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Abstract: The derivation of reduced MHD models for fusion plasma is here formulated as a special instance of the general theory of singular limit of hyperbolic system of PDEs with large operator. This formulation allows to use the general results of this theory and to prove rigorously that reduced MHD models are valid approximations of the full MHD equations. In particular, it is proven that the solutions of the full MHD system converge to the solutions of an appropriate reduced model.

Key-words: Asymptotic analysis, hyperbolic systems, singular limit, MHD, Fusion plasma, Tokamaks

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Théorie mathématique des modèles de MHD réduite pour les plasmas de fusion

Résumé : L'établissement de modèles de MHD réduite est formulé comme un exemple de la théorie générale des limites singulières des systèmes hyperboliques. Cette formulation permet d'utiliser les résultats généraux de cette théorie et de prouver rigoureusement que les modèles de MHD réduite sont une approximation valide du modèle complet. En particulier, la convergence des solutions du modèle complet vers les solutions d'un système réduit est démontrée.

Mots-clés : Analyse asymptotique, systèmes hyperboliques, limite singulière, MHD, Plasmas de fusion, Tokamaks

1 Introduction

Magnetohydrodynamics (MHD) is a macroscopic theory describing electrically conducting fluids. It addresses laboratory as well as astrophysical plasmas and therefore is extensively used in very different contexts. One of these contexts concerns the study of fusion plasmas in tokamak machines. A tokamak is a toroidal device in which hydrogen isotopes in the form of a plasma reaching a temperature of the order of the hundred of millions of Kelvins is confined thanks to a very strong applied magnetic field. Tokamaks are used to study controlled fusion and are considered as one of the most promising concepts to produce fusion energy in the near future. However a hot plasma as the one present in a tokamak is subject to a very large number of instabilities that can lead to the end of the existence of the plasma. An important goal of MHD studies in tokamaks is therefore to determine the stability domain that constraints the operational range of the machines. A secondary goal of these studies is to evaluate the consequences of these possible instabilities in term of heat loads and stresses on the plasma facing components of the machines. Numerical simulations using the MHD models are therefore of uttermost importance in this field and therefore the design of MHD models and of models beyond the standard one (e.g incorporating two-fluid or kinetic effects) is the subject of an intense activity.

However, the MHD model is a very complex one : it contains 8 independent variables, three velocity components, three components of the magnetic field, density and pressure. Although the system is hyperbolic, it is not strictly hyperbolic leading to the existence of possible resonance between waves of different types and moreover the MHD system has the additional complexity of being endowed with an involution. An involution in the sense of conservation law systems is an additional equation that if satisfied at $t = 0$ is satisfied for all $t > 0$ [5]. For all these reasons, approximations and simplified models have been designed both for theoretical studies as well as numerical ones. In the field of fusion plasmas, these models are denoted as *reduced MHD models*¹. These models initially proposed in the 70' [27]) have been progressively refined to include more and more physical effects and corrections [28, 3, 22, 12]. In particular, some earlier models conserve a non-standard energy and in some modeling works, special attention have been paid to insure the conservation of the usual energy e.g [29, 7, 17] (see also [8]). At present the literature on the physics of fusion plasma concerned by reduced MHD models is huge and contains several hundred of references. From a numerical point of view, several well-known numerical codes (e.g [21], [4]) used routinely for fusion plasma studies are based on these reduced models. Actually, while there is a definite tendency in the fusion plasma community to use full MHD models e.g [9], [13], [10], a large majority of non-linear simulations of tokamak plasmas have been and still are conducted with these approximations.

Until recently, reduced MHD models have not attracted a lot of interest in the mathematical or numerical analysis literature. One can cite [6] and [8] that have shown that these models can be interpreted as some special case of "Galerkin" methods where the velocity and magnetic fields are constrained to belong to some lower dimensional space. This interpretation is also implicit in the design of the M3D-C1 code [13] where instead of the usual projection on the coordinate system axis, the equations governing the scalar components of the vector fields are obtained by special projections that allow to recover reduced models.

In this work, we adopt the different point of view of asymptotic analysis and show that reduced MHD models can be understood as a special instance of the general theory of singular limit of hyperbolic system of PDEs with large constant operators. This formulation allows to use

¹while the standard MHD model is by contrast designated as the *full* MHD model

the general results of this theory and to prove rigorously the validity of these approximations of the MHD equations. In particular, it is proven here, we believe for the first time, that the solutions of the full MHD system converge to the solutions of an appropriate reduced model.

This paper is organized as follows : First, we recall the general theory of singular limits of quasi-linear hyperbolic system with a large parameter. In the third section, we show how this general framework can be used to analyze reduced MHD models. Finally, we conclude by some remarks on possible extensions of the present work.

2 Singular limit of hyperbolic PDEs

2.1 General framework

In this section, we are concerned with the behavior when $\varepsilon \rightarrow 0$ of the solutions of hyperbolic system of PDEs of the following form :

$$\begin{cases} A_0(\mathbf{W}, \varepsilon) \partial_t \mathbf{W} + \sum_j A_j(\mathbf{W}, \varepsilon) \partial_{x_j} \mathbf{W} + \frac{1}{\varepsilon} \sum_j C_j \partial_{x_j} \mathbf{W} = 0 \\ \mathbf{W}(0, \mathbf{x}, \varepsilon) = \mathbf{W}_0(\mathbf{x}, \varepsilon) \end{cases} \quad (1)$$

Here $\mathbf{W} \in \mathcal{S} \subset \mathbb{R}^N$ is a vector function depending of $(t, x_j; j = 1, \dots, d)$ where d is the space dimension while the A_0, A_j, C_j are square $N \times N$ matrices. Due to the presence of the large coefficient $1/\varepsilon$ multiplying the operator $\sum_j C_j \partial_{x_j}(\cdot)$, we may expect the velocity of some waves present in (1) to become infinite and therefore, for a solution to exist on a $\mathcal{O}(1)$ time scale, it has to be close in some sense to the kernel $K = \{\mathbf{W} \in \mathbb{R}^N \text{ s.t. } \sum_j C_j \partial_{x_j} \mathbf{W} = 0\}$ of the large operator. The limit system obtained from (1) is therefore a *singular* limit since the constraint $\mathbf{W} \in K$ may change the hyperbolic nature of the system (1). A prototypical example of this behavior is given by the incompressible limit of the *hyperbolic* equations governing compressible Euler flows where the propagation at infinite speed of the acoustic waves gives rise to an *elliptic* equation on the pressure coming from the global constraint $\nabla \cdot \mathbf{u} = 0$.

The nature of the singular limit depends on the initial data. Using the terminology of Schochet [25] the limit is called “slow” if the initial data makes the first time derivatives at time $t = 0$ stay bounded as $\varepsilon \rightarrow 0$. The term “well-prepared initial data” is also used to qualify this situation. In this case, under appropriate assumptions, the solutions exist for a time T independent of ε and converge to the solutions of a limit system when $\varepsilon \rightarrow 0$.

