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# Design of multi-shell sampling schemes with uniform coverage in diffusion MRI

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## Abstract

**Purpose** In diffusion MRI, a technique known as Diffusion Spectrum Imaging reconstructs the propagator with a discrete Fourier transform, from a Cartesian sampling of the diffusion signal. Alternatively, it is possible to directly reconstruct the orientation distribution function in Q-ball imaging, providing so-called high angular resolution diffusion imaging. In between these two techniques, acquisitions on several spheres in Q-space offer an interesting trade-off between the angular resolution and the radial information gathered in diffusion MRI. A careful design is central in the success of multi-shell acquisition and reconstruction techniques.

**Methods** The design of acquisition in multi-shell is still an open and active field of research however. In this work, we provide a general method to design multi-shell acquisition with uniform angular coverage. This method is based on a generalization of electrostatic repulsion to multi-shell.

**Results** We evaluate the impact of our method using simulations, on the angular resolution in one and two bundles of fibers configurations. Compared to more commonly used radial sampling, we show that our method improves the angular resolution, as well as fiber crossing discrimination.

**Discussion** We propose a novel method to design sampling schemes with optimal angular coverage, and show the positive impact on angular resolution in diffusion MRI.

## Introduction

Diffusion MRI is an imaging technique discovered in the mid 1980's [1, 2, 3] that maps the local displacement probability of water molecules within biological tissues. This has provided a great tool over the past 20 years for the early diagnosis of brain disorders and the study of brain structural connectivity, and a precious help for pre-operative planning in neurosurgery [4, 5]. Using a pulsed-gradient spin-echo sequence [6], the MR echo magnitude is attenuated due to proton diffusion, and by repeating acquisitions with various diffusion encoding gradients, one can characterize and recover information on the water molecules displacement. This in turns reflect the organization of the underlying tissue microstructure, which restricts the displacement of water molecules.

Formally, the diffusion of water molecules is well described by the ensemble average propagator (EAP),  $P(\mathbf{r}; \tau)$ , which is the full 3D probability density function of water molecules displacement during a given observation time  $\tau$ . Under the narrow-pulse assumption, which is verified whenever the diffusion time  $\tau$  is much larger than the pulse duration  $\delta$ , the signal attenuation,  $E(\mathbf{q})$ , is related to the EAP through a Fourier transform [7]:

$$E(\mathbf{q}) = \int_{\mathbb{R}^3} P(\mathbf{r}) e^{2i\pi\mathbf{q} \cdot \mathbf{r}} d\mathbf{r}, \quad (1)$$

where the wavevector is  $\mathbf{q} = \gamma\delta\mathbf{G}/2\pi$ ,  $\gamma$  is the gyromagnetic ratio, and  $\mathbf{G}$  is the magnetic field gradient.

A technique, known as  $q$ -space imaging (QSI) or diffusion spectrum imaging (DSI) [7, 8], consists in sampling the diffusion weighted MR attenuation  $E(\mathbf{q})$  on a Cartesian grid in the reciprocal space. The EAP is then reconstructed through a discrete Fourier transform, and other quantities of interest can be computed such as the orientation distribution function (ODF),  $\psi(\mathbf{u})$ , which is the angular marginal probability density of water molecules motion. This technique has been applied successfully for the *in vivo* imaging of human brain white matter structures. However, the long acquisition time required for such technique limits its application in a clinical context. Several approaches [9, 10, 11, 12, 13] use a hybrid sampling method, where the diffusion attenuation  $E(\mathbf{q})$  is sampled on several spheres in the  $q$ -space, rather than on a Cartesian lattice. Multiple  $q$ -shell sampling offers an interesting trade-off between classical high angular resolution diffusion imaging (HARDI) techniques in  $q$ -ball imaging [14, 15], and DSI.

The design of sampling protocols in single shell has received much attention from the community [16, 17, 18]. However, the design of multi-shell sampling is still an active subject of research. There are many degrees of freedom in the construction of a multi-shell design. If we try to determine all the parameters that fully describe a sampling protocol on several shells, we have: the total number of samples,  $K$ ; the number of spheres in the  $q$ -space,  $S$ ; the shell radii (related to the  $b$ -values),  $q_s$ ; the number of points on each shell,  $K_s$ , such that  $\sum_{s \leq S} K_s = K$ , and the directions on each sampling shell,  $\mathbf{u}_{s,k} \in \mathcal{S}^2$ . With the large and increasing number of reconstruction techniques in the literature [10, 9, 13, 19, 20, 21, 22], it is not clear whether a preferred, unified strategy would fit the needs of every method. In particular we believe that the selection of parameters  $K$ ,  $S$ ,  $q_s$  and  $K_s$  should be driven by the needs of the reconstruction method, the time limit for the acquisition and the physical limitations of the imaging system. Still, the choice of sampling directions should follow the same unified strategy, commonly adopted in  $q$ -ball imaging [16, 17, 18], in order to achieve an angular coverage as uniform as possible. As for the choice of shell radii, number of shells and number of points per shell, we will follow the strategy recently proposed in [22], which is optimized for reconstruction in the continuous and orthonormal basis called modified spherical polar Fourier (mSPF) [23].

