathbf{e} - \mathbf{L}_1\mathbf{d} + \mathbf{S}\mathbf{v} + \\ & + \mathbf{G}\{\mathbf{F}(\mathbf{H}\mathbf{x}, \mathbf{u} + \mathbf{f}, \boldsymbol{\theta}) - \mathbf{F}[\mathbf{H}\mathbf{z} + \mathbf{L}_2(\mathbf{y} - \mathbf{C}\mathbf{z}), \mathbf{u} + \\ & + \mathbf{L}_3(\mathbf{y} - \mathbf{C}\mathbf{z}), \boldsymbol{\theta}^* + \mathbf{L}_4(\mathbf{y} - \mathbf{C}\mathbf{z})]\}. \end{aligned}$$

Under Assumption 1 with $\mathbf{z} \in \mathcal{X}$ due to (3), and applying the LPV transformation method we can show that there exist some maps $\Delta_x : \mathbb{R} \rightarrow \mathbb{R}^{s \times l}$, $\Delta_u : \mathbb{R} \rightarrow \mathbb{R}^{s \times m}$, $\Delta_\theta : \mathbb{R} \rightarrow \mathbb{R}^{s \times q}$ such that for all $t \geq 0$

$$\begin{aligned} \mathbf{F}(\mathbf{H}\mathbf{x}, \mathbf{u} + \mathbf{f}, \boldsymbol{\theta}) - \mathbf{F}[\mathbf{H}\mathbf{z} + \mathbf{L}_2(\mathbf{y} - \mathbf{C}\mathbf{z}), \mathbf{u} + \mathbf{L}_3(\mathbf{y} - \mathbf{C}\mathbf{z}), \boldsymbol{\theta}^* + \\ + \mathbf{L}_4(\mathbf{y} - \mathbf{C}\mathbf{z})] = \Delta_x(t)[(\mathbf{H} - \mathbf{L}_2\mathbf{C})\mathbf{e} - \mathbf{L}_2\mathbf{d}] + \\ + \Delta_u(t)[\mathbf{f} - \mathbf{L}_3\mathbf{C}\mathbf{e} - \mathbf{L}_3\mathbf{d}] + \Delta_\theta(t)[\boldsymbol{\theta} - \boldsymbol{\theta}^* - \mathbf{L}_4\mathbf{C}\mathbf{e} - \mathbf{L}_4\mathbf{d}]. \end{aligned}$$

The exact values of the matrix functions $\Delta_x(t)$, $\Delta_u(t)$, $\Delta_\theta(t)$ are unknown, but the set of admissible values is known (the values of the function \mathbf{F} gradient on \mathcal{X} , \mathcal{U} , \mathcal{F} , \mathcal{V} , \mathcal{D} and $\boldsymbol{\Omega} \subset \mathbb{R}^q$), i.e. there are the known sets of matrices Υ_x , Υ_u , Υ_θ such that for all $t \geq 0$:

$$\Delta_x(t) \in \Upsilon_x, \Delta_u(t) \in \Upsilon_u, \Delta_\theta(t) \in \Upsilon_\theta.$$

Having enabled the projection algorithm (3), we can now apply a LPV transformation to the equation of estimation error dynamics:

$$\begin{aligned} \dot{\mathbf{e}} = & \{(\mathbf{A} - \mathbf{L}_1\mathbf{C}) + \mathbf{G}[\Delta_x(t)(\mathbf{H} - \mathbf{L}_2\mathbf{C}) - \Delta_u(t)\mathbf{L}_3\mathbf{C} - \\ & - \Delta_\theta(t)\mathbf{L}_4\mathbf{C}]\}\mathbf{e} - \{\mathbf{L}_1 + \mathbf{G}[\Delta_x(t)\mathbf{L}_2 + \Delta_u(t)\mathbf{L}_3 + \\ & + \Delta_\theta(t)\mathbf{L}_4]\}\mathbf{d} + \mathbf{S}\mathbf{v} + \mathbf{G}\{\Delta_u(t)\mathbf{f} + \Delta_\theta(t)[\boldsymbol{\theta} - \boldsymbol{\theta}^*]\}. \end{aligned} \quad (4)$$

The signal $\mathbf{C}\mathbf{e}(t)$ is available for measurements and can be used for residual generation in fault detection.

R e m a r k . As we can conclude from (4), the influence of the measurement noise \mathbf{d} on $\mathbf{C}\mathbf{e}$ is hard to attenuate since the multiplicative gain for this input is proportional to the sum of all \mathbf{L}_i , $i = \overline{1,4}$. However, robustness with respect to the inputs \mathbf{v} , \mathbf{f} and the parametric mismatch $\boldsymbol{\theta} - \boldsymbol{\theta}^*$ can be augmented by a proper choice of the gains \mathbf{L}_i , $i = \overline{1,4}$ (the same with the sensitivity with respect to \mathbf{f}). \square

In the following sections two techniques are presented for stability analysis of (4) and performance improvement of (2), (3) as well.

IV. LMI BASED STABILITY CONDITIONS

Denote the identity matrix with dimension $n \times n$ by \mathbf{I}_n , and state the symbols $\lambda_{\max}(\mathbf{P})$, $\lambda_{\min}(\mathbf{P})$ for the maximal and minimal eigenvalues of a square matrix \mathbf{P} .

A. Stability conditions

Theorem 1. Assume that

1. Assumption 1 is satisfied.
2. There exist matrices \mathbf{W}_x , \mathbf{W}_u , \mathbf{W}_θ such that

$$\tau_x \Delta_x^T \Delta_x - \Delta_x^T \mathbf{W}_x - \mathbf{W}_x^T \Delta_x - \alpha_x \mathbf{I}_g \leq 0, \quad \tau_u \Delta_u^T \Delta_u - \Delta_u^T \mathbf{W}_u - \mathbf{W}_u^T \Delta_u - \alpha_u \mathbf{I}_g \leq 0, \quad \tau_\theta \Delta_\theta^T \Delta_\theta - \Delta_\theta^T \mathbf{W}_\theta - \mathbf{W}_\theta^T \Delta_\theta - \alpha_\theta \mathbf{I}_g \leq 0$$

for all $\Delta_x \in \Upsilon_x$, $\Delta_u \in \Upsilon_u$, $\Delta_\theta \in \Upsilon_\theta$ and some real τ_x , τ_u , τ_θ , α_x , α_u , α_θ .