In the opposite case, denoted as a “fast” singular limit, $\partial_t \mathbf{W}$ is not $\mathcal{O}(1)$ at time zero and fast oscillations developing on a $1/\varepsilon$ time scale can persist on the long time scale. Solutions of fast singular limit cannot converge as $\varepsilon \rightarrow 0$ in the usual sense since the time derivative of the solution is of order $1/\varepsilon$. In this case, convergence means the existence of an “averaged” limit profile $\mathcal{W}(t, \tau, \mathbf{x})$ such that $\mathbf{W}(t, \mathbf{x}, \varepsilon) - \mathcal{W}(t, t/\varepsilon, \mathbf{x}) \rightarrow 0$ with ε . The question of the existence of fast singular limit is in particular examined in [25]. A review article summarizing results on this subject with a special emphasis on the low Mach number limit is [1].

In this work, we will be mainly concerned by the slow case. Even in this case, the existence for a time independent of ε and the convergence of the solutions to the solutions of a limit system may require additional assumptions on the structure of (1). Beginning with the earlier works in the 80’ of Klainerman and Majda [15, 14, 19] and those of Kreiss and his co-workers [16, 2], these questions have been examined in several works [23, 24] with the main objective to

justify the passage to the incompressible limit in low Mach number compressible flows. Several extensions of these works for viscous flows or general hyperbolic-parabolic systems are also available. Again we can refer to [1] for a review.

The following theorem (see [19], chapter 2) summarizes the main results of these works in a form suitable for our purposes :

Theorem 1 1. *Assume that :*

1. *Conditions on the initial data :* $W_0(\mathbf{x}, \varepsilon) = W_0^0(\mathbf{x}) + \varepsilon W_0^1(\mathbf{x}, \varepsilon)$

(a) $W_0^0(\mathbf{x})$ and $W_0^1(\mathbf{x}, \varepsilon)$ are in H^s

(b) $\sum_j C_j \partial_j W_0^0 = 0$

(c) $\|W_0^1(\mathbf{x}, \varepsilon)\|_s \leq C\varepsilon$

2. *Structure of the system*

(a) *The matrices A_0, A_j and C_j are symmetric*

(b) *A_0 is positive definite at least in a neighborhood of the initial data*

(c) *A_0 and A_j are C^s continuous for some $s \geq [n/2] + 2$, where n is the number of spatial dimensions*

(d) *The C_j are constant matrices*

(e) *The matrix $A_0(\mathbf{W}, \varepsilon) = A_0(\varepsilon \mathbf{W})$*

then the solution $\mathbf{W}(t, \mathbf{x}, \varepsilon)$ of system (1) with the initial data satisfying condition 1 is unique and exists for a time T independent of ε . In addition the solutions $\mathbf{W}(t, \mathbf{x}, \varepsilon)$ satisfy :

$$\|\mathbf{W}(t, \mathbf{x}, \varepsilon) - \mathbf{W}^0(t, \mathbf{x})\|_{s-1} \leq C\varepsilon \text{ for } t \in [0, T]$$

where $\mathbf{W}^0(t, \mathbf{x})$ is the solution of the reduced system :

$$\begin{cases} A_0(0) \partial_t \mathbf{W}^0 + \sum_j A_j(\mathbf{W}^0, 0) \partial_{x_j} \mathbf{W}^0 + \sum_j C_j \partial_{x_j} \mathbf{W}^1 = 0 \\ \sum_j C_j \partial_{x_j} \mathbf{W}^0 = 0 \\ \mathbf{W}^0(0, \mathbf{x}) = \mathbf{W}_0^0(\mathbf{x}) \end{cases} \quad (2)$$

Proof. : The proof of this result can be found in [19], chapter 2, Theorems 2.3 and 2.4. We do not repeat this proof here but briefly comment on some of their aspects: The assumptions 2.(a) et 2.(b) simply means that system (1) is a quasi-linear symmetric hyperbolic system in the sense of Friedrichs. The uniqueness and existence of solution on a finite time $T > 0$ can then be established by classical iteration techniques relying on energy estimates (see for instance [18] or [19]). However the presence of the large coefficient $1/\varepsilon$ could possibly make this time of existence ε -dependent and shrinking to 0 with ε . Assumption 2.(d) ensures that this will not be the case since the matrices C_j being constant, the large terms will not contribute to the energy estimates.

The assumption 2.(e) $A_0 = A_0(\varepsilon \mathbf{W})$ allows to bound its time derivative independently of ε : Since we have

$$\partial_t A_0(\varepsilon \mathbf{W}) = \frac{DA_0}{D\mathbf{W}} \varepsilon \partial_t \mathbf{W} = -\frac{DA_0}{D\mathbf{W}} \varepsilon A_0^{-1} [A_j \partial_j \mathbf{W} + \frac{1}{\varepsilon} \partial_j C_j \mathbf{W}]$$

The ε and $1/\varepsilon$ terms balance together and give an estimate independent of ε .

The assumptions 1.(b) and 1.(c) means that the initial condition is sufficiently close to the kernel of the large operator to ensure that the time derivative $\partial_t \mathbf{W}(0, \mathbf{x}, \varepsilon)$ is bounded in H^{s-1} independently of ε . This condition implies that the initial data are “well-prepared” and will not generate fast oscillations on a $1/\varepsilon$ time scale. \square

2.2 Reduced limit system

Even if (2) provides a complete description of the behavior of the solutions of the original system as ε tends to 0, the limit system contains as many unknowns as the original one. Actually, one may even consider that it contains more unknowns as the first order correction \mathbf{W}^1 have also to be computed. In practice, this largely depends on the specific system considered as some lines of the matrices $A_j(\mathbf{W}^0, 0)$ may be identically zero and/or the evaluation of some terms of the first order correction can be completely obvious. However, it can be interesting to derive from (2) a “reduced” set of equations containing less unknowns by eliminating the first order correction \mathbf{W}^1 . A particularly pleasant framework to construct such a reduced system is the following :

Assume that the kernel $K = \{\mathbf{W} \in \mathbb{R}^N \text{ s.t. } \sum_j C_j \partial_{x_j} \mathbf{W} = 0\}$ have dimension $n < N$ and can be parametrized by a linear operator with constant coefficients such that :

$$\forall \mathbf{W} \in K \subset \mathbb{R}^N, \quad \exists \boldsymbol{\omega} \in S \subset \mathbb{R}^n, \quad \mathbf{W} = \mathcal{M}(\boldsymbol{\omega})$$