In particular, recent studies have shown that for a better angular resolution, the sampling directions should be as different as possible from one shell to another [24, 21, 25]. The constructions in [24] and [25] start from a uniform set of directions on the unit sphere, which is then separated into  $S$  subsets of quasi-uniform directions on the sphere, that correspond to the  $S$  spheres under consideration for sampling. This method leads to a discrete search problem, that is solved at the cost of a timely optimization procedure in [25], or at the cost of a sub-optimal greedy approach in [24]. Another related method, presented in [26] and, in deeper details, in a private communication with the authors, starts from independent sets of directions uniformly spread on the sphere, and then finds the optimal composition of rigid rotations of each set with respect to the others, so that the projection of the rotated sets of points onto the same unit spheres gives the most uniform coverage possible. Finally, the method in [21] is based on a geometrical construction, using the concept of uniform and dual polyhedra. The vertices of two polyhedra dual to each other give two complementary sets of directions, that are used to design multi-shell sampling strategy. The

drawback with this technique is that it only provides two separate sets of directions, which is not enough for more than 2 shells sampling. Moreover, the choice of the number of points per shell is limited by the finite number of uniform polyhedra (see [27] and the related software Kaleido for a mathematical construction).

In this work, we present a general method to design multi-shell sampling protocols, with a uniform coverage on each shell, and a global uniform angular coverage. We propose a cost function that generalizes electrostatic repulsion to multi-shell, which is presented in the first section, together with an efficient method to minimize this cost function. We also show that the same objective function can be used to design incremental acquisition schemes, that are compatible with prematurely aborted scans. In the results section, we compute some geometrical properties of the optimal point sets. We demonstrate the properties of our new sampling scheme through Monte-Carlo simulations. A preliminary version of this work was presented in [28, 29].

## Methods

The cost function we present in this section is a generalization of the electrostatic repulsion in high angular resolution diffusion imaging [16, 17, 18], adapted to the problem of multi-shell sampling. The cost function is made of two terms: the first term controls the repartition on each shell, while the second controls the angular uniformity of the set of directions as a whole. A point set minimizing this cost function can be constructed by direct minimization, and we report how to minimize this cost function. Alternatively, to construct incremental acquisition schemes, that are compatible with prematurely stopped scans (see [30] for instance in  $q$ -ball imaging), the same cost function can be minimized incrementally, following the method in [31].

### Multi-shell $q$ -space sampling with uniform coverage

In the design of  $q$ -ball imaging acquisition, the most popular approach is to spread out the sampling directions as uniformly as possible on the sphere [16, 17, 18]. Similarly, we propose to construct the sampling directions on each shell, with the following principles: First, for the sake of rotational invariance, it is desirable that the coverage of each sphere be as uniform as possible. Second,

we require the whole set of directions (*i.e.* the set of all sampling points in  $q$ -space, reprojected onto the unit sphere) to be as uniform as possible. We therefore propose a split cost function  $V = \alpha V_1 + (1 - \alpha)V_2$ , where  $V_1$  and  $V_2$  address, respectively, the two principles stated above.

The cost function, is a natural generalization of the method in [16, 18] to multi-shell,

$$V_1 = \frac{1}{S} \sum_{s=1}^S \frac{1}{K_s^2} \sum_{i < j} v(\mathbf{u}_{s,i}, \mathbf{u}_{s,j}), \quad (2)$$

where  $S$  is the number of shells,  $K_s$  is the number of points on shell  $s$ , and  $\{\mathbf{u}_{s,k}, k = 1 \dots K_s\}$  are the unit directions on shell  $s$ . The magnitude of the elementary electrostatic repulsion force,  $v$ , between two points  $\mathbf{u}$  and  $\mathbf{v}$  on the unit sphere is "according to Coulomb's law, inversely proportional to the square of the distance between the charges" (see [16]),

$$v(\mathbf{u}, \mathbf{v}) = \frac{1}{\|\mathbf{u} - \mathbf{v}\|^2} + \frac{1}{\|\mathbf{u} + \mathbf{v}\|^2}. \quad (3)$$

This elementary repulsion force ensures that a sampling direction,  $\mathbf{u}$ , and its opposite  $-\mathbf{u}$  play the same role [16, 32]. Minimizing the cost function  $V_1$ , corresponds to minimizing the electrostatic cost function on each shell, separately. Note that the cost of shell  $s$  is weighted by  $1/K_s^2$ ; indeed, the cost function increases as  $K^2$  [32], and this weighting ensures equal importance of the uniformity for each shell.