3. The gains \mathbf{L}_i , $i = 1, 4$ for some $\mathbf{P} = \mathbf{P}^T > 0$ admit the matrix inequality

$$\mathbf{Y} = \begin{bmatrix} (\mathbf{A} - \mathbf{L}_1 \mathbf{C})^T \mathbf{P} + \mathbf{P}(\mathbf{A} - \mathbf{L}_1 \mathbf{C}) & \mathbf{P}\mathbf{G} & -\mathbf{P}\mathbf{G} & -\mathbf{P}\mathbf{G} \\ \mathbf{G}^T \mathbf{P} & 0 & 0 & 0 \\ -\mathbf{G}^T \mathbf{P} & 0 & 0 & 0 \\ -\mathbf{G}^T \mathbf{P} & 0 & 0 & 0 \end{bmatrix} \leq \begin{bmatrix} \mathbf{Z} & -(\mathbf{H} - \mathbf{L}_2 \mathbf{C})^T \mathbf{W}_x^T & -(\mathbf{L}_3 \mathbf{C})^T \mathbf{W}_u^T & -(\mathbf{L}_4 \mathbf{C})^T \mathbf{W}_\theta^T \\ -\mathbf{W}_x (\mathbf{H} - \mathbf{L}_2 \mathbf{C}) & \tau_x \mathbf{I}_g & 0 & 0 \\ -\mathbf{W}_u \mathbf{L}_3 \mathbf{C} & 0 & \tau_u \mathbf{I}_g & 0 \\ -\mathbf{W}_\theta \mathbf{L}_4 \mathbf{C} & 0 & 0 & \tau_\theta \mathbf{I}_g \end{bmatrix},$$

where

$$\mathbf{Z} = -v \mathbf{I}_n - \alpha_x (\mathbf{H} - \mathbf{L}_2 \mathbf{C})^T (\mathbf{H} - \mathbf{L}_2 \mathbf{C}) - \alpha_u (\mathbf{L}_3 \mathbf{C})^T (\mathbf{L}_3 \mathbf{C}) - \alpha_\theta (\mathbf{L}_4 \mathbf{C})^T (\mathbf{L}_4 \mathbf{C}).$$

Then in (1)–(3) for all $t \geq 0$ we have

$$\|\mathbf{e}(t)\| \leq \kappa \{ \|\mathbf{e}(0)\| e^{-0.25v\lambda_{\min}^{-1}(\mathbf{P})t} + 4v^{-1}(\sqrt{\lambda_d} \|\mathbf{d}\| + \sqrt{\lambda_s} \|\mathbf{s}\| + \sqrt{\lambda_f} \|\mathbf{f}\| + \sqrt{\lambda_\theta} \|\boldsymbol{\theta} - \boldsymbol{\theta}^*\|) \},$$

$$\kappa = \sqrt{\lambda_{\max}(\mathbf{P}) / \lambda_{\min}(\mathbf{P})}, \quad \lambda_\theta = \max_{\Delta_\theta \in \Upsilon_\theta} \lambda_{\max}(\Delta_\theta^T \mathbf{G}^T \mathbf{P} \mathbf{P} \mathbf{G} \Delta_\theta),$$

$$\lambda_d = \max_{\Delta_x \in \Upsilon_x, \Delta_u \in \Upsilon_u, \Delta_\theta \in \Upsilon_\theta} \lambda_{\max}(\{\mathbf{L}_1 + \mathbf{G}[\Delta_x \mathbf{L}_2 + \Delta_u \mathbf{L}_3 + \Delta_\theta \mathbf{L}_4]\}^T \mathbf{P} \mathbf{P} \{\mathbf{L}_1 + \mathbf{G}[\Delta_x \mathbf{L}_2 + \Delta_u \mathbf{L}_3 + \Delta_\theta \mathbf{L}_4]\}),$$

$$\lambda_v = \lambda_{\max}(\mathbf{S}^T \mathbf{P} \mathbf{P} \mathbf{S}), \quad \lambda_f = \max_{\Delta_u \in \Upsilon_u} \lambda_{\max}(\Delta_u^T \mathbf{G}^T \mathbf{P} \mathbf{P} \mathbf{G} \Delta_u).$$

Proof. The projection algorithm ensures the trajectories boundedness in the large ($\mathbf{z}(t) \in \mathcal{X}$ for all $t \geq 0$), let us analyze the error dynamics (4) into the set \mathcal{X} using the Lyapunov function $\mathbf{V}(\mathbf{e}) = \mathbf{e}^T \mathbf{P} \mathbf{e}$:

$$\begin{aligned} \dot{\mathbf{V}} &= \mathbf{e}^T [(\mathbf{A} - \mathbf{L}_1 \mathbf{C})^T \mathbf{P} + \mathbf{P}(\mathbf{A} - \mathbf{L}_1 \mathbf{C})] \mathbf{e} + 2\mathbf{e}^T \mathbf{P} \{ \mathbf{G}[\Delta_x(t)(\mathbf{H} - \mathbf{L}_2 \mathbf{C}) - \Delta_u(t)\mathbf{L}_3 \mathbf{C} - \Delta_\theta(t)\mathbf{L}_4 \mathbf{C}] \} \mathbf{e} - 2\mathbf{e}^T \mathbf{P} \{ \mathbf{L}_1 + \\ &+ \mathbf{G}[\Delta_x(t)\mathbf{L}_2 + \Delta_u(t)\mathbf{L}_3 + \Delta_\theta(t)\mathbf{L}_4] \} \mathbf{d} + 2\mathbf{e}^T \mathbf{P} \mathbf{S} \mathbf{v} + \\ &+ 2\mathbf{e}^T \mathbf{P} \mathbf{G} \{ \Delta_u(t)\mathbf{f} + \Delta_\theta(t)[\boldsymbol{\theta} - \boldsymbol{\theta}^*] \}. \end{aligned}$$

For $\boldsymbol{\rho}(t, \mathbf{e}) = [\mathbf{e} \quad \Delta_x(t)(\mathbf{H} - \mathbf{L}_2 \mathbf{C})\mathbf{e} \quad \Delta_u(t)\mathbf{L}_3 \mathbf{C}\mathbf{e} \quad \Delta_\theta(t)\mathbf{L}_4 \mathbf{C}\mathbf{e}]^T$, applying some algebra we get:

$$\begin{aligned}\dot{V} &= \boldsymbol{\rho}(t, \mathbf{e})^T \mathbf{Y} \boldsymbol{\rho}(t, \mathbf{e}) - \\ &\quad - 2\mathbf{e}^T \mathbf{P} \{ \mathbf{L}_1 + \mathbf{G}[\Delta_x(t)\mathbf{L}_2 + \Delta_u(t)\mathbf{L}_3 + \Delta_\theta(t)\mathbf{L}_4] \} \mathbf{d} + \\ &\quad + 2\mathbf{e}^T \mathbf{P} \mathbf{S} \mathbf{v} + 2\mathbf{e}^T \mathbf{P} \mathbf{G} \{ \Delta_u(t)\mathbf{f} + \Delta_\theta(t)[\boldsymbol{\theta} - \boldsymbol{\theta}^*] \}.\end{aligned}$$