Since the operator $\mathbb{L} = \sum_j C_j \partial_{x_j}$ have constant coefficients, $\mathcal{M}(\boldsymbol{\omega})$ is also a differential operator of order 1 with constant coefficients that can be written :

$$\mathcal{M}(\boldsymbol{\omega}) = \left(\sum_{j=1}^d P_j \partial_{x_j} + P_0 \right) \boldsymbol{\omega} \quad (3)$$

where the matrices $\{P_j; j = 0, d\}$ are rectangular $N \times n$ constant matrices. Then consider the adjoint operator \mathcal{M}^* from \mathbb{R}^N to \mathbb{R}^n satisfying

$$(\mathcal{M}(\boldsymbol{\omega}), \mathbf{W}) = (\boldsymbol{\omega}, \mathcal{M}^* \mathbf{W})$$

The operator \mathcal{M}^* is an “annhilator” for the \mathbb{L} operator in the sense that

$$\mathcal{M}^* \mathbb{L} = 0$$

Indeed we have :

$$(\mathcal{M}^* \mathbb{L} \mathbf{W}, \boldsymbol{\omega}) = (\mathbb{L} \mathbf{W}, \mathcal{M} \boldsymbol{\omega}) = -(\mathbf{W}, \mathbb{L} \mathcal{M} \boldsymbol{\omega}) = 0$$

since the C_j being symmetric matrices, \mathbb{L} is a skew-symmetric operator.

From (3) \mathcal{M}^* has the explicit expression :

$$\mathcal{M}^*(\mathbf{W}) = - \sum_{j=1}^d P_j^t \partial_{x_j} \mathbf{W} + P_0^t \mathbf{W} \quad (4)$$

where $P_j^t; j = 0, \dots, d$ are rectangular $n \times N$ matrices, transposes of the P_j .

With the operators \mathcal{M} and $\mathcal{A} = \mathcal{M}^*$ at hand, a reduced system of equations can be obtained by left multiplying (2) by the annhilator \mathcal{A} for functions $\mathbf{W} = \mathcal{M}(\boldsymbol{\omega})$. In this operation, the first-order correction $\sum_j C_j \partial_{x_j} \mathbf{W}^1$ vanishes and we obtain with $\mathbf{W} = \mathcal{M}(\boldsymbol{\omega})$:

$$\begin{cases} \mathcal{A} A_0(0) \mathcal{M} \partial_t \boldsymbol{\omega} + \sum_j \mathcal{A} A_j(\mathcal{M}(\boldsymbol{\omega}), 0) \mathcal{M} \partial_{x_j} \boldsymbol{\omega} = 0 \\ \boldsymbol{\omega}(0, \mathbf{x}) = \boldsymbol{\omega}^0(\mathbf{x}) \end{cases} \quad (5)$$

that is an autonomous system for the reduced variable $\omega \in \mathbb{R}^n$. Note that to obtain (5), we have used the fact that \mathcal{M} being a linear differential operator defined by constant matrices P_j , it commutes with the time and spatial derivatives.

Note also that spatial derivatives are "hidden" in the definition of the operators \mathcal{A} and \mathcal{M} . Therefore in contrast with the equations (2) that is a first-order differential system, (5) defines a *third-order* differential system of equations (see section 3.2.3 for the concrete example of reduced MHD system). The choice of using (5) instead of (2) as a basis for a numerical method is therefore problem dependent and in practice (5) can be more difficult to approximate than the original limit system.

3 Application to reduced MHD

3.1 The ideal MHD system

We now proceed to show how this general framework can be applied to the MHD equations and begin to recall some basic facts about this system. In the sequel, we will make the assumption that the flow is barotropic, that is the pressure is only a function of the density. This assumptions includes isentropic as well as isothermal flows.

The ideal MHD system can be written under many different forms. Since the general theory we have described make use of the symmetry of the jacobian matrices, we use here a symmetric form of the system :

$$\rho \frac{D}{Dt} \mathbf{u} + \nabla(p + \mathbf{B}^2/2) - (\mathbf{B} \cdot \nabla) \mathbf{B} = 0 \quad (6.1)$$

$$\frac{D}{Dt} \mathbf{B} - (\mathbf{B} \cdot \nabla) \mathbf{u} + \mathbf{B} \nabla \cdot \mathbf{u} = 0 \quad (6.2)$$

$$\frac{1}{\gamma p} \frac{D}{Dt} p + \nabla \cdot \mathbf{u} = 0 \quad (6.3)$$

In these equation, \mathbf{u} is the velocity, \mathbf{B} the magnetic field and p is the pressure. The density ρ is related to the pressure by a state law $\rho = \rho(p)$, for instance the perfect gas state law that writes $\rho = A(p/s)^{1/\gamma}$ where A and γ are constant and s is the (here constant) entropy. The notation $D \cdot /Dt$ stands for the material derivative that is defined by $D \cdot /Dt = \partial_t \cdot + (\mathbf{u} \cdot \nabla) \cdot$.

To system (6) one must add the involution :

$$\nabla \cdot \mathbf{B} = 0 \quad (7)$$

and it is easily checked that if (7) is verified at $t = 0$, it is verified for all $t > 0$.

The system (6) is hyperbolic, its Jacobian has real eigenvalues and a complete set of eigenvectors. However, it is not a strictly hyperbolic system since some eigenvalues may coincide. Apart from waves moving with the material velocity, it is usual to split the set of MHD eigenvalues and associated waves into three groups, that are defined as :

Fast Magnetosonic waves :

$$\lambda_F^\pm = \mathbf{u} \cdot \mathbf{n} \pm C_F \quad \text{with } C_F^2 = \frac{1}{2}(V_t^2 + v_A^2 + \sqrt{(V_t^2 + v_A^2)^2 - 4V_t^2 C_A^2}) \quad (8.1)$$

Alfen waves :

$$\lambda_A^\pm = \mathbf{u} \cdot \mathbf{n} \pm C_A \quad \text{with } C_A^2 = (\mathbf{B} \cdot \mathbf{n})^2 / \rho \quad (8.2)$$

Slow Magnetosonic waves :

$$\lambda_S^\pm = \mathbf{u} \cdot \mathbf{n} \pm C_S \quad \text{with } C_S^2 = \frac{1}{2}(V_t^2 + v_A^2 - \sqrt{(V_t^2 + v_A^2)^2 - 4V_t^2 C_A^2}) \quad (8.3)$$

where v_A and V_t are defined by : $v_A^2 = |\mathbf{B}|^2 / \rho$ and $V_t^2 = \gamma p / \rho$.

The velocity of these waves is ordered as follows :

$$\lambda_S^2 \leq \lambda_A^2 \leq \lambda_F^2$$

Fast and slow Magnetosonic waves are the equivalent of acoustic waves in fluid dynamics. Alfen waves (sometimes also called shear Alfen waves) are of a different nature : The expression (8.2) shows that they do not propagate in the direction orthogonal to the the magnetic field. Actually in the direction orthogonal to the magnetic field, the speed of propagation of Alfen and slow magnetosonic waves is zero (in a frame moving with the material velocity) and only the fast magnetosonic waves survive.