So that the whole set of sampling directions be uniform, we also consider this second cost function

$$V_2 = \frac{1}{K^2} \sum_{s \neq t} \sum_{i=1}^{K_s} \sum_{j=1}^{K_t} v(\mathbf{u}_{s,i}, \mathbf{u}_{t,j}), \quad (4)$$

where  $K$  is the total number of sampling points in  $Q$ -space. This cost function,  $V_2$ , is the sum of magnitude of all electrostatic forces between any two directions coming from two different shells. This will ensure that the optimal directions are different from one shell to another.

Finally, we construct our set of points by minimizing the cost function

$$V = \alpha V_1 + (1 - \alpha)V_2, \quad (5)$$

under the constraint that each direction lies on the unit sphere,

$$\arg \min_{\mathbf{u}_{s,k} \in \mathbb{R}^3} V(\mathbf{u}_{s,k}), \quad \text{subject to} \quad \forall s \in \{1 \dots S\}, \forall k \in \{1 \dots K_s\}, \|\mathbf{u}_{k,s}\|^2 = 1. \quad (6)$$

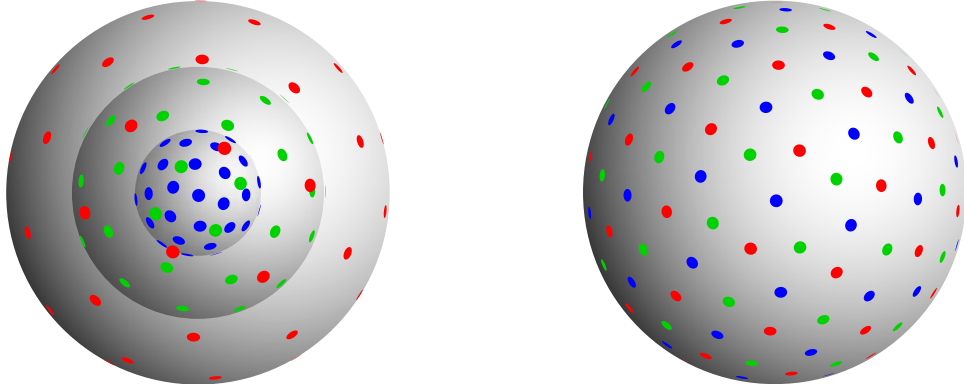


Figure 1: Optimal point set on 3 shells, 30 points per shell. The weighting parameter is set to  $\alpha = 0.5$ . (left) sample points in the  $q$ -space, (right) sampling directions, *i.e.* the sampling points reprojected onto the unit sphere.

This minimization is a non-convex optimization problem under quadratic equality constraint. We implemented the minimization through sequential least squares quadratic programming, with analytically pre-calculated gradient to speedup the optimization. The gradient of the functional  $V$  is derived from the partial derivatives of  $v(\mathbf{u}, \mathbf{v})$ ,

$$\frac{\partial v}{\partial x_{\mathbf{u}}} = -2 \left( \frac{x_{\mathbf{u}} - x_{\mathbf{v}}}{\|\mathbf{u} - \mathbf{v}\|^4} + \frac{x_{\mathbf{u}} + x_{\mathbf{v}}}{\|\mathbf{u} + \mathbf{v}\|^4} \right), \quad (7)$$

where the directions are parameterized by their Cartesian coordinates,  $\mathbf{u} = [x_{\mathbf{u}} \ y_{\mathbf{u}} \ z_{\mathbf{u}}]^T$ . Besides, the equality constraint is also easily implemented, as the normal to the surface defined by the equality constraint is known: it is simply  $\mathbf{u}_{s,k}$ . Our implementation, in Python<sup>TM</sup>, makes use of the `fmin_slsqp` routine from the SciPy optimization package [33]. An example of optimal configuration on 3 shells, with 30 points per shell, and a weighting parameter  $\alpha = 0.5$  is plotted on Fig. 1.