Using the matrix inequality for \mathbf{Y} introduced in the theorem we obtain:

$$\begin{aligned}\boldsymbol{\rho}(t, \mathbf{e})^T \mathbf{Y} \boldsymbol{\rho}(t, \mathbf{e}) &\leq \mathbf{e}^T \{ -\nu \mathbf{I}_n + (\mathbf{H} - \mathbf{L}_2 \mathbf{C})^T [\tau_x \Delta_x^T(t) \Delta_x(t) - \\ &\quad - \Delta_x^T(t) \mathbf{W}_x - \mathbf{W}_x^T \Delta_x(t) - \alpha_x \mathbf{I}_g] (\mathbf{H} - \mathbf{L}_2 \mathbf{C}) + \\ &\quad + (\mathbf{L}_3 \mathbf{C})^T [\tau_u \Delta_u^T(t) \Delta_u(t) - \Delta_u^T(t) \mathbf{W}_u - \mathbf{W}_u^T \Delta_u(t) - \\ &\quad - \alpha_u \mathbf{I}_g] (\mathbf{L}_3 \mathbf{C}) + (\mathbf{L}_4 \mathbf{C})^T [\tau_\theta \Delta_\theta^T(t) \Delta_\theta(t) - \Delta_\theta^T(t) \mathbf{W}_\theta - \\ &\quad - \mathbf{W}_\theta^T \Delta_\theta(t) - \alpha_\theta \mathbf{I}_g] (\mathbf{L}_4 \mathbf{C}) \} \mathbf{e}.\end{aligned}$$

Substitution of the inequalities for \mathbf{W}_x , \mathbf{W}_u , \mathbf{W}_θ gives:

$$\boldsymbol{\rho}(t, \mathbf{e})^T \mathbf{Y} \boldsymbol{\rho}(t, \mathbf{e}) \leq -\nu \mathbf{e}^T \mathbf{e},$$

then

$$\begin{aligned}\dot{V} &\leq -\nu \mathbf{e}^T \mathbf{e} - 2\mathbf{e}^T \mathbf{P} \{ \mathbf{L}_1 + \mathbf{G}[\Delta_x(t)\mathbf{L}_2 + \Delta_u(t)\mathbf{L}_3 + \\ &\quad + \Delta_\theta(t)\mathbf{L}_4] \} \mathbf{d} + 2\mathbf{e}^T \mathbf{P} \mathbf{S} \mathbf{v} + 2\mathbf{e}^T \mathbf{P} \mathbf{G} \{ \Delta_u(t)\mathbf{f} + \\ &\quad + \Delta_\theta(t)[\boldsymbol{\theta} - \boldsymbol{\theta}^*] \} \leq -0.5\nu \mathbf{e}^T \mathbf{e} + 8\nu^{-1} (\lambda_d \mathbf{d}^T \mathbf{d} + \\ &\quad + \lambda_s \mathbf{s}^T \mathbf{s} + \lambda_f \mathbf{f}^T \mathbf{f} + \lambda_\theta [\boldsymbol{\theta} - \boldsymbol{\theta}^*]^T [\boldsymbol{\theta} - \boldsymbol{\theta}^*]).\end{aligned}$$

That provides the estimate on the error \mathbf{e} behavior and terminates the proof. \blacksquare

C o m m e n t . The condition on existence of the matrices \mathbf{W}_q , $q \in \{x, u, \theta\}$ looks like hard to satisfy, however it can be easily fulfilled under certain structural restrictions imposed on \mathbf{F} . For example, this condition is always true for $\mathbf{W}_q = 0$ and some τ_q, α_q such that $\tau_q \Delta_q^T \Delta_q \leq \alpha_q \mathbf{I}_g$, $q \in \{x, u, \theta\}$ (introduction of $\mathbf{W}_q \neq 0$ may relax the conservatism of LMI). Additionally, the conditions for \mathbf{W}_q , $q \in \{x, u, \theta\}$ have the form of Lyapunov inequalities and for interval sets Υ_q they solutions can be obtained by a conventional LMI-based routine. Next, if for all F_j , $j = \overline{1, g}$ the partial derivatives are sign definite elementwise, then it is possible to find some \mathbf{W}_q such that for all $\Delta_q \in \Upsilon_q$ the inequalities are true:

$$\Delta_q^T \mathbf{W}_q + \mathbf{W}_q^T \Delta_q \geq 0, \quad q \in \{x, u, \theta\}, \quad (5)$$

then the condition of Theorem 1 holds for $\tau_q = \alpha_q = 0$ (if the inequalities (5) are strict, then $\alpha_q = 0$ only), in these cases the theorem conditions are reduced to LMI checking. \square

B. Performance optimization

The estimate derived in Theorem 1 gives some hints on possible performance optimization for the observer (2). For example, minimization of the value κ / ν improves overall accuracy of estimation. The value $\lambda_{\max}(\mathbf{P})$ regulates the rate of the system convergence. Additional minimization of the values λ_ν , λ_θ and λ_d allows us to increase robustness margins of the estimation error dynamics with respect to corresponding variables. Simultaneous maximization of the value λ_f ensures improvement of the sensitivity with respect to \mathbf{f} . The obtained expressions for these coefficients indicate that their parallel optimization is not possible and a trade-off has to be found. Since such optimization is based on an upper estimate tuning, it

does not provide an optimal solution (the conversation is about a suboptimal one).

The above discussion on the coefficients $\lambda_v, \lambda_\theta, \lambda_f, \lambda_d$ optimization reveals that it is rather hard to optimize robustness of the system with respect to all variables $\mathbf{v}, \boldsymbol{\theta}, \mathbf{d}$ with simultaneous improvement of sensitivity with respect to the faults \mathbf{f} . Additionally, such an adjustment needs application of the nonlinear optimization routine. In the following section we will focus our attention on particular cases (robustness with respect to \mathbf{v} or sensitivity to harmonic signals \mathbf{f}).

