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► **To cite this version:**

Pavol Kocsis, Robert Fonod. Eigenstructure Decoupling in State Feedback Control Design. ATP Journal plus, HMM s.r.o., 2012, ATP Journal plus, 2, pp.34-39. <hal-00847146>

HAL Id: hal-00847146

<https://hal.inria.fr/hal-00847146>

Submitted on 22 Jul 2013

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Eigenstructure Decoupling in State Feedback Control Design

Pavol Kocsis and Róbert Fónod

Abstract

The presented design method aim is to synthesize a state feedback control law in such way that with respect to the prescribed eigenvalues of the closed-loop system matrix the corresponding eigenvectors are as close as possible to a decoupled system eigenvectors. It is demonstrated that some degree of freedom existing in the control design, representing by the parametric vectors set as well as by the set of closed-loop eigenvalues, can be properly used to meet some desired specification requirement. An illustrative example and the simulation results show that the proposed design principle is effective and simple.

Keywords: State feedback, eigenstructure assignment, mode decoupling, singular value decomposition, orthogonal complement.

Introduction

The static and the dynamic pole placement belongs to the prominent design problems of modern control theory, and, although its practical usefulness has been continuously in dispute, it is one of the most intensively investigated in control system design. It seems that the state-feedback pole assignment in control system design is one from the preferred techniques. In the single-input case the solution to this problem, when it exists, is unique. In the multi-input multi output (MIMO) case various solutions may exist [6], [10], and to obtain a specific solution some additional conditions have to be supplied in order to eliminate the extra degrees of freedom in design strategy.

In the last decade significant progress has been achieved in this field, coming in its formulation closest to the algebraic geometric nature of the pole placement problem [11], [17]. The reason for the discrepancy in opinions about the conditioning of the pole assignment problem is that one has to distinguish among three aspects of the pole placement problem, the computation of the memory-less feedback control law matrix gain, the computation of the closed loop system matrix eigenvalues spectrum and the suppressing of the cross-coupling effect [16], where one manipulated input variable cause change in more outputs variables.

Thus, eigenstructure assignment seems to be a powerful technique concerned with the placing of eigenvalues and their associated eigenvectors via feedback control laws, to meet closed-loop design specifications. The eigenvalues are the principal factors that govern the stability and the rates of decay or rise of the system dynamic response. The right and left eigenvectors, on the other hand, are dual factors that together determine the relative shape of the system dynamic response [9], [12], [15].

The general problem of assigning the system matrix eigenstructure using the state feedback control is considered in this paper. Based on the classic algebraic methods [3], [4], [14], as well as on the algorithms for pole assignment using Singular Value Decomposition (SVD) [5], [13] the exposition of the pole eigenstructure assignment problem is generalized here to handle the specified structure of the left eigenvector set in state feedback control design for MIMO linear

systems. Extra freedom, which makes dependent the closed-loop eigenvalues spectrum, is used for closed-loop state variables mode decoupling.

The integrated procedure provides a straightforward methodology usable in linear control system design techniques when the memory-free controller in the state-space control structures takes the standard form. Presented application for closed-loop state variables mode decoupling is relative simple and its worth can help to disclose the continuity between eigenstructure assignment and system variable dominant dynamic specification.

1. Problem Statement

Linear dynamic system with n degree of freedom can be modelled by the state-space equations

$$\dot{\mathbf{q}}(t) = \mathbf{A}\mathbf{q}(t) + \mathbf{B}\mathbf{u}(t) \quad (1)$$

$$\mathbf{y}(t) = \mathbf{C}\mathbf{q}(t) \quad (2)$$

where $\mathbf{q}(t) \in \mathbf{R}^n$, $\mathbf{u}(t) \in \mathbf{R}^r$ and $\mathbf{y}(t) \in \mathbf{R}^m$ are vectors of the state, input and measurable output variables, respectively, and the system matrix parameters $\mathbf{A} \in \mathbf{R}^{n \times n}$, $\mathbf{B} \in \mathbf{R}^{n \times r}$, and $\mathbf{C} \in \mathbf{R}^{m \times n}$ are constant and finite valued.

Generally, to the controllable time-invariant linear MIMO system (1) a linear state-feedback controller can be defined by a control policy

$$\mathbf{u}(t) = -\mathbf{K}\mathbf{q}(t) + \mathbf{L}\mathbf{w}(t) \quad (3)$$

$\mathbf{K} \in \mathbf{R}^{r \times n}$, $\mathbf{L} \in \mathbf{R}^{r \times m}$ to give rise to the closed-loop system description

$$\dot{\mathbf{q}}(t) = \mathbf{A}_c\mathbf{q}(t) + \mathbf{B}\mathbf{L}\mathbf{w}(t) \quad (4)$$

in such way that roots of the closed loop characteristic polynomial are eigenvalues of $\mathbf{A}_c = (\mathbf{A} - \mathbf{B}\mathbf{K})$, $\mathbf{A}_c \in \mathbf{R}^{n \times n}$.

Throughout the paper it is assumed that the pair (\mathbf{A}, \mathbf{B}) is controllable.