The weighting parameter  $\alpha \in [0, 1]$  balances the trade-off between uniformity on each shell (measured by cost function  $V_1$ ), and angular uniformity of the sampling scheme as a whole (measured by function  $V_2$ ). The case  $\alpha = 0$  is somehow underdetermined, as any rotation of one shell with respect to the others does not change the cost function. At the opposite, the case  $\alpha = 1$  would put all the weight on the global angular uniformity, but nothing would prevent poor coverage of



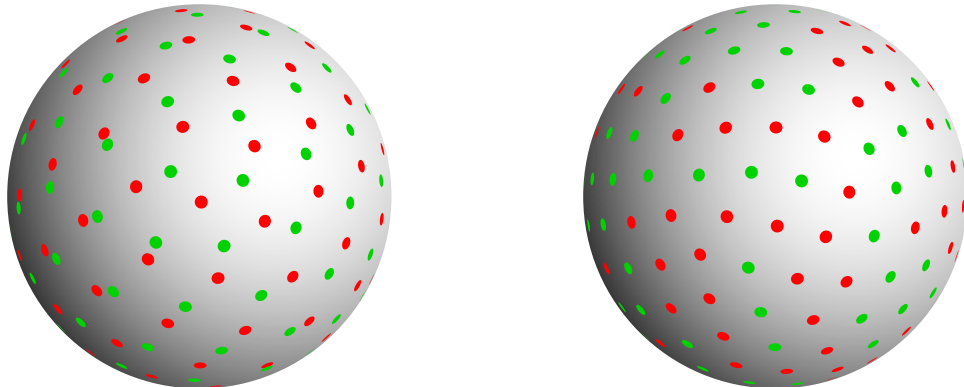


Figure 2: Extremal values of the weighting factor  $\alpha$ : minimum cost configurations for  $S = 2$  shells,  $K_1 = K_2 = 50$  points per shell, points reprojected on the unit sphere. (left)  $\alpha = 0$ : all the importance is given to the uniformity of the configuration on each shell, independently of the other. As a result, the global coverage is non-uniform, and so we get almost "aligned" sampling on both shells. (right)  $\alpha = 1$ : the global angular coverage is uniform, but if we consider the repartition of points on shell 1 (green dots) or shell 2 (red dots) separately, the angular coverage is not uniform.

each single shell. These two extremal cases are illustrated on Fig. 2.

We plot on Fig. 3 the value of both energies  $V_1$  and  $V_2$  for the configuration minimizing  $V$ , while the  $\alpha$  parameter varies from 0 to 1. Except near these extremal values of  $\alpha$ , the solution is not much sensitive to the choice of  $\alpha$ . We chose  $\alpha = 0.5$  throughout our experiments.

### Incremental construction of an optimal arrangement

Some recent work on single shell acquisition design [32, 30, 31] have shown the practical interest of incrementally optimal sampling sequences. In short, these acquisition sequences are carefully designed and ordered, so that an interruption at any point of the acquisition would result in an approximately optimal design. Such designs are compatible with acquisitions that have been stopped early because of subject motion or request. In  $q$ -ball imaging, the greedy optimization method proposed in [31] was shown to be very computationally attractive. Besides, in Q-ball imaging, point sets generated with this method well compare to results obtained by a modification of the cost function, introducing weighting in the sum of magnitude of electrostatic elementary

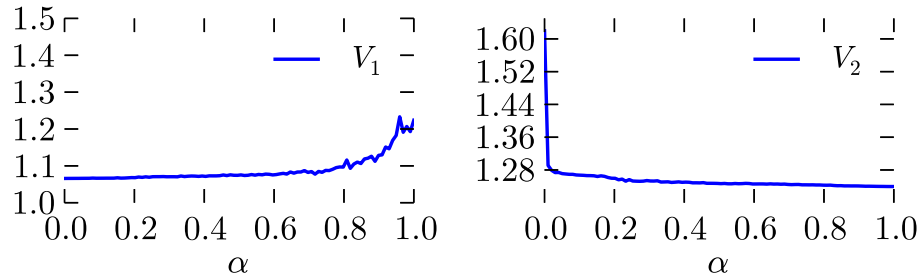


Figure 3: (left) Cost function  $V_1$ , measuring uniformity on each shell, and (right)  $V_2$ , measuring uniformity of the set of directions as a whole. Cost function evaluated for the optimum configurations, for various  $\alpha$ . Except near 0 and 1, the solution does not depend strongly on the choice of  $\alpha$ .

repulsion forces, as in [30, 32]. For these reasons, we adapt the approach in [31] to the problem of multi-shell design.