V. MONOTONE SYSTEM APPROACH

Another approach for stability analysis and performance optimization is based on the system (4) reduction to linear majorant and minorant systems using *monotone* system techniques, with posterior solution of the optimization problem for these linear simplified systems. To apply the monotone systems theory, rewrite the equation (4):

$$\dot{\mathbf{e}} = \tilde{\mathbf{A}}(t)\mathbf{e} + \mathbf{w}(t), \quad (6)$$

where

$$\begin{aligned} \tilde{\mathbf{A}}(t) &= (\mathbf{A} - \mathbf{L}_1\mathbf{C}) + \mathbf{G}[\Delta_x(t)(\mathbf{H} - \mathbf{L}_2\mathbf{C}) - \Delta_u(t)\mathbf{L}_3\mathbf{C} - \Delta_\theta(t)\mathbf{L}_4\mathbf{C}], \\ \mathbf{w}(t) &= -\{\mathbf{L}_1 + \mathbf{G}[\Delta_x(t)\mathbf{L}_2 + \Delta_u(t)\mathbf{L}_3 + \Delta_\theta(t)\mathbf{L}_4]\}\mathbf{d}(t) + \\ &\quad + \mathbf{S}\mathbf{v}(t) + \mathbf{G}\{\Delta_u(t)\mathbf{f}(t) + \Delta_\theta(t)[\boldsymbol{\theta} - \boldsymbol{\theta}^*]\}. \end{aligned}$$

Under Assumption 1 the signal \mathbf{w} is bounded ($\|\mathbf{w}\| < +\infty$) as well as the matrix function of time $\tilde{\mathbf{A}}$.

Assumption 2. Let for all $\Delta_x \in \Upsilon_x, \Delta_u \in \Upsilon_u, \Delta_\theta \in \Upsilon_\theta$ the matrix

$$(\mathbf{A} - \mathbf{L}_1\mathbf{C}) + \mathbf{G}[\Delta_x(\mathbf{H} - \mathbf{L}_2\mathbf{C}) - \Delta_u\mathbf{L}_3\mathbf{C} - \Delta_\theta\mathbf{L}_4\mathbf{C}]$$

be Metzler, all non-zero elements of \mathbf{C} have the same sign. □

Assumption 2 means that the system (6) is monotone and we can apply the above mentioned theory to their analysis and optimization. This assumption can be relaxed assuming existence of a linear transformation $\mathbf{e} = \mathbf{X}\boldsymbol{\varepsilon}$, such that in the new coordinates $\boldsymbol{\varepsilon}$ the matrix $\mathbf{X}^{-1}\tilde{\mathbf{A}}(t)\mathbf{X}$ is Metzler for all $\Delta_x \in \Upsilon_x, \Delta_u \in \Upsilon_u, \Delta_\theta \in \Upsilon_\theta$. This relaxation is technical and skipped here for brevity of presentation. The matrix \mathbf{C} satisfies this assumption in a conventional case $\mathbf{C} = [1 \ 0 \dots 0]$, thus this condition is also a question of coordinate transformation.

A. Stability conditions

Theorem 2. Let assumptions 1 and 2 hold. Let the gains $\bar{\mathbf{L}}_i, i = \overline{1,4}$ be chosen to satisfy the elementwise constraint

$$(\mathbf{A} - \mathbf{L}_1\mathbf{C}) + \mathbf{G}[\Delta_x(\mathbf{H} - \mathbf{L}_2\mathbf{C}) - \Delta_u\mathbf{L}_3\mathbf{C} - \Delta_\theta\mathbf{L}_4\mathbf{C}] \leq \bar{\mathbf{A}}$$

for all $\Delta_x \in \Upsilon_x, \Delta_u \in \Upsilon_u, \Delta_\theta \in \Upsilon_\theta$, where

$$\bar{\mathbf{A}} = (\mathbf{A} - \mathbf{L}_1\mathbf{C}) + \mathbf{G}[\bar{\Delta}_x(\mathbf{H} - \mathbf{L}_2\mathbf{C}) - \bar{\Delta}_u\mathbf{L}_3\mathbf{C} - \bar{\Delta}_\theta\mathbf{L}_4\mathbf{C}]$$

is Metzler and Hurwitz for some matrices $\bar{\Delta}_k, k \in \{x, u, \theta\}$. Then in (1), (2) the estimation error \mathbf{e} stays bounded for all $t \geq 0$.

Proof. Introduce the following auxiliary dynamical systems (they will be used for analysis purposes only):

$$\dot{\mathbf{e}}^r = \bar{\mathbf{A}}\mathbf{e}^r + \mathbf{w}^r(t), \quad r \in \{m, M\}, \quad (7)$$

$$-\infty < \mathbf{w}^m(t) \leq \mathbf{w}(t) \leq \mathbf{w}^M(t) < +\infty, \quad \mathbf{w}^m(t) \leq 0 \leq \mathbf{w}^M(t)$$

for all $t \geq 0$, where $\mathbf{e}^r \in \mathbb{R}^n$, $r \in \{m, M\}$ and the initial conditions are $\mathbf{e}^m(0) \leq \mathbf{e}(0) \leq \mathbf{e}^M(0)$, $\mathbf{e}^m(0) \leq 0 \leq \mathbf{e}^M(0)$ (all vector inequalities are understood elementwise). Since the matrix $\bar{\mathbf{A}}$ is Hurwitz and $\|\mathbf{w}^r\| < +\infty$, $r \in \{m, M\}$ the variables \mathbf{e}^r , $r \in \{m, M\}$ are bounded for all $t \geq 0$. Moreover, $\mathbf{e}^M(t) \geq 0$, $\mathbf{e}^m(t) \leq 0$ for all $t \geq 0$ for Metzler matrix $\bar{\mathbf{A}}$ and sign definite initial conditions and input signals \mathbf{w}^r , $r \in \{m, M\}$. Define two relative errors $\boldsymbol{\varepsilon}^M = \mathbf{e}^M - \mathbf{e}$ and $\boldsymbol{\varepsilon}^m = \mathbf{e} - \mathbf{e}^m$, then

$$\begin{aligned} \dot{\boldsymbol{\varepsilon}}^M &= \bar{\mathbf{A}}\mathbf{e}^M - \tilde{\mathbf{A}}(t)\mathbf{e} + \mathbf{w}^M(t) - \mathbf{w}(t) = \\ &= \tilde{\mathbf{A}}(t)\boldsymbol{\varepsilon}^M + [\bar{\mathbf{A}} - \tilde{\mathbf{A}}(t)]\mathbf{e}^M + [\mathbf{w}^M(t) - \mathbf{w}(t)], \\ \dot{\boldsymbol{\varepsilon}}^m &= \tilde{\mathbf{A}}(t)\mathbf{e} - \bar{\mathbf{A}}\mathbf{e}^m + \mathbf{w}(t) - \mathbf{w}^m(t) = \\ &= \tilde{\mathbf{A}}(t)\boldsymbol{\varepsilon}^m + [\tilde{\mathbf{A}}(t) - \bar{\mathbf{A}}]\mathbf{e}^m + [\mathbf{w}(t) - \mathbf{w}^m(t)]. \end{aligned}$$