2. Basic Preliminaries

2.1 Orthogonal Complement

Definition 1. (Null space) Let $\mathbf{E}, \mathbf{E} \in \mathbf{R}^{h \times h}$, $\text{rank}(\mathbf{E}) = k < h$ be a rank deficient matrix. Then the null space $\mathcal{N}_{\mathbf{E}}$ of \mathbf{E} is the orthogonal complement of the row space of \mathbf{E} .

Proposition 1. Let $\mathbf{E}, \mathbf{E} \in \mathbf{R}^{h \times h}$, $\text{rank}(\mathbf{E}) = k < h$ be a rank deficient matrix. Then an orthogonal complement \mathbf{E}^{\perp} of \mathbf{E} is

$$\mathbf{E}^{\perp} = \mathbf{D}\mathbf{U}_2^T \quad (5)$$

where \mathbf{U}_2^T is the null space of \mathbf{E} and \mathbf{D} is an arbitrary matrix of appropriate dimension.

Proof. (see e.g. [8]) The SVD of $\mathbf{E}, \mathbf{E} \in \mathbf{R}^{h \times h}$, $\text{rank}(\mathbf{E}) = k < h$ gives

$$\mathbf{U}^T \mathbf{E} \mathbf{V} = \begin{bmatrix} \mathbf{U}_1^T \\ \mathbf{U}_2^T \end{bmatrix} \mathbf{E} \begin{bmatrix} \mathbf{V}_1 & \mathbf{V}_2 \end{bmatrix} = \begin{bmatrix} \Sigma_1 & \mathbf{0}_{12} \\ \mathbf{0}_{21} & \mathbf{0}_{22} \end{bmatrix} \quad (6)$$

where $\mathbf{U} \in \mathbf{R}^{h \times h}$ is the orthogonal matrix of the left singular vectors, $\mathbf{V} \in \mathbf{R}^{h \times h}$ is the orthogonal matrix of the right singular vectors of \mathbf{E} and $\Sigma_1 \in \mathbf{R}^{k \times k}$ is the diagonal positive definite matrix

$$\Sigma_1 = \text{diag}[\sigma_1 \cdots \sigma_k], \quad \sigma_1 \geq \cdots \geq \sigma_k > 0 \quad (7)$$

which diagonal elements are the singular values of \mathbf{E} . Using orthogonal properties of \mathbf{U} and \mathbf{V} , i.e. $\mathbf{U}^T \mathbf{U} = \mathbf{I}_h$, $\mathbf{V}^T \mathbf{V} = \mathbf{I}_h$, $\mathbf{U}_2^T \mathbf{U}_1 = \mathbf{0}$, then

$$\mathbf{E} = \mathbf{U} \Sigma \mathbf{V}^T = \begin{bmatrix} \mathbf{U}_1 & \mathbf{U}_2 \end{bmatrix} \begin{bmatrix} \Sigma_1 & \mathbf{0}_{12} \\ \mathbf{0}_{21} & \mathbf{0}_{22} \end{bmatrix} \begin{bmatrix} \mathbf{V}_1^T \\ \mathbf{V}_2^T \end{bmatrix} = \quad (8)$$

$$= \begin{bmatrix} \mathbf{U}_1 & \mathbf{U}_2 \end{bmatrix} \begin{bmatrix} \mathbf{S}_1 \\ \mathbf{0}_2 \end{bmatrix} = \mathbf{U}_1 \mathbf{S}_1$$

where $\mathbf{S}_1 = \Sigma_1 \mathbf{V}_1^T$. Thus (8) implies

$$\mathbf{U}_2^T \mathbf{E} = \mathbf{U}_2^T \begin{bmatrix} \mathbf{U}_1 & \mathbf{U}_2 \end{bmatrix} \begin{bmatrix} \mathbf{S}_1 \\ \mathbf{0}_2 \end{bmatrix} = \mathbf{0} \quad (9)$$

It is evident that for an arbitrary matrix \mathbf{D} is

$$\mathbf{D}\mathbf{U}_2^T \mathbf{E} = \mathbf{E}^{\perp} \mathbf{E} = \mathbf{0} \quad (10)$$

respectively, which implies (5). ■

2.2 System Model Canonical Form

Proposition 2. If $\text{rank}(\mathbf{CB}) = m$ then there exists a coordinates change in which $(\mathbf{A}^{\circ}, \mathbf{B}^{\circ}, \mathbf{C}^{\circ})$ takes the structure

$$\mathbf{A}^{\circ} = \begin{bmatrix} \mathbf{A}_{11}^{\circ} & \mathbf{A}_{12}^{\circ} \\ \mathbf{A}_{21}^{\circ} & \mathbf{A}_{22}^{\circ} \end{bmatrix}, \quad \mathbf{B}^{\circ} = \begin{bmatrix} \mathbf{0} \\ \mathbf{B}_2^{\circ} \end{bmatrix}, \quad \mathbf{C}^{\circ} = [\mathbf{0} \quad \mathbf{I}_m] \quad (11)$$

where $\mathbf{A}_{11}^{\circ} \in \mathbf{R}^{(n-m) \times (n-m)}$, $\mathbf{B}_2^{\circ} \in \mathbf{R}^{m \times m}$ is a non-singular matrix, and $\mathbf{I}_m \in \mathbf{R}^{m \times m}$ is identity matrix.