To find a nearly optimal design for  $K$  points, we construct the point set incrementally. At each iteration  $k$ , we first select the sphere  $s_k$  on which to add the  $k$ -th point, so that the ratio of samples on each shell is approximately respected. Then we find the direction  $\mathbf{u}$  minimizing  $V$ , while the  $k - 1$  previously defined directions remain fixed. This minimization algorithm is very efficient, as at each step, we need to optimize a single direction (two parameters). Furthermore, as we show in the results section, the geometrical properties of this incrementally constructed point set are close to the optimal one, provided that enough sample points are considered.

## Results

### Geometrical properties of multi-shell point sets

We present in this section some geometrical measures on the generated point sets, and compare to optimal configurations on the sphere. We also compare the incremental point sets configurations to the optimal configurations. As a measure of the uniformity of a set of directions  $\mathcal{X} = \{\mathbf{u}_k, k \in \mathcal{K}\}$ ,

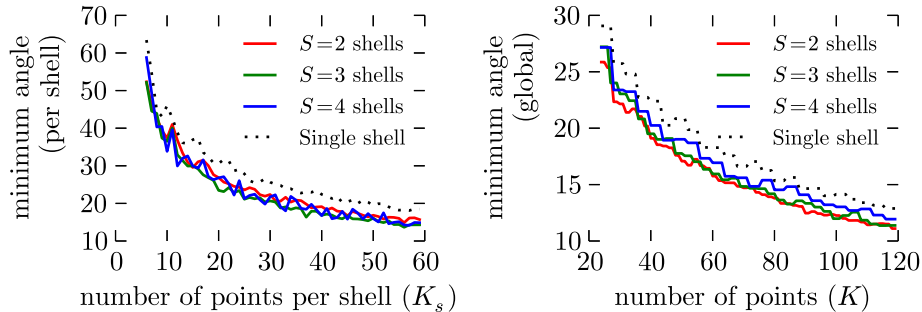


Figure 4: Minimum angular distance ( $^\circ$ ) between any two points (left) within the same shell and (right) globally. We compare the sets generated using generalized electrostatic analogy, for  $S = 2$ , 3 and 4 shells, to the optimum electrostatic point sets in one shell.

we compute the minimum angular distance between any two points, defined as

$$d(\mathcal{X}) = \min_{i \neq j} \arccos(|\mathbf{u}_i \cdot \mathbf{u}_j|).$$

The larger  $d(\mathcal{X})$ , the more uniform is the set of directions  $\mathcal{X}$ . For reference, we compare to the minimum angular distance of the optimal electrostatic distribution with the same number of points.

We generated sampling protocols on  $S = 2$ , 3 and 4 shells, with the same number of points per shell. The total number of points ranges from  $K = 12$  to  $K = 240$ . We report on Fig. 4 (left) the minimum angular distance between any two points on the same shell. Similarly, we report the minimum angular distance between any two points of the whole set of points, on Fig. 4 (right). The minimum angular distance remains close to that of the optimal point sets with same number of points, which suggests that the method offers a very good compromise between uniformity per shell, and global uniformity. This means there is very little price to pay on the uniformity per shell, to get a globally angular uniform configuration. This validate our approach, which consists in optimizing both the angular distribution of the sampling protocol, and the distribution on each single shell.

We also evaluate the geometrical properties of incrementally constructed multi-shell point sets. We report on Fig. 5 the minimum angular distance between any two points, per shell and as a whole. We observe that, provided that enough measurements are considered, the values of the

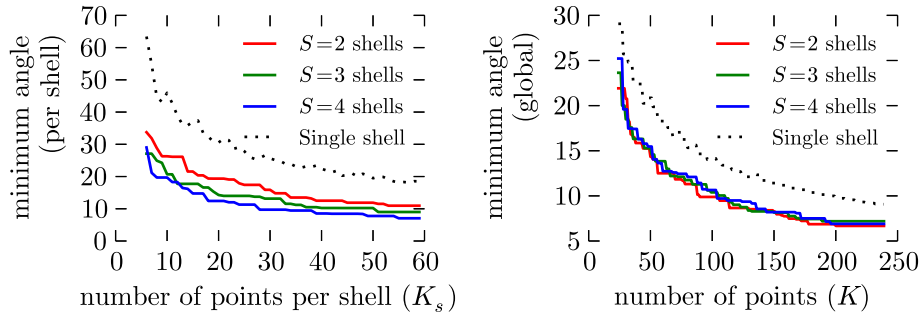


Figure 5: Geometrical properties of the incrementally constructed point sets on  $S$  shells. Minimum angular distance ( $^\circ$ ) between any two points (left) within the same shell and (right) globally. We compare the incremental sets generated using generalized electrostatic analogy, for  $S = 2, 3$  and  $4$  shells, to the optimum electrostatic point sets in one shell.

minimum angular distance are reasonably close to that of the optimal configuration on a single shell, for the same number of points.