By Assumption 2 the matrix $\tilde{\mathbf{A}}(t)$ is Metzler for all $t \geq 0$ and the signals $[\bar{\mathbf{A}} - \tilde{\mathbf{A}}(t)]\mathbf{e}^M + [\mathbf{w}^M(t) - \mathbf{w}(t)]$, $[\tilde{\mathbf{A}}(t) - \bar{\mathbf{A}}]\mathbf{e}^m + [\mathbf{w}(t) - \mathbf{w}^m(t)]$ are elementwise positive for all $t \geq 0$, therefore the variables $\boldsymbol{\varepsilon}^M(t)$, $\boldsymbol{\varepsilon}^m(t)$ are also positive for all $t \geq 0$ since $\boldsymbol{\varepsilon}^M(0) \geq 0$, $\boldsymbol{\varepsilon}^m(0) \geq 0$. Indeed, if there exists a coordinate $\varepsilon_i^r(t)$, $i \in \overline{1, n}$, $r \in \{m, M\}$ approaching zero for some $t \geq 0$, then necessarily $\dot{\varepsilon}_i^r(t) \geq 0$ from the conditions above, that prevents change of the sign. Thus $\mathbf{e}^m(t) \leq \mathbf{e}(t) \leq \mathbf{e}^M(t)$ for all $t \geq 0$ due to positivity of $\boldsymbol{\varepsilon}^M(t)$, $\boldsymbol{\varepsilon}^m(t)$, that implies \mathbf{e} boundedness. \blacksquare

It follows from Theorem 2, that under the monotonicity Assumption 2 the matrix inequalities from Theorem 1 can be replaced with some simple additive linear matrix constraints. The projection algorithm (3) becomes redundant in this case.

B. Performance optimization

To formulate the optimization criteria we need the following definitions. Let $\gamma: \mathbb{R}_+ \rightarrow \mathbb{R}_+$ be the stability margin gain (that is a nonlinear counterpart of H_∞ gain [24]) for the estimation error \mathbf{e} with respect to the input \mathbf{v} , i.e.

$$\lim_{t \rightarrow +\infty} \|\mathbf{e}(t)\| \leq \gamma(\|\mathbf{v}\|).$$

For any $\mathbf{f}(t) = \boldsymbol{\varepsilon}\alpha \sin(\omega t)$, $\boldsymbol{\varepsilon} = [1 \dots 1]^T \in \mathbb{R}^m$ and some $\alpha > 0$, $\omega > 0$ let $\nu: \mathbb{R}_+^2 \rightarrow \mathbb{R}_+$ be the output frequency response map for (1), (2) (see [18] for such function definition for the class of convergent systems, for generic case such type of maps can be introduced using the theory of Cauchy gains and asymptotic amplitudes [25]), i.e.

$$\lim_{t \rightarrow +\infty} \|\mathbf{C}\mathbf{e}(t)\| \leq \nu(\alpha, \omega).$$

Corollary 1. *Let all conditions of Theorem 2 hold, then*

$$\gamma(\|\mathbf{v}\|) \leq \|\bar{\mathbf{A}}^{-1}\bar{\mathbf{S}}\| \|\mathbf{v}\|, \quad \nu(\alpha, \omega) \leq \alpha \max_{r \in \{m, M\}} |W^r(i\omega)|,$$

where

$$\begin{aligned} \bar{S}_{i,j} &= |S_{i,j}|, \quad i = \overline{1, n}, \quad j = \overline{1, \nu}; \quad W^r(s) = \mathbf{C}(\mathbf{I}_n s - \bar{\mathbf{A}})^{-1} \mathbf{G}^r, \\ \mathbf{G}^M &= \max\{\sup_{\Delta_u \in \Upsilon_u} \mathbf{G}\Delta_u, -\inf_{\Delta_u \in \Upsilon_u} \mathbf{G}\Delta_u\}, \quad \mathbf{G}^m = -\mathbf{G}^M. \end{aligned}$$

Proof. The systems (7) determine the asymptotic behavior for (1), (2) (the estimation accuracy bounds) and the limit quality of transients. These upper and lower bounds can be exact in the cases when $\tilde{\mathbf{A}}(t) \rightarrow \bar{\mathbf{A}}$ and $\mathbf{w}(t) \rightarrow \mathbf{w}^r(t)$,

$r \in \{m, M\}$. The systems (7) are linear, their robustness and sensitivity analysis is simple and numerically tractable. For a linear system (due to the superposition principle) its response to different inputs can be analyzed independently.

The input \mathbf{w} depends on \mathbf{v} in linear fashion with the constant gain \mathbf{S} , then in the signals \mathbf{w}^r , $r \in \{m, M\}$ this term can be taken into account as $\mathbf{S}^r \bar{\mathbf{v}}(t)$, where $S_{i,j}^m = -|S_{i,j}|$, $S_{i,j}^M = |S_{i,j}|$, $\bar{v}_j = |v_j|$, $i = \overline{1, n}$, $j = \overline{1, v}$. For linear systems

$$\dot{\mathbf{e}}^r = \bar{\mathbf{A}} \mathbf{e}^r + \mathbf{S}^r \bar{\mathbf{v}}(t), \quad r \in \{m, M\}$$

we have that $\lim_{t \rightarrow +\infty} |\mathbf{e}^r(t)| \leq |\bar{\mathbf{A}}^{-1} \mathbf{S}^r| \|\bar{\mathbf{v}}\| \leq |\bar{\mathbf{A}}^{-1} \mathbf{S}^r| \|\mathbf{v}\|$. Therefore, $\gamma(\|\mathbf{v}\|) \leq |\bar{\mathbf{A}}^{-1} \bar{\mathbf{S}}| \|\mathbf{v}\|$, $\bar{\mathbf{S}} = \mathbf{S}^M$.