Proof. (see e.g. [7]) Considering the state-space description of the system (1), (2) with $r = m$ and defining the transform matrix \mathbf{T}_1^{-1} such that

$$\mathbf{C}_1 = \mathbf{C}\mathbf{T}_1 = [\mathbf{0} \quad \mathbf{I}_m], \quad \mathbf{T}_1^{-1} = \begin{bmatrix} \mathbf{I}_{n-m} & \mathbf{0} \\ \mathbf{0} & \mathbf{C} \end{bmatrix} \quad (12)$$

then

$$\mathbf{B}_1 = \mathbf{T}_1^{-1} \mathbf{B} = \mathbf{T}_1^{-1} \begin{bmatrix} \mathbf{B}_1 \\ \mathbf{B}_2 \end{bmatrix} = \begin{bmatrix} \mathbf{B}_1 \\ \mathbf{CB} \end{bmatrix} = \begin{bmatrix} \mathbf{B}_{11} \\ \mathbf{B}_{12} \end{bmatrix} \quad (13)$$

If $\mathbf{CB} = \mathbf{B}_{12}$ is a regular matrix (in opposite case the pseudo inverse of \mathbf{B}_{12} is possible to use), then the second transform matrix \mathbf{T}_2^{-1} can be defined as follows

$$\mathbf{T}_2^{-1} = \begin{bmatrix} \mathbf{I}_{n-m} & -\mathbf{B}_{11} \mathbf{B}_{12}^{-1} \\ \mathbf{0} & \mathbf{I}_m \end{bmatrix} \quad (14)$$

$$\mathbf{T}_2 = \begin{bmatrix} \mathbf{I}_{n-m} & \mathbf{B}_{11} \mathbf{B}_{12}^{-1} \\ \mathbf{0} & \mathbf{I}_m \end{bmatrix} \quad (15)$$

This application results in

$$\mathbf{B}^{\circ} = \mathbf{T}_2^{-1} \mathbf{B}_1 = \begin{bmatrix} \mathbf{0} \\ \mathbf{B}_2^{\circ} \end{bmatrix} = \mathbf{T}_2^{-1} \mathbf{T}_1^{-1} \mathbf{B} = \mathbf{T}_c^{-1} \mathbf{B} \quad (16)$$

where

$$\mathbf{B}_{11} = \mathbf{B}_1, \quad \mathbf{B}_2^{\circ} = \mathbf{B}_{12} = \mathbf{CB}, \quad \mathbf{T}_c^{-1} = \mathbf{T}_1^{-1} \mathbf{T}_2^{-1} \quad (17)$$

and analogously

$$\mathbf{C}^{\circ} = \mathbf{C}_1 \mathbf{T}_2 = \mathbf{C} \mathbf{T}_c = [\mathbf{0} \quad \mathbf{I}_m] \mathbf{T}_2 = [\mathbf{0} \quad \mathbf{I}_m] \quad (18)$$

Finally, it yields

$$\mathbf{A}^{\circ} = \mathbf{T}_c^{-1} \mathbf{A} \mathbf{T}_c = \mathbf{T}_2^{-1} \mathbf{T}_1^{-1} \mathbf{A} \mathbf{T}_1 \mathbf{T}_2 \quad (19)$$

Thus, (16), (18), and (19) implies (11). This concludes the proof. ■

Note, the structure of \mathbf{T}_1^{-1} is not unique and others can be obtained by permutations of the first $n-m$ rows in the structure defined in (12).

2.3 System Modes Properties

Proposition 3. Given system eigenstructure with distinct eigenvalues then for $j, k \in \{1, 2, \dots, n\}$, $l \in \{1, 2, \dots, m\}$, $m = r$

i. the k -th mode $(s - s_k)$ is unobservable from the l -th system output if the l -th row of matrix \mathbf{C} is orthogonal to the k -th eigenvector of the closed-loop system matrix \mathbf{A}_c , i.e. with $j \neq k$

$$\mathbf{c}_l^T \mathbf{n}_k = \mathbf{n}_j^T \mathbf{n}_k = 0, \quad \mathbf{C}^T = [\mathbf{c}_1 \cdots \mathbf{c}_m] \quad (20)$$

ii. the k -th mode $(s - s_k)$ is uncontrollable from the l -th column of matrix \mathbf{B} is orthogonal to the k -th eigenvector of the closed-loop system matrix \mathbf{A}_c , i.e. with $j \neq k$

$$\mathbf{n}_k^T \mathbf{b}_l = \mathbf{n}_k^T \mathbf{n}_j = 0, \quad \mathbf{B} = [\mathbf{b}_1 \cdots \mathbf{b}_r] \quad (21)$$

Proof. (see e.g. [13]) Let \mathbf{n}_k is the k -th right eigenvector corresponding to the eigenvalue s_k , i.e.

$$\mathbf{A}_c \mathbf{n}_k = (\mathbf{A} - \mathbf{BK}) \mathbf{n}_k = s_k \mathbf{n}_k \quad (22)$$