Finally, we compare our method to three other state-of-the-art approaches that were briefly presented in the introduction, and aim at constructing acquisition designs on multiple shells with uniform angular coverage. The first method, called sparse and optimal acquisition (SOA) designs [25], starts from a uniform arrangement of  $K$  points on the unit sphere. Then it searches for the optimal partition of this set of points into  $S$  subsets (corresponding to  $S$  spheres), with  $K_s$  points on shell  $s$ , with respect to an objective function. We use the Java implementation provided in the HI-SPEED software, publicly available on the first author’s website. The second method [24] also starts from a set of  $K$  points uniformly spread on the unit sphere, though obtained with a different method [34]. Then it constructs  $S$  subsets which are nearly-optimal, minimizing electrostatic energy in a greedy fashion [35]. We will refer to this method as discrete greedy. The last method was presented in [26] and, in deeper details, in a private communication with the authors. This method starts from  $S$  independent sets of directions uniformly spread on the sphere, and then finds the optimal composition of rigid rotations of each set with respect to the others, so that the projection of the rotated sets of points onto the same unit spheres gives the most uniform coverage possible. We will

	Shell 1	Shell 2	Shell 3	global
	$K_1 = 28$	$K_2 = 28$	$K_3 = 28$	$K = 84$
SOA design [25]	15.9°	15.8°	16.7°	15.1°
discrete greedy [24]	14.5°	14.5°	14.5°	0.0°
solid rotation [26]	25.7°	25.7°	25.7°	7.4°
generalized electrostatic (this article)	22.2°	22.2°	22.0°	13.2°
Single shell (for reference) [16, 18]	25.7°	25.7°	25.7°	15.6°

Table 1: Minimum angular distance for a 3-shell design, with equal number of points per shell  $K_s = 28$ . On the last row, we also report the minimum angular distance of the optimal single shell point set with the same number of points (28 points for the first three rows, and 84 for the last row).

refer to this last method as solid rotation optimization. The optimization is done using simulated annealing, and implemented in Python<sup>TM</sup>, with the `anneal` routine from the SciPy optimization package [33]. The minimum angular distance per shell and globally are compared and reported in Table 1.

### Minimization of the cost function

As already stated above, the minimization of cost function  $V$  is a non-convex optimization problem, and we have no mathematical clue on the convergence of the optimization. We decided to test this point by repeating the optimization process, with random initial guess. The difference observed in the cost function at the end of the optimization is of the order of  $10^{-2}$ , which is negligible.

Another concern is about the computational cost of the minimization. While we cannot precisely measure the implementation of the SOA method [25], as the HI-SPEED software packages come with a GUI, we observed a time of several hours for the computation of a point set with 100 points on a modern desktop computer. Our method, the solid rotation method [26] and the discrete greedy method [24] give a result within minutes on the same hardware, and therefore are more attractive

from a computational perspective.

## Monte-Carlo simulations

We provide in this section an experimental validation of our sampling approach. We test the sampling schemes, and evaluate the angular resolution of generalized electrostatic, compared to the other, above mentioned approaches.

We simulated a single fiber by a cylinder with impermeable wall. The diffusion signal was simulated following [36]. The cylinder dimensions were set to  $L = 5$  mm, and  $\rho = 5$   $\mu\text{m}$ ; and the diffusion time is set to  $\tau = 20.8$  ms. The signal is simulated for different acquisitions schemes, with a maximum wavevector norm  $q_{\text{max}} = 60$   $\text{mm}^{-1}$ , which corresponds to a  $b$  value  $b_{\text{max}} = 3000$   $\text{s} \cdot \text{mm}^{-2}$ . The diffusion weighted signal was corrupted by Rician noise, with corresponding  $\text{SNR} = 25$  with respect to the baseline, non diffusion-weighted signal. This corresponds to a SNR range from 0.1 to 7.0 on the diffusion-weighted signal.