The harmonic input \mathbf{f} influence on the signals \mathbf{w}^r , $r \in \{m, M\}$ can be evaluated using the term $\mathbf{G}^r \bar{\mathbf{f}}(t)$, $r \in \{m, M\}$, where $\mathbf{G}^M = \max\{\sup_{\Delta_u \in \Upsilon_u} \mathbf{G} \Delta_u, -\inf_{\Delta_u \in \Upsilon_u} \mathbf{G} \Delta_u\}$, $\mathbf{G}^m = -\mathbf{G}^M$; $\bar{f}_k(t) = \alpha |\sin(\omega t)|$, $k = \overline{1, m}$. Then the following equations can be analyzed:

$$\dot{\mathbf{e}}^r = \bar{\mathbf{A}} \mathbf{e}^r + \mathbf{G}^r \bar{\mathbf{f}}(t), \quad r \in \{m, M\}.$$

According to Assumption 2 the matrix \mathbf{C} has all elements with the same sign, thus

$$\mathbf{C} \mathbf{e}^m(t) \leq \mathbf{C} \mathbf{e}(t) \leq \mathbf{C} \mathbf{e}^M(t)$$

for all $t \geq 0$ with positive elements of \mathbf{C} , the reverse sign inequalities are satisfied for the negative elements of \mathbf{C} . Therefore in the system (1), (2), the output $\mathbf{C} \mathbf{e}$ response on the harmonic fault input \mathbf{f} can be estimated using the standard Bode magnitude plot:

$$v(\alpha, \omega) \leq \alpha \max_{r \in \{m, M\}} |W^r(i\omega)|,$$

$$W^r(s) = \mathbf{C}(\mathbf{I}_n s - \bar{\mathbf{A}})^{-1} \mathbf{G}^r, \quad r \in \{m, M\}. \quad \blacksquare$$

This approach provides clear guidelines for the performance optimization: minimization of the norm $|\bar{\mathbf{A}}^{-1} \mathbf{S}^r|$, $r \in \{m, M\}$ leads to robustness improvement, maximization of the gain $|W^r(i\omega)|$, $r \in \{m, M\}$ enhances the system sensitivity with respect to harmonic components in \mathbf{f} with the frequency ω . In some cases an analytical solution can be obtained for minimization/maximization of $|\bar{\mathbf{A}}^{-1} \mathbf{S}^r|$ and $|W^r(i\omega)|$, $r \in \{m, M\}$. However, Assumption 2 could be rather restrictive: first, it may fail in some applications, second, even being verified the system with non monotone dynamics may have better performance.

VI. NUMERICAL EXAMPLE: OSCILLATORY FAILURE CASE

In this section the ideas presented in this paper are illustrated through analytical design of a harmonic OFC detector in the Electronic Flight Control System [11]. OFC could result in unacceptable high loads and vibrations particularly if they resonate at a frequency critical for the aircraft structure [11]. For example, an OFC occurring on an aileron creates inertial moment and aerodynamic forces (hinge moment). Due to the control surface oscillation, vibrations appear on the wing leading to the its bending and thus loads are generated very quickly on the wing and then on the whole aircraft. The capability to detect OFC, robustly and as fast as possible, is very important because it has an impact on the structural design of the aircraft. In this paper only failures located in the control servo-loop of the moving surfaces is considered [11]. Habitually, such type of failure generates spurious sinusoidal signals (mainly due to electronic components) propagating through the control

servo-loop, leading to control surface oscillation (see Fig. 1, where the structural scheme of servo-loop is shown). The faulty components may be located inside the flight control computer, the analogue inputs/outputs, the position sensors or the actuators. The flight control computer may also generate unwanted oscillations of the command current sent to the actuator servo-valve. The fault signals are considered to be sinusoidal with amplitude and frequency uniformly distributed over the range 1–10 Hz (above 10 Hz, the failure has no significant effects because of the low-pass nature of the actuator). The detection time is expressed in period numbers, thus depending on the failure frequency, the time permissible for detection is varying.

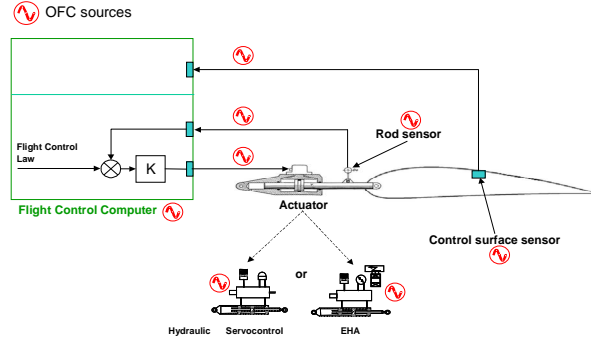


Fig. 1. Structural scheme of the actuator servo-loop.

The following actuator model is considered [11]:

$$\dot{x}(t) = \varphi[y_f(t) - x(t) + u(t) + f(t)] + v(t), \quad (8)$$

$$y_f(t) = W_f(p)[x(t) - u(t) - f(t)], \quad y(t) = x(t) + d(t),$$

where $x \in \mathbb{R}$ is the actuator rod position, $u \in \mathbb{R}$ is the control signal, $y \in \mathbb{R}$ is the available measurement output, $f \in \mathbb{R}$ is the sinusoidal fault, v and d are the disturbances as before; y_f is the output of a filter, p is stated for the time differentiation operator, $W_f(p)$ is the filter transfer function. The function φ and its derivative are given in Fig. 2, for simplicity of presentation a high pass filter is considered in this work: $W_f(p) = -Tp / (Tp + 1)$, $T = 10$.

The model (8) can be presented in the form (1) introducing the following functions and matrices:

$$\mathbf{A} = \frac{1}{T} \begin{bmatrix} 0 & 0 \\ 1 & -1 \end{bmatrix}, \quad \mathbf{G} = \begin{bmatrix} 1 & 0 \\ 0 & T^{-1} \end{bmatrix}, \quad \mathbf{F}(h, u) = \begin{bmatrix} \varphi(h+u) \\ u \end{bmatrix},$$

$$\mathbf{S} = \begin{bmatrix} 1 \\ 0 \end{bmatrix}, \quad \mathbf{H} = \begin{bmatrix} -1 \\ 1 \end{bmatrix}^T, \quad \mathbf{C} = \begin{bmatrix} 1 \\ 0 \end{bmatrix}^T.$$

Assume that the sets required in Assumption 1 are given. Since the system (8) has one nonlinearity only (the condition (5) is satisfied), after some transformations the observer (2) can be presented as follows:

$$\dot{e}_1 = \Delta(t)[e_2 - e_1 + f - (L_2 + L_3)(e_1 + d)] - L_{11}(e_1 + d) + v, \quad (9a)$$

$$\dot{e}_2 = T^{-1}(e_1 - f - e_2) - (L_{12} - T^{-1}L_3)(e_1 + d), \quad (9b)$$

where $\Delta = \varphi'(\eta^h)$ and according to Fig. 2 $0 \leq \Delta(t) \leq \varphi_{\max} = 18.11$ for all $t \geq 0$. For the matrix $\mathbf{P} = \mathbf{I}_2$ the estimate from

Theorem 1 on the error dynamics takes form:

$$|\mathbf{e}(t)| \leq |\mathbf{e}(0)| e^{-0.125t/T} + 2\sqrt{2}[\sqrt{\hat{\phi}_{\max}} + 4/T] \|f\| + \|\nu\| + (L_{11} + \hat{\phi}_{\max}\{L_2 + L_3\} + 2(L_{12} - T^{-1}L_3)) \|d\|.$$

Thus the gain before $\|d\|$ is the only one available for optimization using the observer gains tuning.