3.2 Large aspect ratio theory

3.2.1 Geometry and coordinate system

In this section, we are concerned with the model of the “straight tokamak” that consists of a slender torus characterized by a small aspect ratio $\varepsilon = a/R_0$ (see figure 1). In this model, the torus is approximated by a periodic cylinder of length $2\pi R_0$ and of section of radius a . Some of the dynamical effects that occur in a tokamak are well represented in this way and this model have been extensively used in theoretical studies to understand tokamak dynamics. In particular, it is the model considered in [27] to derive his original reduced model.

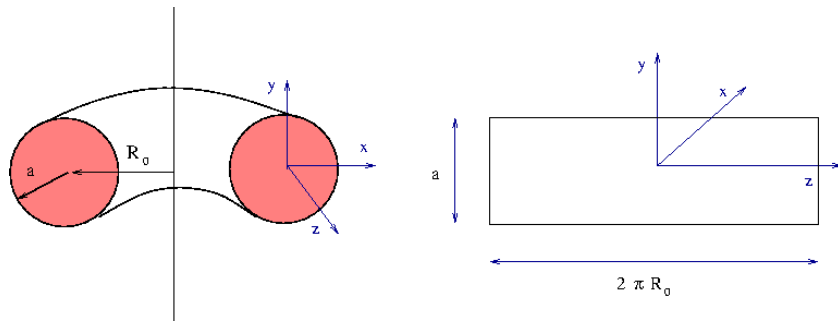


Figure 1: Straight tokamak model : the slender torus is unfold to form a periodic cylinder

Now, let (ξ, η, ζ) be the usual cartesian coordinate system and let us introduce the normalized variables :

$$\begin{cases} x = \xi/a \\ y = \eta/a \\ z = \zeta/R_0 \end{cases}$$

In a way consistent with the underlying physical problem, the z direction will be denoted as the toroidal direction while the planes (x, y) are the poloidal sections. Note also that the introduction of the normalized coordinates (x, y, z) corresponds actually to a *two scale* analysis : z the toroidal coordinate is scaled with R_0 while the poloidal coordinates (x, y) are scaled with the small radius a .

With these normalized coordinates, the expression of the spatial operators becomes :

$$a\nabla f = \frac{\partial f}{\partial x}\mathbf{e}_x + \frac{\partial f}{\partial y}\mathbf{e}_y + \varepsilon \frac{\partial f}{\partial z}\mathbf{e}_z \quad (9.1)$$

$$a\nabla \bullet \mathbf{v} = \nabla_{\perp} \bullet \mathbf{v}_{\perp} + \varepsilon \frac{\partial v_z}{\partial z} \quad (9.2)$$

$$\begin{aligned} a\nabla \times \mathbf{v} &= (\mathbf{e}_z \bullet \nabla_{\perp} \times \mathbf{v}_{\perp})\mathbf{e}_z + \nabla_{\perp} v_z \times \mathbf{e}_z + \varepsilon(-\mathbf{e}_x \frac{\partial v_y}{\partial z} + \frac{\partial v_x}{\partial z}\mathbf{e}_y) \\ &= \partial_y v_z \mathbf{e}_x - \partial_x v_z \mathbf{e}_y + (\partial_x v_y - \partial_y v_x)\mathbf{e}_z + \varepsilon(-\partial_z v_y \mathbf{e}_x + \partial_z v_x \mathbf{e}_y) \end{aligned} \quad (9.3)$$

with the definitions :

$$\begin{aligned} \mathbf{v} &= \mathbf{v}_{\perp} + v_z \mathbf{e}_z & \mathbf{v}_{\perp} &= v_x \mathbf{e}_x + v_y \mathbf{e}_y \\ \nabla_{\perp} f &= \frac{\partial f}{\partial x}\mathbf{e}_x + \frac{\partial f}{\partial y}\mathbf{e}_y & \nabla_{\perp} \bullet \mathbf{v}_{\perp} &= \frac{\partial v_x}{\partial x} + \frac{\partial v_y}{\partial y} \end{aligned}$$

3.2.2 Scaling

We now proceed to scale the unknown variables. To recast the equations into an useful form, the usual procedure is to write them in dimensionless form by scaling every variable by a characteristic value. Here, in an equivalent manner, we will consider the following change of variables:

$$\text{Magnetic field : } \mathbf{B} = \frac{F}{R}\mathbf{e}_z + \mathbf{B}_P = B_0(\mathbf{e}_z + \varepsilon\mathcal{B}) \quad (10.1)$$

$$\text{Pressure : } p = P_0(\bar{p} + \varepsilon q) \quad (10.2)$$

$$\text{Velocity : } \mathbf{u} = \varepsilon v_A \mathbf{v} \quad (10.3)$$

$$\text{Time : } t = \frac{a}{\varepsilon v_A} \tau \quad (10.4)$$

where B_0 is the reference value of the toroidal magnetic field on the magnetic axis ($R = R_0$) and \bar{p} is a constant. In these expressions, v_A is the Alfen speed defined by $v_A^2 = B_0^2/\rho_0$ where ρ_0 is some reference density (for instance, a characteristic value of the density on the magnetic axis). We choose for simplicity $P_0 = \rho_0 v_A^2$ (this only affects the value of the constant \bar{p}). The important assumptions made in (10) are :

i) that the toroidal magnetic field dominates the flow and that the poloidal field is of order ε

with respect to the toroidal field : $\mathbf{B} = \mathbf{B}_T + \varepsilon \mathbf{B}_P$. In tokamaks, the toroidal field is mainly due to external coils and it varies typically as $\mathbf{B}_T = \frac{F}{R} \mathbf{e}_z$ where F is approximately a constant and R is the distance to the rotation axis of the torus. In the model of the "straight tokamak" and in the limit of small aspect ratio a/R_0 , this leads to the following expansion of the magnetic field :

$$\mathbf{B} = \frac{F}{R} \mathbf{e}_z + \varepsilon \mathbf{B}_P = \frac{F_0}{R_0(1 + \varepsilon x)} \mathbf{e}_z + \frac{F - F_0}{R_0(1 + \varepsilon x)} \mathbf{e}_z + \varepsilon \mathbf{B}_P = B_0(\mathbf{e}_z + \varepsilon \mathcal{B})$$

where $B_0 = F_0/R_0$ is the value of the toroidal magnetic field on the magnetic axis. Note that \mathcal{B} contains a toroidal component. This component is assumed to be of the same order than the magnetic poloidal field.

ii) that the pressure fluctuations are also of order ε . Since the poloidal magnetic field is of order ε with respect to the toroidal field, this means that the poloidal plasma β parameter is of order 1. In the physical literature, this situation is referred to as a "high" β ordering [28].

iii) that the velocities are small with respect to the Alfen speed. Strictly speaking this assumption needs only to be done for the perpendicular velocity. We adopt it for the full velocity vector in order to simplify the presentation.

iv) that we are interested in the long time behavior. Actually, the assumption (10) means that we are interested in the long time behavior of the system with respect to the Alfen time a/v_A that represent the typical time for a magnetosonic wave to cross the tokamak section. (see section 3.2.4 for some remarks on the short time behavior of the system on the fast scale a/v_A).