From these noisy measurements, we fit a diffusion tensor model, using the weighted linear least squares method [37]. This process is repeated 100 times for a given cylinder model, to get an estimate of the average angular error. To test the rotational invariance of acquisition schemes, this in turn is repeated 2000 times, for cylinders with different axis orientations. Acquisition protocols are defined on  $S = 3$  shells in  $q$ -space, where the shell radii  $q_1$ ,  $q_2$  and  $q_3$  are evenly distributed between  $q_{\text{min}}$  and  $q_{\text{max}}$ . The number of points per shell is the same on each shell  $K_s = 8$ , which corresponds to a total of  $K = 24$  measurements, typical in diffusion tensor imaging. For reference, we also compare to a single shell experiment with  $K = 24$  measurements,  $q = q_{\text{max}}$ . Results are reported on Fig. 6. and in Table 2.

We also compare the accuracy of multiple fiber detection and discrimination. The signal is now simulated using a mixture of 2 Gaussian distributions, with equal compartment size,

$$E(\mathbf{q}) = 0.5(\exp(-\mathbf{q}^T \mathbf{D}_1 \mathbf{q}) + \exp(-\mathbf{q}^T \mathbf{D}_2 \mathbf{q})). \quad (8)$$

The corresponding diffusion tensors  $\mathbf{D}_1$  and  $\mathbf{D}_2$  have a  $\text{FA} = 0.7$  and a mean diffusivity  $2.1 \cdot 10^{-3}$   $\text{m}^2 \cdot \text{s}^{-1}$ . This corresponds to classical values for the apparent diffusion tensor observed in brain white matter. We consider a  $60^\circ$  crossing angle. The signal is corrupted by Rician noise, with corresponding

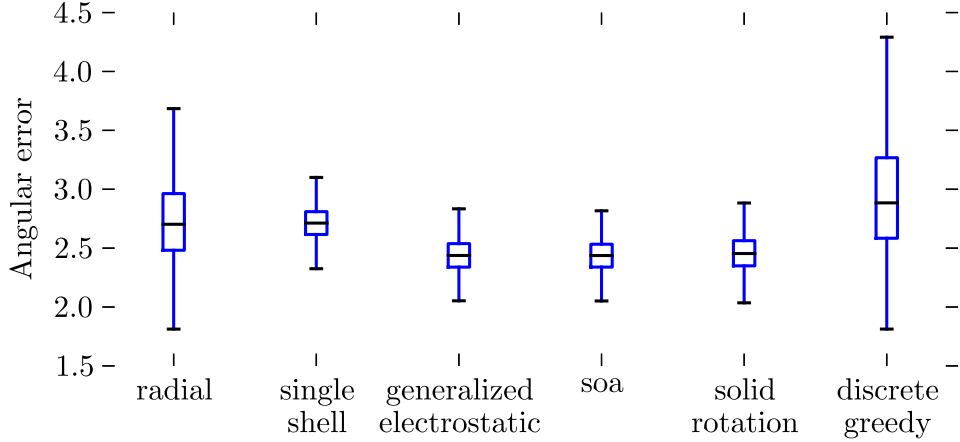


Figure 6: Average angular error between the principal direction of the estimated tensor and the axis of the cylinder. Signal simulation and reconstruction were repeated with 2000 different cylinder orientations following a random uniform distribution on the sphere, and 100 repetitions with random, Rician noise for each orientation. We plot here the median, first and third quartiles, and extremal values of the angular error (in degrees). The height of each boxplot represents how rotationally invariant each method performs.. See Table 2 for quantitative results.

	radial	single shell	generalized electrostatic	soa	solid rotation	discrete greedy
angular error	$2.70^\circ \pm 0.22$	$2.71^\circ \pm 0.09$	$2.44^\circ \pm 0.10$	$2.44^\circ \pm 0.10$	$2.47^\circ \pm 0.11$	$2.88^\circ \pm 0.34$

Table 2: Angular error between the principal direction of the estimated tensor and the axis of the cylinder. We report the median and angular deviation. See Fig. 6 for more details.

	radial	CSA	generalized	soa	solid	discrete
		ODF	electrostatic		rotation	greedy
estimated crossing	$58.5^\circ \pm 3.8$	$66.1^\circ \pm 2.6$	$61.5^\circ \pm 2.7$	$59.4^\circ \pm 4.0$	$59.2^\circ \pm 3.5$	$59.2^\circ \pm 3.7$

Table 3: Crossing angle for a reconstructed fiber crossing (ground truth is  $60^\circ$ ). See legend in Fig. 7 for more details.

SNR = 25 with respect to the baseline, non diffusion-weighted signal. This corresponds to a SNR range from 1.0 to 20.0 on the diffusion-weighted signal.