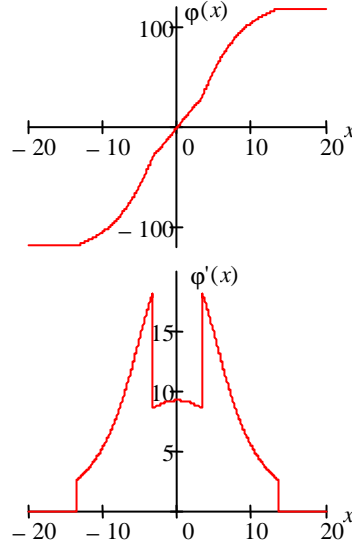


Fig. 2. The actuator nonlinearity.

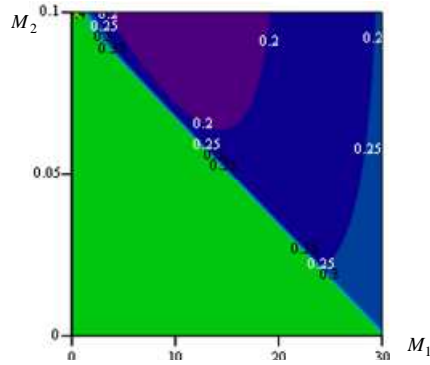


Fig. 3. Performance functional values.

To apply Theorem 2 note that the system (9) is monotonous while $T^{-1}(1 - L_3) \geq L_{12}$. Under this constraint

$$\tilde{\mathbf{A}}(t) = \begin{bmatrix} -L_{11} - (1 + L_2 + L_3)\Delta(t) & \Delta(t) \\ T^{-1} - (L_{12} - T^{-1}L_3) & -T^{-1} \end{bmatrix}$$

is a Metzler matrix for any $0 \leq \Delta(t) \leq \hat{\phi}_{\max}$. Then

$$\bar{\mathbf{A}} = \begin{bmatrix} -L_{11} & \hat{\phi}_{\max} \\ T^{-1} - (L_{12} - T^{-1}L_3) & -T^{-1} \end{bmatrix},$$

$$\mathbf{G}^m = \begin{bmatrix} -\dot{\phi}_{\max} \\ T^{-1} \end{bmatrix}, \quad \mathbf{G}^M = \begin{bmatrix} \dot{\phi}_{\max} \\ T^{-1} \end{bmatrix},$$

and $\bar{\mathbf{A}}$ is Metzler. The matrix $\bar{\mathbf{A}}$ is Hurwitz under proper choice of the gains L_{11} , L_{12} , L_3 . The analytical formulas for gains to be optimized are as follows:

$$\begin{aligned} |\bar{\mathbf{A}}^{-1}\bar{\mathbf{S}}| &= \gamma(M_1, M_2) = \sqrt{1 + M_2^2} / |M_1 - \dot{\phi}_{\max} M_2|, \\ |W^M(i\omega)| &= \beta(\omega, M_1, M_2) = \dot{\phi}_{\max} \sqrt{4 + T^2 \omega^2} / D(\omega, M_1, M_2), \\ |W^m(i\omega)| &= \dot{\phi}_{\max} T \omega / D(\omega, M_1, M_2), \\ D(\omega, M_1, M_2) &= \sqrt{\omega^2 (1 + M_1 T)^2 + (M_1 - T \omega^2 - \dot{\phi}_{\max} M_2)^2}, \end{aligned}$$

where $M_1 = L_{11}$ and $M_2 = 1 - L_{12}T + L_3$ are new tuning parameters. Note that

$$\max_{r \in \{m, M\}} |W^r(i\omega)| = |W^M(i\omega)| = \beta(\omega, M_1, M_2).$$

The values of $\gamma(M_1, M_2)$ and $\beta(\omega, M_1, M_2)$ could be optimized numerically for new set of planar parameters M_1 , M_2 taking in mind stability of the matrix $\bar{\mathbf{A}}$ and the monotonicity constraint $M_2 \geq 0$. The following functional has been chosen for minimization:

$$J(M_1, M_2) = \kappa \gamma(M_1, M_2) + (1 - \kappa) / \sum_{\omega \in \Omega_f} \beta(\omega, M_1, M_2),$$

where $\Omega_f = \{1, 2, 3, 4, 5, 7\}$ is the set of the fault most important frequencies that could happen, $0 \leq \kappa \leq 1$ is a weighting parameter. The contour plot of this functional for $\kappa = 0.3$ is shown in Fig. 3, where the left low uncolored corner corresponds to the cases with unstable matrix $\bar{\mathbf{A}}$. The following values of the observer gains provide the minimum of this functional:

$$L_{11} = 12, \quad L_{12} = 0.1, \quad L_2 = 1, \quad L_3 = 0.08.$$

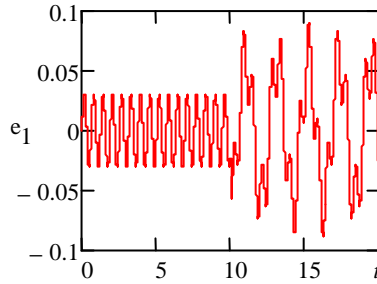


Fig. 4. Behavior of the output residual.

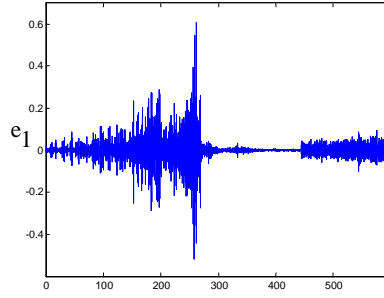


Fig. 5. The output residual in the ADDSAFE benchmark.