Introducing these expression into the MHD system, we get :

$$\begin{aligned} \rho(\bar{p} + \varepsilon q) \left[\frac{\partial}{\partial \tau} \mathbf{v} + (\mathbf{v}_\perp \cdot \nabla_\perp) \mathbf{v} \right] + \partial_z (q + \mathcal{B}_z) \mathbf{e}_z + \nabla_\perp \mathcal{B}^2 / 2 - \partial_z \mathcal{B} - (\mathcal{B}_\perp \cdot \nabla_\perp) \mathcal{B} \\ + \varepsilon (\rho v_z \partial_z \mathbf{v} + \partial_z (\mathcal{B}^2 / 2) \mathbf{e}_z - \mathcal{B}_z \partial_z \mathcal{B}) + \frac{1}{\varepsilon} \nabla_\perp (q + \mathcal{B}_z) = 0 \end{aligned} \quad (11.2)$$

$$\begin{aligned} \frac{\partial}{\partial \tau} \mathcal{B}_\perp + (\mathbf{v}_\perp \cdot \nabla_\perp) \mathcal{B}_\perp - (\mathcal{B}_\perp \cdot \nabla_\perp) \mathbf{v}_\perp + \mathcal{B}_\perp \nabla_\perp \cdot \mathbf{v}_\perp - \partial_z \mathbf{v}_\perp \\ + \varepsilon (\mathbf{v}_z \partial_z \mathcal{B}_\perp - \mathcal{B}_z \partial_z \mathbf{v}_\perp + \partial_z \mathbf{v}_z \mathcal{B}_\perp) = 0 \end{aligned} \quad (11.3)$$

$$\frac{\partial}{\partial \tau} \mathcal{B}_z + (\mathbf{v}_\perp \cdot \nabla_\perp) \mathcal{B}_z - (\mathcal{B}_\perp \cdot \nabla_\perp) \mathbf{v}_z + \mathcal{B}_z \nabla_\perp \cdot \mathbf{v}_\perp + \varepsilon \mathbf{v}_z \partial_z \mathcal{B}_z + \frac{1}{\varepsilon} \nabla_\perp \cdot \mathbf{v}_\perp = 0 \quad (11.4)$$

$$\frac{1}{\gamma(\bar{p} + \varepsilon q)} \left[\frac{\partial}{\partial \tau} q + (\mathbf{v}_\perp \cdot \nabla_\perp) q + \varepsilon \mathbf{v}_z \partial_z q \right] + \partial_z \mathbf{v}_z + \frac{1}{\varepsilon} \nabla_\perp \cdot \mathbf{v}_\perp = 0 \quad (11.5)$$

If one introduces the variable $\mathbf{W} = (\mathbf{v}_x, \mathbf{v}_y, \mathbf{v}_z, \mathcal{B}_x, \mathcal{B}_y, \mathcal{B}_z, q)^t$, the previous system can be written as

$$A_0(\varepsilon \mathbf{W}) \partial_\tau \mathbf{W} + \sum_j A_j(\mathbf{W}, \varepsilon \mathbf{W}) \partial_{x_j} \mathbf{W} + \frac{1}{\varepsilon} \sum_j C_j \partial_{x_j} \mathbf{W} = 0 \quad (12)$$

where the matrices $A_0, A_j(\mathbf{W}, \varepsilon \mathbf{W})$ are defined by :

$$A_0 = \begin{pmatrix} \rho I_3 & 0_3 & 0 \\ 0_3 & I_3 & 0 \\ 0_3 & 0_3 & \frac{1}{\gamma(\bar{p} + \varepsilon q)} \end{pmatrix}$$

$$A_x = \begin{pmatrix} \rho v_x & 0 & 0 & 0 & \mathcal{B}_y & \mathcal{B}_z & 0 \\ 0 & \rho v_x & 0 & 0 & -\mathcal{B}_x & 0 & 0 \\ 0 & 0 & \rho v_x & 0 & 0 & -\mathcal{B}_x & 0 \\ 0 & 0 & 0 & v_x & 0 & 0 & 0 \\ \mathcal{B}_y & -\mathcal{B}_x & 0 & 0 & v_x & 0 & 0 \\ \mathcal{B}_z & 0 & -\mathcal{B}_x & 0 & 0 & v_x & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & \frac{v_x}{\gamma(\bar{p} + \varepsilon q)} \end{pmatrix}$$

$$A_y = \begin{pmatrix} \rho v_y & 0 & 0 & -\mathcal{B}_y & 0 & 0 & 0 \\ 0 & \rho v_y & 0 & \mathcal{B}_x & 0 & \mathcal{B}_z & 0 \\ 0 & 0 & \rho v_y & 0 & 0 & -\mathcal{B}_y & 0 \\ -\mathcal{B}_y & \mathcal{B}_x & 0 & v_y & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & v_y & 0 & 0 \\ 0 & \mathcal{B}_z & -\mathcal{B}_y & 0 & 0 & v_y & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & \frac{v_y}{\gamma(\bar{p} + \varepsilon q)} \end{pmatrix}$$

$$A_z = \begin{pmatrix} \varepsilon \rho v_z & 0 & 0 & -(1 + \varepsilon \mathcal{B}_z) & 0 & 0 & 0 \\ 0 & \varepsilon \rho v_z & 0 & 0 & -(1 + \varepsilon \mathcal{B}_z) & 0 & 0 \\ 0 & 0 & \varepsilon \rho v_z & \varepsilon \mathcal{B}_x & \varepsilon \mathcal{B}_y & 0 & 1 \\ -(1 + \varepsilon \mathcal{B}_z) & 0 & \varepsilon \mathcal{B}_x & \varepsilon v_z & 0 & 0 & 0 \\ 0 & -(1 + \varepsilon \mathcal{B}_z) & \varepsilon \mathcal{B}_y & 0 & \varepsilon v_z & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & \varepsilon v_z & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 & \varepsilon \frac{v_z}{\gamma(\bar{p} + \varepsilon q)} \end{pmatrix}$$

while the constant matrices C_j are given by :

$$C_x = \begin{pmatrix} 0 & 0 & 0 & 0 & 0 & 1 & 1 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 1 & 0 & 0 & 0 & 0 & 0 & 0 \\ 1 & 0 & 0 & 0 & 0 & 0 & 0 \end{pmatrix} \quad C_y = \begin{pmatrix} 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 & 1 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 & 0 \end{pmatrix}$$