By definition, the closed-loop system resolvent kernel is

$$\mathbf{Y} = (s\mathbf{I}_n - \mathbf{A}_c)^{-1} \quad (23)$$

If the closed-loop system matrix is with distinct eigenvalues, (22) can be written in the compact form

$$\mathbf{A}_c [\mathbf{n}_1 \cdots \mathbf{n}_n] = [\mathbf{n}_1 \cdots \mathbf{n}_n] \begin{bmatrix} s_1 & & \\ & \ddots & \\ & & s_n \end{bmatrix} \quad (24)$$

$$\mathbf{A}_c \mathbf{N} = \mathbf{N} \mathbf{S}, \quad \mathbf{N}^{-1} = \mathbf{N}^T \quad (25)$$

respectively, where

$$\mathbf{S} = \text{diag}[s_1 \cdots s_n], \quad \mathbf{N} = [\mathbf{n}_1 \cdots \mathbf{n}_n] \quad (26)$$

Using the orthogonal property given in (25), the resolvent kernel of the system takes the next form

$$\mathbf{Y} = (s\mathbf{N}\mathbf{N}^{-1} - \mathbf{N}\mathbf{S}\mathbf{N}^{-1})^{-1} = \mathbf{N}(s\mathbf{I} - \mathbf{S})^{-1}\mathbf{N}^T \quad (27)$$

$$\mathbf{Y} = [\mathbf{n}_1 \cdots \mathbf{n}_n] \begin{bmatrix} s_1 & & \\ & \ddots & \\ & & s_n \end{bmatrix}^{-1} \begin{bmatrix} \mathbf{n}_1^T \\ \vdots \\ \mathbf{n}_n^T \end{bmatrix} \quad (28)$$

$$\mathbf{Y} = \sum_{h=1}^n \frac{\mathbf{n}_h \mathbf{n}_h^T}{s - s_h} \quad (29)$$

respectively. Thus, the closed loop transfer functions matrix takes form

$$\mathbf{G}(s) = \mathbf{C}(s\mathbf{I} - \mathbf{A}_c)^{-1}\mathbf{B}\mathbf{L} = \sum_{h=1}^n \frac{\mathbf{C}\mathbf{n}_h \mathbf{n}_h^T \mathbf{B}}{s - s_h} \mathbf{L} \quad (30)$$

It is obvious that (30) implies (20), (21). This concludes the proof. ■

3. Eigenstructure Assignment

In the pole assignment problem, a feedback gain matrix \mathbf{K} is sought so that the closed-loop system has a prescribed eigenvalues spectrum $\Omega(\mathbf{A}_c) = \{s_h : \Re(s_h) < 0, h = 1, 2, \dots, n\}$. Note, the spectrum $\Omega(\mathbf{A}_c)$ is closed under complex conjugation, and the observability and controllability of modes is determined by the closed-loop eigenstructure.

Considering the same assumptions as above then (22) can be rewritten as

$$[s_h \mathbf{I} - \mathbf{AB}] \begin{bmatrix} \mathbf{n}_h \\ \mathbf{K}\mathbf{n}_h \end{bmatrix} = \mathbf{L}_h \begin{bmatrix} \mathbf{n}_h \\ \mathbf{K}\mathbf{n}_h \end{bmatrix} = \mathbf{0} \quad (31)$$

where $\mathbf{L}_h \in \mathbf{R}^{n \times (n+r)}$,

$$\mathbf{L}_h = [s_h \mathbf{I} - \mathbf{AB}] \quad (32)$$

Subsequently, the singular value decomposition (SVD) of \mathbf{L}_h gives

$$\begin{bmatrix} \mathbf{u}_{h1}^T \\ \vdots \\ \mathbf{u}_{hn}^T \end{bmatrix} \mathbf{L}_h [\mathbf{v}_{h1} \cdots \mathbf{v}_{hm} \quad \mathbf{v}_{h,(n+1)} \cdots \mathbf{v}_{h,(n+r)}] = \quad (33)$$

$$= \begin{bmatrix} \sigma_{h1} & & & & \\ & \ddots & & & \\ & & \mathbf{0}_{n+1} & \cdots & \mathbf{0}_{n+r} \\ & & & \sigma_{hm} & \\ & & & & \end{bmatrix}$$

where $\{\mathbf{u}_{hl}^T, l = 1, 2, \dots, n\}, \{\mathbf{v}_{hk}, k = 1, 2, \dots, n+r\}$ are sets of the left and right singular vectors of \mathbf{L}_h associated with the set of singular values $\{\sigma_{hl}, l = 1, 2, \dots, n\}$.

It is evident that vectors $\{\mathbf{v}_{hj}, j = n+1, n+2, \dots, n+r\}$ satisfy (31), i.e.

$$\mathbf{L}_h \mathbf{v}_{hj} = [s_h \mathbf{I} - \mathbf{AB}] \mathbf{v}_{hj} = \mathbf{0} \quad (34)$$

The set of vectors $\{\mathbf{v}_{hj}, j = n+1, n+2, \dots, n+r\}$ is a non-trivial solution of (32), and results the null space of $\mathbf{L}_h, h = 1, 2, \dots, n$

$$\begin{bmatrix} \mathbf{n}_h \\ \mathbf{K}\mathbf{n}_h \end{bmatrix} \in \mathcal{N}[s_h \mathbf{I} - \mathbf{AB}] = \mathbf{0} \quad (35)$$

The null space (35) consists of the normalized orthogonal set of vectors. Any combination of these vectors (the span of null space) will provide a vector \mathbf{n}_h which used as an eigenvector produces the desired eigenvalue s_h in the closed-loop system matrix.