These gains form a suboptimal solution in the sense of the observer (2) response optimization. An example of the residual signal e_1 obtained for these observer gains is shown in Fig. 4, where for simulation it was used

$$u = \sin(t) + \sin(0.2t) + \cos(2t), \quad v(t) = \sin(10t),$$

$$f(t) = \begin{cases} 0, & \text{if } t \leq 10, \\ 0.2 \sin(3t), & \text{if } t > 10. \end{cases}$$

For nonlinear systems any type of optimization is a complex issue, even choice of an optimizing functional corresponding to the posed performance goal is a hard problem. In this example, for instance, application of Theorem 1 does not provide a hint how to evaluate the output estimation error sensitivity with respect to harmonic faults. The Theorem 2 provides us with a performance functional in a systematic way, that is a big advantage of the presented approach. This technique has been successfully verified on the OFC detection problem in the European FP7 ADDSAFE project, the result of this algorithm operation in the ADDSAFE benchmark is shown in Fig. 5.

VII. CONCLUSION

The problem of nonlinear observer design for fault detection with optimized performance is studied. It is assumed that the plant model contains unknown parameters and it is subjected by external disturbances and faults. Two approaches for observer design are presented. The first one is based on solution of LMIs, its novelty consists in introduction of additional observer gains in the conventional routine for LMI-based observer design. The additional observer gains may be used for performance optimization. The second method uses monotonicity assumption on the estimation error dynamics, it introduces a new tool to design nonlinear observers. An advantage of the second approach is that it gives a simple technique to tune the observer gains in order to optimize the fault detection performance and robustness. Efficiency of the proposed approach is demonstrated through the oscillatory failure case in aircraft control surface servo-loops.

REFERENCES

- [1] Abbaszadeh M., Marquez H.J. (2008). Robust H_∞ observer design for sampled-data Lipschitz nonlinear systems with exact and Euler approximate models. *Automatica*, **44**(3), pp. 799–806.
- [2] Alcorta-Garcia E., Zolghadri A., Goupil P. (2011). A Nonlinear Observer-Based Strategy for Aircraft Oscillatory Failure Detection: A380 Case Study. *IEEE Trans. Aerospace and Electronic Systems*, October.
- [3] Arcak M., Kokotović P. (2001). Nonlinear observers: a circle criterion design and robustness analysis. *Automatica*, **37**, pp. 1923–1930.
- [4] Besançon G. (Ed.) (2007). *Nonlinear observers and applications*. Lecture Notes in Control and Information Science, v. 363, Springer Verlag: Berlin.

- [5] Bokor J., Balas G. (2004). Detection Filter Design for LPV Systems – a Geometric Approach. *Automatica*, **40**, pp. 511–518.
- [6] Bortoff S.A., Lynch A.F. (1995). Synthesis of optimal nonlinear observers. *Proc. 34th Conf. on Decision and Control*, pp. 95–100.
- [7] Chen J., Patton R.J. (1999). *Robust model-based fault diagnosis for dynamic systems*. Kluwer Academic Publishers.
- [8] Casavola A., Famularo D., Franze G. (2008). Robust fault detection of uncertain linear systems via quasi-LMIs. *Automatica*, **44**, pp. 289–295.
- [9] Ding, S.X. (2008). *Model-based Fault Diagnosis Techniques. Design Schemes, Algorithms, and Tools*. Springer, Heidelberg, Berlin.
- [10] Ding S.X., Jeinsch T., Frank P.M., Ding E.L. (2000). A unified approach to the optimization of fault detection systems. *Int. J. Adaptive Control and Signal Processing*, **14**, pp. 725–745.
- [11] Goupil P. (2010). Oscillatory Failure Case Detection In The A380 Electrical Flight Control System By Analytical Redundancy, *Control Engineering Practice*, **18**, pp. 1110-1119.
- [12] Hwang I., Kim S., Kim Y. (2010). A survey on Fault Detection, Isolation and Reconfiguration methods. *IEEE Trans. Control Systems Technology*, **18**(3), pp. 636–653.
- [13] Lee L.H. (1997). *Identification and Robust Control of Linear Parameter-Varying Systems*. PhD thesis, University of California at Berkeley, Berkeley, California.
- [14] Leonides C.T., Yocum J.F. (1975). Optimal observers for continuous time linear stochastic systems. *Automatica*, **11**(1), pp. 61–73.
- [15] Li X., Zhou K. (2009). A time domain approach to robust fault detection of linear time-varying systems. *Automatica*, **45**, pp. 94–102.
- [16] Moïana M., Bernard O., Gouzé J.-L. (2009). Near optimal interval observers bundle for uncertain bioreactors. *Automatica*, **45**(1), pp. 291–295.
- [17] Nijmeijer H., Fossen T.I. (1999). *New Directions in Nonlinear Observer Design*. London, U.K.: Springer-Verlag.
- [18] Pavlov A.V., van de Wouw N., Nijmeijer H. (2007). Frequency response functions for nonlinear convergent systems. *IEEE Trans. on Aut. Control*, **52**, pp. 1159–1165.
- [19] Pomet J.B., Praly L. (1992). Adaptive nonlinear regulation: Estimation from the Lyapunov equation. *IEEE Trans. Automatic Control*, **AC-37**, pp. 729–740.
- [20] Poznyak A., Nazin A., Murano D. (2004). Observer matrix gain optimization for stochastic continuous time nonlinear systems. *Systems & Control Letters*, **52**(5), pp. 377–385.
- [21] Raïssi T., Videau G., Zolghadri A. (2010). Interval observers design for consistency checks of nonlinear continuous-time systems. *Automatica*, **46**(3).
- [22] Simon D. (2006). *Optimal State Estimation: Kalman, H Infinity, and Nonlinear Approaches*. Wiley-Interscience.
- [23] Smith H.L. (1995). *Monotone Dynamical Systems: An Introduction to the Theory of Competitive and Cooperative Systems*, vol. 41 of Surveys and Monographs, AMS, Providence.
- [24] Sontag E.D. (2007). *Input to state stability: Basic concepts and results*. In P. Nistri and G. Stefani, editors, *Nonlinear and Optimal Control Theory*, pages 163-220. Springer-Verlag, Berlin.
- [25] Sontag E.D. (2002). Asymptotic amplitudes and Cauchy gains: a small-gain principle and an application to inhibitory biological feedback. *Systems & Control Let.*, **47**, pp. 167–179.
- [26] Wang J., Yang G., Liu J. (2007). An LMI approach to H_{∞} index and mixed H_{∞}/H_1 fault detection observer design. *Automatica*, **43**, pp. 1656–1665.
- [27] Zhong M., Ding S.X., Ding E.L. (2010). Optimal fault detection for linear discrete time-varying systems. *Automatica*, **46**, pp. 1395–1400.