This form makes apparent that the ideal MHD system can be put under the general form studied in section 2.1. Therefore, the general results obtained in this section can be applied and we have

Theorem 2 1. Assume that the initial velocity, magnetic field and pressure are defined by :

$$\begin{cases} \mathbf{u}(0, \mathbf{x})/V_A = \varepsilon(\mathbf{v}^0(\mathbf{x}) + \varepsilon \mathbf{v}^1(\varepsilon, \mathbf{x})) \\ \mathbf{B}(0, \mathbf{x})/B_0 = \mathbf{e}_z + \varepsilon(\mathcal{B}^0(\mathbf{x}) + \varepsilon \mathcal{B}^1(\varepsilon, \mathbf{x})) \\ p(0, \mathbf{x})/p_0 = \bar{p} + \varepsilon(q^0(\mathbf{x}) + \varepsilon q^1(\varepsilon, \mathbf{x})) \end{cases}$$

where \bar{p} is a constant, the functions $\mathbf{v}^0, \mathcal{B}^0, q^0$ and $\mathbf{v}^1, \mathcal{B}^1, q^1$ are bounded in H^s and where the 0-th order initial data verifies :

$$\begin{cases} \nabla_\perp \cdot \mathbf{v}^0(\mathbf{x}) = 0 & (13.1) \\ \exists f(z) \text{ such that } \mathcal{B}_z^0(\mathbf{x}) = f(z) - q^0(\mathbf{x}) & (13.2) \end{cases}$$

then the solution of the full MHD system (6) exists for a time T independent of ε and this solution converges in H^{s-1} to the solution of the reduced system given below in section 3.2.3.

Proof. The conditions on the structure of the system given in theorem 1 are satisfied while the conditions (13) express the fact that the 0–order initial data is in the kernel of the large operator. The assumptions of theorem 1 are then fulfilled and the result follows. \square

3.2.3 Slow limit of the system

According to the general theory described in section 2.1, the solutions of (6) will be close to the solutions of the limit system of equations given by

$$\begin{cases} A_0(0)\partial_\tau \mathbf{W}^0 + A_j(\mathbf{W}^0, 0)\partial_{x_j} \mathbf{W}^0 + C_j\partial_{x_j} \mathbf{W}^1 = 0 \\ C_j\partial_{x_j} \mathbf{W}^0 = 0 \end{cases} \quad (14)$$

The zero-order solutions are functions $\mathbf{W}^0 = (v_x, v_y, v_z, \mathcal{B}_x, \mathcal{B}_y, \mathcal{B}_z, q)$ that are in the kernel of the large operator. These functions must therefore verify :

$$\nabla_\perp \cdot \mathbf{v}_\perp = 0 \quad (15.1)$$

$$\nabla_\perp(q + \mathcal{B}_z) = 0 \quad (15.2)$$

using these results, the explicit form of system (14) can be written

$$\rho(\bar{p})\left[\frac{\partial}{\partial\tau} \mathbf{v}_z + (\mathbf{v}_\perp \cdot \nabla_\perp)\mathbf{v}_z\right] + \partial_z q + (\mathcal{B}_\perp \cdot \nabla_\perp)q = 0 \quad (16.1)$$

$$\frac{\partial}{\partial\tau} \mathcal{B}_\perp + (\mathbf{v}_\perp \cdot \nabla_\perp)\mathcal{B}_\perp - (\mathcal{B}_\perp \cdot \nabla_\perp)\mathbf{v}_\perp - \partial_z \mathbf{v}_\perp = 0 \quad (16.2)$$

$$\begin{aligned} \rho(\bar{p})\left[\frac{\partial}{\partial\tau} \mathbf{v}_\perp + (\mathbf{v}_\perp \cdot \nabla_\perp)\mathbf{v}_\perp\right] + \nabla_\perp \mathcal{B}^2/2 - \partial_z \mathcal{B}_\perp - (\mathcal{B}_\perp \cdot \nabla_\perp)\mathcal{B}_\perp \\ + \nabla_\perp(q^1 + \mathcal{B}_z^1) = 0 \end{aligned} \quad (16.3)$$

$$\frac{\partial}{\partial\tau} \mathcal{B}_z + (\mathbf{v}_\perp \cdot \nabla_\perp)\mathcal{B}_z - (\mathcal{B}_\perp \cdot \nabla_\perp)\mathbf{v}_z + \nabla_\perp \cdot \mathbf{v}_\perp^1 = 0 \quad (16.4)$$

$$\frac{1}{\gamma\bar{p}}\left[\frac{\partial}{\partial\tau} q + (\mathbf{v}_\perp \cdot \nabla_\perp)q\right] + \partial_z \mathbf{v}_z + \nabla_\perp \cdot \mathbf{v}_\perp^1 = 0 \quad (16.5)$$

where \bar{p} and $\rho(\bar{p})$ are constant. Using the fact that by (15.2) $q + \mathcal{B}_z = f(z)$ where $f(z)$ is an arbitrary function, equations (16.4) and (16.5) can be combined to eliminate the corrective term $\nabla_\perp \cdot \mathbf{v}_\perp^1$ resulting in :

$$\left(\frac{1}{\gamma\bar{p}} - 1\right)\left[\frac{\partial}{\partial\tau} q + (\mathbf{v}_\perp \cdot \nabla_\perp)q\right] + (\mathcal{B}_\perp \cdot \nabla_\perp)\mathbf{v}_z + \partial_z \mathbf{v}_z = 0$$

We also note that in the perpendicular momentum equation, the term $\nabla_\perp(q^1 + \mathcal{B}_z^1)$ ensures that $\nabla_\perp \cdot \mathbf{v}_\perp = 0$, this term can therefore be combined with the $\nabla_\perp \mathcal{B}^2/2$ term with no change in the result. Introducing the notations

$$\frac{D^\perp}{Dt} \cdot = \frac{\partial}{\partial\tau} \cdot + (\mathbf{v}_\perp \cdot \nabla_\perp) \cdot \quad \nabla_{//} \cdot = (\mathcal{B}_\perp \cdot \nabla_\perp) \cdot + \partial_z \cdot$$

we get the final limit system :

$$\rho \frac{D^\perp}{Dt} \mathbf{v}_\perp - \nabla_{//} \mathcal{B}_\perp + \nabla_\perp \lambda = 0 \quad (17.1)$$

$$\frac{D^\perp}{Dt} \mathcal{B}_\perp - \nabla_{//} \mathbf{v}_\perp = 0 \quad (17.2)$$

$$\rho \frac{D^\perp}{Dt} \mathbf{v}_z + \nabla_{//} q = 0 \quad (17.3)$$

$$\left(\frac{1}{\gamma \bar{p}} - 1\right) \frac{D^\perp}{Dt} q + \nabla_{//} \mathbf{v}_z = 0 \quad (17.4)$$

where λ stands here for a scalar “pressure” that ensures that the perpendicular divergence of the perpendicular velocity is zero.