Proposition 4. The canonical form eigenstructure optimization provides optimal eigenstructure also for that model from which the canonical form was derived.

Proof. Using (16), (18), (19) and (22) it can be simply written

$$(\mathbf{A} - \mathbf{BK}) \mathbf{n}_k = (\mathbf{T}_c \mathbf{A}^\circ \mathbf{T}_c^{-1} - \mathbf{T}_c \mathbf{B}^\circ \mathbf{K}^T \mathbf{T}_c^{-1}) \mathbf{n}_k = \mathbf{T}_c (\mathbf{A}^\circ - \mathbf{B}^\circ \mathbf{K}^\circ) \mathbf{T}_c^{-1} \mathbf{n}_k = s_h \mathbf{n}_k \quad (36)$$

$$(\mathbf{A}^\circ - \mathbf{B}^\circ \mathbf{K}^\circ) \mathbf{T}_c^{-1} \mathbf{n}_k = s_h \mathbf{T}_c^{-1} \mathbf{n}_k \quad (37)$$

$$(\mathbf{A}^\circ - \mathbf{B}^\circ \mathbf{K}^\circ) \mathbf{n}_k^\circ = \mathbf{A}_c^\circ \mathbf{n}_k^\circ = s_h \mathbf{n}_k^\circ \quad (38)$$

respectively, where $\mathbf{K}^\circ = \mathbf{K}^T \mathbf{T}_c, \mathbf{n}_k = \mathbf{T}_c \mathbf{n}_k^\circ$.

Writing compactly the set $\{\mathbf{n}_h = \mathbf{T}_c \mathbf{n}_h^\circ, h = 1, 2, \dots, n\}$ as follows

$$\mathbf{N} = \mathbf{T}_c \mathbf{N}^\circ, \quad \mathbf{N}^{-1} = \mathbf{N}^{\circ T} \mathbf{T}_c^{-1} \quad (39)$$

then using (27), (30), (39) it yields

$$\begin{aligned} \mathbf{G}(s) &= \mathbf{C}\mathbf{Y}\mathbf{B}\mathbf{L} = \mathbf{C}\mathbf{N}(s\mathbf{I} - \mathbf{S})^{-1}\mathbf{N}^{-1}\mathbf{B}\mathbf{L} = \\ &= \mathbf{C}\mathbf{T}_c \mathbf{N}^\circ (s\mathbf{I} - \mathbf{S})^{-1} \mathbf{N}^{\circ T} \mathbf{T}_c^{-1} \mathbf{B}\mathbf{L} = \\ &= \mathbf{C}^\circ \mathbf{N}^\circ (s\mathbf{I} - \mathbf{S})^{-1} \mathbf{N}^{\circ T} \mathbf{B}^\circ \mathbf{L} \end{aligned} \quad (40)$$

$$\mathbf{G}(s) = \mathbf{C}(s\mathbf{I} - \mathbf{A}_c)^{-1}\mathbf{B}\mathbf{L} = \mathbf{C}^\circ (s\mathbf{I} - \mathbf{A}_c^\circ)^{-1} \mathbf{B}^\circ \mathbf{L} \quad (41)$$

respectively, and evidently

$$\mathbf{G}(s) = \sum_{h=1}^n \frac{\mathbf{C}\mathbf{n}_h \mathbf{n}_h^T \mathbf{B}}{s - s_h} \mathbf{L} = \sum_{h=1}^n \frac{\mathbf{C}^\circ \mathbf{n}_h^\circ \mathbf{n}_h^{\circ T} \mathbf{B}^\circ}{s - s_h} \mathbf{L} \quad (42)$$

It is obvious that optimizing product $\mathbf{C}^\circ \mathbf{n}_h^\circ$ then it is optimized also $\mathbf{C}\mathbf{n}_h$. This concludes the proof. ■

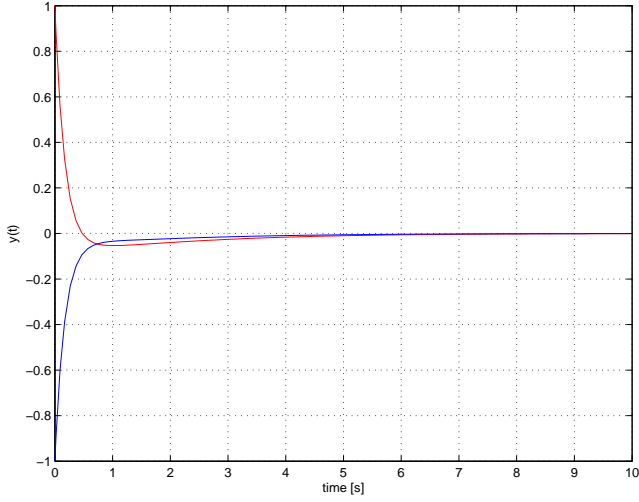


Fig. 1 System output response

4. Parameter Design

Using eigenvector orthogonal properties, (22) can be rewritten for $h=1, 2, \dots, n$ as follows