The signal is estimated in the continuous, modified spherical polar Fourier (mSPF) basis with Laplace regularization [23]. This is an orthonormal basis of continuous functions to represent the diffusion signal. The coefficients of the signal are estimated analytically, with a Laplace regularization penalty to promote smoothness. From the coefficients of the signal in this basis, the orientation distribution function (ODF) in constant solid angle is estimated analytically using the SPFI method in [38]. The angular and radial truncation orders were set to  $L = 6$  and  $N = 2$ , respectively. The maxima of the ODF are computed with a discrete search on a set of 10000 points on the sphere, leading to an accuracy of  $0.1^\circ$ .

We compare several acquisition protocols with  $K = 100$  points, and a maximum  $b$ -value of  $2500 \text{ s} \cdot \text{mm}^{-2}$ . For radial sampling, discrete greedy sampling [24] and solid rotation sampling [26], we use 4 shells with radii linearly spaced between  $q_{\min}$  and  $q_{\max}$ , and  $K_s = 25$  points per shell. For the SOA design, we use 10 shells, each with  $K_s = 10$  points per shell, as advocated in [25]. Finally, for the generalized electrostatic, we use the sampling strategy proposed in [22] and optimized for reconstruction in mSPF with radial truncation order  $N = 2$ . This corresponds to a design on  $S = 2$  shells, with  $b$ -values 900 and  $2500 \text{ s} \cdot \text{mm}^{-2}$ , and  $K_1 = 24$ ,  $k_2 = 76$  points per shell, respectively. Results of the reconstructed crossing angle are reported on Fig 7 and in Table 3. As for the previous experiments, the simulation was repeated 1000 times, with Rician noise and random rotation of the fibers to test the rotational invariance of the reconstruction.

While for the reconstruction of a single fiber, either method give comparable results, the recon-



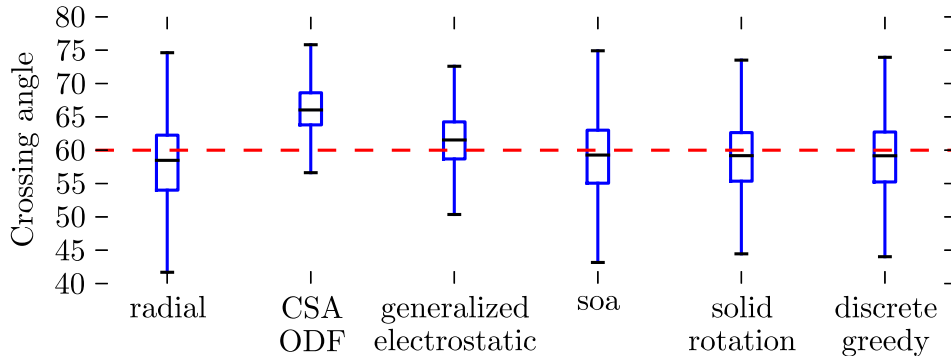


Figure 7: Crossing angle for a reconstructed fiber crossing. The  $q$ -space signal was reconstruction in the mSPF basis, with Laplace regularization (see [23]), fixed regularization weight  $\lambda = 0.5$ . The ODF was further estimated using the SPFI method in [38]. The boxplot represents min and max values, as well as the first and third quartiles. We also compare to the ODF reconstructed in constant solid angle [39], for a single shell experiment with the same number of points  $K = 100$ . See also Table 3.

struction with our method gives the lowest dispersion in angle estimation, and a very small bias, when it comes to multiple shell detection.

## Discussion

We have proposed a novel, efficient method to generate sampling schemes for multi-shell acquisitions. Our method is dedicated to the placement of acquisition directions on each sphere, with a good angular distribution per shell and as a whole. The cost function we propose is an extension of the electrostatic repulsion to multi-shell. With an adequate minimization algorithm, we show that this cost function can be used to create acquisition with incremental angular distribution, that is compatible with prematurely stopped scans.

The focus of the study is more on the angular distribution of points. As for the choice of number of shells, shell radii, number of points per shell, we suggest to follow the strategy optimized for reconstruction in mSPF, recently presented in [22].

The geometrical properties of the generated point sets are satisfactory: the angular distribution

per shell is indeed very close to the optimal arrangements in  $q$ -ball imaging. This is also the case for the angular distribution as a whole. The compromise between the global angular distribution and the angular distribution on each shell is better than for the other methods to which we compared: we are able to increase the global uniformity, at a very small cost on the uniformity on each shell. In simulations, for the reconstruction of single and multiple fiber compartments, this sampling strategies gives a better angular precision than prior arts methods. Single fiber orientation is determined with a lower angular error than simply radial sampling, and the crossing angle in two fibers case is also more accurate.

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