The equations (17) shows that the limit system splits into two different sub-systems :

- (17.1) and (17.2) as well as the constraint (15.1) describe the *incompressible* dynamics of the perpendicular motion of the plasma. This set of equation does not depend on the pressure and toroidal velocity equations and can be solved independently of the other two equations.
- On the other hand, the two scalar equations (17.3) and (17.4) describe the *compressible* parallel dynamics of the plasma. Actually, without the perpendicular convective terms, these two equations describe a compressible one dimensional flow in the parallel direction to the magnetic field. Note that these equations are “slave” of the first two ones since both the perpendicular advection and the $\nabla_{//}$ operator depend only on the solution of equations (17.1) and (17.2). Thus (17.3) and (17.4) can be solved once the solutions of (17.1) and (17.2) have been computed.

As in the original MHD system, the system (17) is endowed with an involution : Using that $\nabla \cdot \mathbf{B} = 0$, we have in the limit $\varepsilon \rightarrow 0$ that the perpendicular divergence of the magnetic field is zero,

$$\nabla_\perp \cdot \mathcal{B}_\perp = 0$$

if this property is true for the initial data, it is conserved by system (17) :

Proposition 1. *Assume that the perpendicular divergence of the perpendicular magnetic field is zero at time $t = 0$: $\nabla_\perp \cdot \mathcal{B}_\perp(\mathbf{x}, t = 0) = 0$ then $\nabla_\perp \cdot \mathcal{B}_\perp(\mathbf{x}, t) = 0$ for $t > 0$.*

Proof. This follows directly by applying the perpendicular divergence operator to the perpendicular Faraday law (17.2). Note that to obtain this result, both the properties $\nabla_\perp \cdot \mathcal{B}_\perp = 0$ and $\nabla_\perp \cdot \mathbf{v}_\perp = 0$ are used. \square

Although, equations (17.1) and (17.2) have a similar structure, we note that $\nabla_\perp \cdot \mathbf{v}_\perp = 0$ is not an involution for the system : equation (17.1) does not conserve the perpendicular divergence of \mathbf{v}_\perp , the corrective term $\nabla_\perp \lambda$ is therefore needed to insure that $\nabla_\perp \cdot \mathbf{v}_\perp = 0$.

We will now from the limit system (17) obtain a *reduced* system characterized by a smaller number of equation than the number of the original system. As explained in section 2.2, this

can be obtained by canceling out the corrective term. Since equations (17.1) and (17.2) form an autonomous system, we concentrate on these two equations. According to the general procedure sketched in section 2.2, we look for a parametrization of the function space where the solution belongs to. In the present case, the space $K = \{(\mathbf{v}_\perp, \mathcal{B}_\perp); \nabla_\perp \cdot \mathbf{v}_\perp = \nabla_\perp \cdot \mathcal{B}_\perp = 0\}$ can be parametrized by 2 scalar functions ϕ, ψ such that

$$\mathbf{v}_\perp = \mathbf{e}_z \times \nabla \phi \quad (18.1)$$

$$\mathcal{B}_\perp = \mathbf{e}_z \times \nabla \psi \quad (18.2)$$

Let us define for any scalar function $F \in H^1$ the operator \mathcal{M} with values in $L^2 \times L^2$ by :

$$\mathcal{M}(F) = \mathbf{e}_z \times \nabla F$$

The following Green formula :

$$\int_\Omega \mathbf{e}_z \times \nabla F \cdot \mathbf{W} dx = \int_{\partial\Omega} F \mathbf{e}_z \times \mathbf{W} \cdot \mathbf{n} ds - \int_\Omega F \mathbf{e}_z \cdot \nabla \times \mathbf{W} dx$$

shows that the adjoint operator of \mathcal{M} is defined by :

$$\mathcal{M}^*(\mathbf{W}) = \mathbf{e}_z \cdot \nabla \times \mathbf{W}$$

Using the general recipe given in section 2.2, we get a reduced system for the variables ϕ, ψ by :

$$\rho \mathcal{M}^* \frac{D^\perp}{Dt} \mathcal{M}(\phi) - \mathcal{M}^* \nabla_{//} \mathcal{M}(\psi) = 0 \quad (19.1)$$

$$\mathcal{M}^* \frac{D^\perp}{Dt} \mathcal{M}(\psi) - \mathcal{M}^* \nabla_{//} \mathcal{M}(\phi) = 0 \quad (19.2)$$

where the corrective term $\nabla_\perp \lambda$ have been canceled out by the annihilator operator \mathcal{M}^* . After some algebra, this system admits the following expression :

$$\rho \frac{D^\perp}{Dt} \mathcal{U} - \nabla_{//} J = 0 \quad (20.1)$$

$$\partial_\tau J - \nabla_\perp^2 (\partial_x \phi \partial_y \psi - \partial_x \psi \partial_y \phi) - \partial_z \mathcal{U} = 0 \quad (20.2)$$

where \mathcal{U} and J are defined as $\mathcal{U} = -\nabla_\perp^2 \phi$ and $J = -\nabla_\perp^2 \psi$. We note that $\mathcal{U} = \partial_y v_x - \partial_x v_y$ represent the z -component of the curl of the velocity vector, therefore in reduced MHD literature, \mathcal{U} is defined as the *vorticity* and (20.1) is called the vorticity equation by analogy with the fluid dynamics case.

From a physical point of view, the quantity $J = -\nabla_\perp^2 \psi$ corresponds to the toroidal current traversing the plasma column and therefore equation (20.2) defines the behavior of the toroidal current. In the framework of reduced MHD model, this equation is not used. Instead, rewriting (20.2) as

$$-\nabla_\perp^2 [\partial_\tau \psi + (\partial_x \phi \partial_y \psi - \partial_x \psi \partial_y \phi) - \partial_z \phi] = 0 \quad (21)$$

and noting that $(\partial_x \phi \partial_y \psi - \partial_x \psi \partial_y \phi)$ corresponds to the advection term $\mathbf{v}_\perp \cdot \nabla_\perp \psi$, one prefers to use the equation :

$$\frac{\partial}{\partial \tau} \psi + \mathbf{v}_\perp \cdot \nabla_\perp \psi - \frac{\partial}{\partial z} \phi = 0 \quad (22)$$

Strictly speaking (22) cannot be deduced directly from (21) and integration factors should have appeared in (22). However, it is possible to establish directly (22). This is done in Annex 1.