$$(s_h \mathbf{I} - \mathbf{A}^\circ) \mathbf{n}_h^\circ = -\mathbf{B}^\circ \mathbf{K}^\circ \mathbf{n}_h^\circ = -\mathbf{B}^\circ \mathbf{r}_h^\circ \quad (43)$$

$$\mathbf{n}_h^\circ = -(s_h \mathbf{I} - \mathbf{A}^\circ)^{-1} \mathbf{B}^\circ \mathbf{r}_h^\circ = \mathbf{V}_h^{\circ*} \mathbf{r}_h^\circ \quad (44)$$

respectively, where

$$\mathbf{r}_h^\circ = \mathbf{K}^\circ \mathbf{n}_h^\circ, \quad \mathbf{V}_h^{\circ*} = -(s_h \mathbf{I} - \mathbf{A}^\circ)^{-1} \mathbf{B}^\circ \quad (45)$$

Subsequently, it can be obtained

$$\mathbf{r}_h^\circ = \mathbf{V}_h^{\circ\dagger} \mathbf{n}_h^\circ \quad (46)$$

where

$$\mathbf{V}_h^{\circ\dagger} = (\mathbf{V}_h^{\circ*T} \mathbf{V}_h^{\circ*})^{-1} \mathbf{V}_h^{\circ*T} \quad (47)$$

is Moore-Penrose pseudo inverse of $\mathbf{V}_h^{\circ*}$.

Of interest are the eigenvectors of the closed-loop system having minimal orthogonal projection to rows of the orthogonal complement $\mathbf{C}^{\circ T \perp}$ of the output matrix $\mathbf{C}^{\circ T}$ and associated with m element eigenvalues subset $\rho(\mathbf{A}^\circ)$ ($m = \text{rank}(\mathbf{C}^\circ)$, $\rho(\mathbf{A}^\circ) \subset \Omega(\mathbf{A}^\circ)$) of the desired closed-loop eigenvalues set $\Omega(\mathbf{A}^\circ) = \{s_h, \Re(s_h) < 0, h=1, 2, \dots, n\}$ $\Omega(\mathbf{A}^\circ) = \Omega(\mathbf{A})$. The rest $(n-m)$ eigenvalues can be associated with rows of the complement matrix \mathbf{C}^\bullet obtained in such way that all zero elements in \mathbf{C}° be changed to ones, and all ones to zeros. Note, direct use of \mathbf{C}° maximize matrix weights of modes.

Let $\rho(\mathbf{A}^\circ) = \{s_h, \Re(s_h) < 0, h=1, 2, \dots, n\}$, then

$$\mathbf{r}_h^* = \mathbf{V}_h^{\circ\dagger} \mathbf{c}_h^{\circ T \perp T}, \quad h=1, 2, \dots, m \quad (48)$$

$$\mathbf{r}_h^\bullet = \mathbf{V}_h^{\circ\dagger} \mathbf{c}_h^{\bullet T}, \quad h=m+1, \dots, n \quad (49)$$

Thus, computing

$$\mathbf{n}_h^* = \mathbf{V}_h^{\circ*} \mathbf{r}_h^*, \quad \mathbf{n}_h^\bullet = \mathbf{V}_h^{\circ*} \mathbf{r}_h^\bullet \quad (50)$$

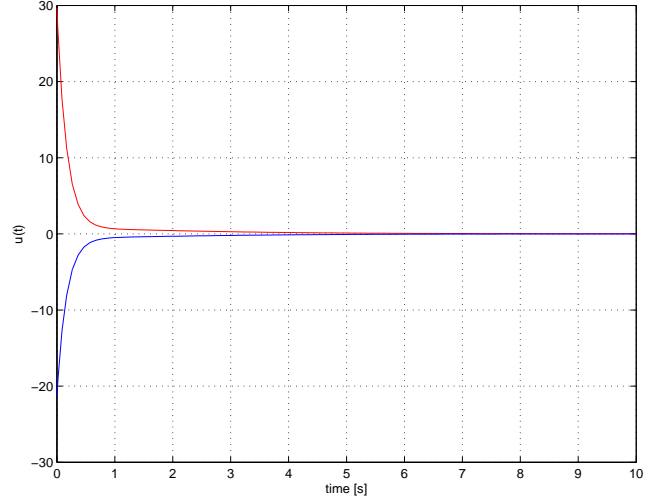


Fig. 2 Control actions

it is possible to construct and to separate the matrix \mathbf{Q}° of the form

$$\mathbf{Q}^\circ = [\mathbf{v}_1^* \quad \dots \quad \mathbf{v}_m^* \quad \mathbf{v}_{m+1}^\bullet \quad \dots \quad \mathbf{v}_n^\bullet] = \begin{bmatrix} \mathbf{P}^\circ \\ \mathbf{R}^\circ \end{bmatrix} \quad (51)$$

with $\mathbf{P}^\circ \in \mathbf{R}^{n \times n}$, $\mathbf{R}^\circ \in \mathbf{R}^{r \times n}$ such that

$$\mathbf{K} = \mathbf{R}^\circ \mathbf{P}^{\circ-1}, \quad \mathbf{K} = \mathbf{K}^\circ \mathbf{T}_c^{-1} \quad (52)$$

4. Illustrative Example

The system under consideration was described by (1), (2), where

$$\mathbf{A} = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -5 & -9 & -5 \end{bmatrix}, \quad \mathbf{B} = \begin{bmatrix} 1 & 3 \\ 2 & 1 \\ 2 & 5 \end{bmatrix}, \quad \mathbf{C}^T = \begin{bmatrix} 1 & 1 \\ 2 & 1 \\ 1 & 0 \end{bmatrix}$$

Constructing the transformation matrices

$$\mathbf{T}_c^{-1} = \begin{bmatrix} 4.0 & 0.5 & -2.5 \\ 1.0 & 2.0 & 1.0 \\ 1.0 & 1.0 & 0.0 \end{bmatrix}, \quad \mathbf{T}_c = \begin{bmatrix} 1.0 & 2.5 & -5.5 \\ -1.0 & -2.5 & 6.5 \\ 1.0 & 3.5 & -7.5 \end{bmatrix}$$

the system model canonical form parameters were computed as

$$\mathbf{A}^\circ = \begin{bmatrix} -1 & 10.5 & 6 \\ 0 & -3.0 & -2 \\ 0 & 1.0 & -1 \end{bmatrix}, \quad \mathbf{B}^\circ = \begin{bmatrix} 0 & 0 \\ 7 & 10 \\ 3 & 4 \end{bmatrix}, \quad \mathbf{C}^\circ = [\mathbf{0} \quad \mathbf{I}_2]$$

Thus, considering $\Omega(\mathbf{A}^\circ) = \{-0.5, -1.2, -6\}$ it is

$$\mathbf{V}_1^\circ = \begin{bmatrix} -37.3846 & -54.4615 \\ 0.7692 & 0.9231 \\ -4.4615 & -6.1538 \end{bmatrix}$$

$$\mathbf{V}_2^\circ = \begin{bmatrix} -10.0610 & -5.4815 \\ 4.5122 & 6.0976 \\ -7.5610 & -10.4878 \end{bmatrix}$$

$$\mathbf{V}_3^\circ = \begin{bmatrix} -5.2059 & -7.3059 \\ 2.4118 & 3.4118 \\ 0.1176 & 0.0176 \end{bmatrix}$$

and with $\mathbf{c}^{\circ T \perp} = [1 \ 0 \ 0]$, $\mathbf{c}_1^{\circ T} = [1 \ 0 \ 1]$ it yields

$$\mathbf{r}_1^{\circ} = \begin{bmatrix} 0.3891 \\ -0.2854 \end{bmatrix}, \quad \mathbf{r}_2^{\circ} = \begin{bmatrix} -0.1645 \\ 0.1194 \end{bmatrix}, \quad \mathbf{r}_3^{\circ} = \begin{bmatrix} 18.4978 \\ -13.2737 \end{bmatrix}$$

$$\mathbf{n}_1^{\circ T} = [0.9983 \ 0.0358 \ 0.0205]$$

$$\mathbf{n}_2^{\circ T} = [0.9997 \ -0.0144 \ -0.0082]$$

$$\mathbf{n}_3^{\circ T} = [0.9983 \ 0.0358 \ 0.0205]$$

Constructing the matrix \mathbf{Q}°

$$\mathbf{Q}^{\circ} = \begin{bmatrix} 0.9983 & 0.9997 & 0.6788 \\ 0.0358 & 0.0144 & -0.6745 \\ 0.0205 & -0.0082 & 0.6146 \\ 0.3891 & -0.1645 & 18.4978 \\ -0.2854 & 0.1194 & -13.2737 \end{bmatrix} = \begin{bmatrix} \mathbf{P}^{\circ} \\ \mathbf{R}^{\circ} \end{bmatrix}$$

the control law parameters satisfying (52) are

$$\mathbf{K}^{\circ} = \begin{bmatrix} -0.0062 & -3.7944 & 25.9402 \\ 0.0036 & 2.6301 & -18.7151 \end{bmatrix}$$

$$\mathbf{K} = \begin{bmatrix} 22.1212 & 18.3483 & -3.7990 \\ -16.0707 & -13.4532 & 2.6211 \end{bmatrix}$$

It is possible to verify that closed-loop system matrix eigenvalues belongs to the desired one.

In the presented Fig. 1, 2 the example is shown of the unforced closed-loop system output response, as well as control actions, where nonzero initial state was considered.

	$\mathbf{c}_1^{\circ T} \leftarrow -0.5$	$\mathbf{c}_1^{\circ T} \leftarrow -1.2$	$\mathbf{c}_1^{\circ T} \leftarrow -6$
$\ \mathbf{k}^{\circ}\ $	17.2524	15.9878	32.3181
$\ \mathbf{k}\ $	46.2521	43.7478	35.8664
ISE	1.8746	0.8183	0.1712
IAE	3.7033	1.6238	0.5651
ITAE	7.0822	1.8607	0.7077

Tab.1 Comparison of performance indicators for different combination of eigenvalue assignment

Concluding remarks

This paper provides a design method for memory-free controllers where the general problem of assigning the eigenstructure for state variable mode decoupling in state feedback control design is considered. The method exploits standard numerical optimization procedures to manipulate the system feedback gain matrix as a direct design variable. The manipulation is accomplished in a manner that produces desired system global performance by pole placement and output dynamics by modification of the mode observability.

With generalization of the known algorithms for pole assignment the modified exposition of the problem is presented here to handle the optimized structure of the left eigenvector set in state feedback control design. Presented method makes full use of the freedom provided by eigenstructure assignment to find a controller which stabilizes the closed-loop system. Therefore, the feedback control law has a clear physical meaning and provides a valid design me-

thod of the controller for real systems. It is shown by appropriately assigning closed-loop eigenstructure in state feedback control the overall stability is achieved. Finally the design methodology is illustrated by an example.

Acknowledgment

The work presented in this paper was supported by VEGA, Grant Agency of Ministry of Education and Academy of Science of Slovak Republic under Grant No. 1/0256/11, as well by Research & Development Operational Programme Grant No. 26220120030 realized in Development of Centre of Information and Communication Technologies for Knowledge Systems. These supports are very gratefully acknowledged.

References

- [1] BACHELIER, O., BOSCHE, J., and MEHDI, D.: On pole placement via eigenstructure assignment Approach, *IEEE Transactions on Automatic Control*, 51:9, 1554-1558, 2006.
- [2] BURNS, R.S.: *Advanced Control Engineering*, Butterworth-Heinemann, Oxford, 2001.
- [3] DATTA, B.N.: *Numerical Methods for Linear Control Systems: Design and Analysis*, Elsevier, London, 2004.
- [4] GOLUB, G.H. and LOAN Van C.F.: *Matrix Computations*, The John Hopkins University Press, Baltimore, 1989.
- [5] FILASOVÁ, A.: Robust control design for large-scale uncertain dynamic system, In *New Trends in Design of Control Systems*, STU, Bratislava, 247-432, 1997.
- [6] FILASOVÁ, A.: Robust control design: An optimal control approach, In *Proceeding of the IEEE International Conference on Intelligent Engineering Systems INES'99*, Stará Lesná, Slovakia, 515-518, 1999.
- [7] FILASOVÁ, A. and KROKAVEC, D.: On sensor faults estimation using sliding mode observers, In *Conference on Control and Fault-Tolerant Systems SysTol'10*, Nice, France, 2010, 44-49.
- [8] FILASOVÁ, A. and KROKAVEC, D.: State estimate based control design using the unified algebraic approach, *Archives of Control Sciences*, 20:1, 5-18, 2010.
- [9] FÓNOD, R. and KOCSIS, P.: State feedback control design using eigenstructure decoupling, In *Proceeding of the 18th International Conference on Process Control PC'11*, Tatranská Lomnica, Slovakia, 268-272, 2011.
- [10] IPSEN, I.C.S.: *Numerical Matrix Analysis. Linear Systems and Least Squares*, SIAM, Philadelphia, 2009.
- [11] KAUTSKY, J., NICHOLS, N. and DOOREN Van, P.: Robust pole assignment in linear state feedback, *International Journal of Control*, 41:5, 1129-1155, 1985.
- [12] KOCSIS, P. and KROKAVEC, D.: State variables mode decoupling in state control design for linear MIMO systems, In *International Conference Cybernetics and Informatics 2009*, Ždiar, Slovak Republic, 44.1-44.8, 2009.
- [13] KROKAVEC, D. and FILASOVÁ, A.: *Dynamic Systems Diagnosis*, Elfa, Košice, 2007. (in Slovak)
- [14] POZNYAK, A.S.: *Advanced Mathematical Tools for Automatic Control Engineers: Deterministic Techniques*, Elsevier, London 2008.
- [15] SOBEL, K.M. and LALLMAN, F.J.: Eigenstructure assignment for the control of highly augmented aircraft, *Jour-*

nal of Guidance, Control and Dynamics, 12:3, 318-324, 1989.

[16] WANG, Q.G.: *Decoupling Control*, Springer-Verlag, Berlin, 2003.

[17] WONHAM, W.M.: *Linear Multivariable Control: A Geometric Approach*, Springer-Verlag, New York, 1985.

[18] XU, X.H. and XIE, X.K.: Eigenstructure assignment by output feedback in descriptor systems, *IMA Journal of Mathematical Control and Information*, 12, 127-132, 1995.

Abstrakt

Cieľom návrhu je syntetizovať stavové riadenie tak, aby vzhľadom na predpísané vlastné hodnoty matice dynamiky uzavretého obvodu boli odpovedajúce vlastné vektory čo najviac podobné vlastným vektorom systému s rozviazaným vstupom a výstupom. V príspevku je ukázané, že existujúci stupeň voľnosti v návrhu, reprezentovaný množinou parametrických vektorov a množinou pólov uzavretého obvodu, možno využiť na dosiahnutie vopred zadaných charakteris-

tík uzavretého obvodu. Príklad a číselné simulácie ukazujú, že takýto spôsob návrhu je efektívny a jednoduchý.

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