To complete the description of the reduced MHD models, we mention that in the present model, it is not necessary to solve the toroidal and pressure equations (17.3) and (17.4) since the dynamics is entirely governed by (17.1) and (17.2). Neglecting these equations, is also sometimes justified as follows ([28]) : The acceleration term of the toroidal momentum equation (17.3) is :

$$\nabla_{//}q = \mathcal{B}_{\perp} \cdot \nabla_{\perp}q + \frac{\partial}{\partial z}q = \mathbf{B} \cdot \nabla q$$

Then it can be shown (see [28]), that if at time $t = 0$, $\mathbf{B} \cdot \nabla q = 0$, then this quantity will stay equal to zero. Therefore, the toroidal acceleration is null and if initially $v_z = 0$, then the toroidal velocity will remain zero. Consequently, the velocity source $\nabla_{//}v_z$ in the pressure equation remains zero and the pressure correction q behaves as a passive scalar.

In the framework of MHD studies in tokamaks, the assumption $\mathbf{B} \cdot \nabla q = 0$ is very natural since the flows under investigation are close to an MHD equilibrium characterized by :

$$\nabla p = \mathbf{J} \times \mathbf{B} \quad (23)$$

that implies that $\mathbf{B} \cdot \nabla p = 0$. Actually, a lot of MHD studies aims to examine the linear or non-linear stability of such equilibrium and therefore these works use precisely the relation (23) to define the initial conditions.

Summarizing, the dynamics of the MHD model can be reduced to a system of 2 equations for the scalar quantities (ϕ, ψ)

$$\left[\begin{array}{l} \rho \frac{D^{\perp}}{Dt} \mathcal{U} - \nabla_{//} J = 0 \quad (24.1) \\ \frac{D^{\perp}}{Dt} \psi - \frac{\partial}{\partial z} \phi = 0 \quad (24.2) \end{array} \right]$$

with

$$\mathcal{U} = -\nabla_{\perp}^2 \phi \quad J = -\nabla_{\perp}^2 \psi$$

These equations are conventionally written in a somewhat different form emphasizing their hamiltonian character [20]. Introducing the bracket

$$[f, g] = \mathbf{e}_z \cdot \nabla_{\perp} f \times \nabla_{\perp} g$$

we have that for any f

$$\mathbf{v}_{\perp} \cdot \nabla_{\perp} f = [\phi, f] \quad \text{while} \quad \mathcal{B}_{\perp} \cdot \nabla_{\perp} f = [\psi, f]$$

and the previous system can be written as

$$\left[\begin{array}{l} \frac{\partial}{\partial \tau} \mathcal{U} + [\phi, \mathcal{U}] - [\psi, J] - \frac{\partial}{\partial z} J = 0 \quad (25.1) \\ \frac{\partial}{\partial \tau} \psi + [\phi, \psi] - \frac{\partial}{\partial z} \phi = 0 \quad (25.2) \end{array} \right]$$

where we have assumed $\rho = 1$ using an appropriate scaling of the density.

3.2.4 Fast modes of the system

In this section, we briefly comment on the solutions of the full MHD system that are eliminated by the reduced model. In other term, we analyze the short time behavior of system (12). Considering the fast time scale $\tau' = \varepsilon\tau$ or in an equivalent manner the fast reference time $t' = \frac{a}{v_A}$, it is seen that the system (12) reduces to the linear hyperbolic system

$$A_0(0)\partial_{\tau'}\mathbf{W} + \sum_j C_j\partial_{x_j}\mathbf{W} = 0 \quad (26)$$

Let $\mathbf{n} = (\mathbf{n}_x, \mathbf{n}_y)^t$ be a 2D unit vector in the poloidal plane, the matrix $A_0(0)^{-1}(\mathbf{n}_x C_x + \mathbf{n}_y C_y)$ is diagonalizable and its eigenvalues are :

$$\lambda_0 = 0 \text{ (with multiplicity 6)}, \lambda_+ = \sqrt{\frac{\gamma\bar{p} + 1}{\rho}}, \lambda_- = -\sqrt{\frac{\gamma\bar{p} + 1}{\rho}} \quad (27)$$

or in term of non-normalized variables :

$$\lambda_0 = 0 \text{ (with multiplicity 6)}, \lambda_+ = \sqrt{\frac{\gamma p + B_0^2}{\rho}}, \lambda_- = -\sqrt{\frac{\gamma p + B_0^2}{\rho}} \quad (28)$$

Comparing these expression to (8), it is readily be seen that the non-zero eigensolutions correspond to fast magnetosonic waves traveling in the direction perpendicular to the toroidal magnetic field $B_0\mathbf{e}_z$. The situation here is quite similar to the one encountered with the compressible Euler equation where the fast limit corresponds to the acoustic equations describing the propagation of acoustic waves. Here, however, we also have an additional splitting in term of space directions. The fast limit of the system describes the propagation of magnetosonic waves *in the poloidal plane* while waves traveling in the toroidal direction are not present in this limit. The slow limit of the system that have been examined in section 3.2.3 thus excludes perpendicular magnetosonic waves in the same way as acoustic waves are filtered out from the compressible Euler equation when one consider the incompressible limit equation.

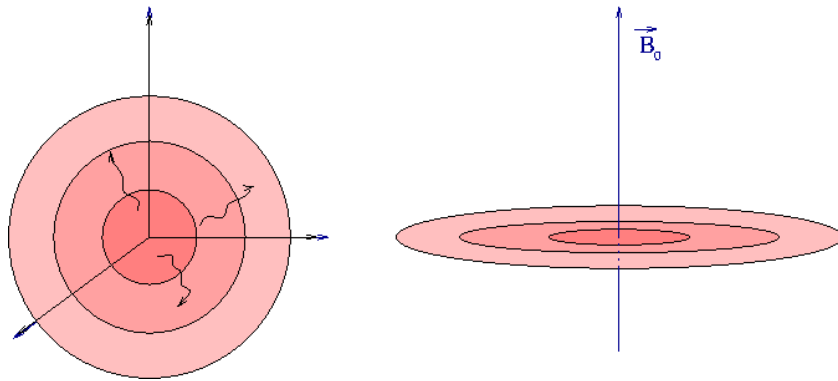


Figure 2: Comparison of the fast modes between the low Mach number limit and reduced MHD model; Left, Low Mach number limit : 3D isotropic propagation of acoustic waves; Right, reduced MHD models : 2D propagation of fast magnetosonic waves in the poloidal plane.

From a numerical point of view, this is one of the main advantage of reduced MHD since the use of the full MHD system (6) implies strong CFL stability requirement linked to the propagation of magnetosonic waves. Note however that this splitting of the waves is not due to differences in the *speed of propagation* as for the Euler equation but rather to the different *space scales* in the toroidal and poloidal directions. In a toroidal system as a tokamak is, gradients in the toroidal directions are small with respect to gradient in the perpendicular directions and it is this fact that produce the wave separation rather than their speed of propagation since the velocities of Alfen and magnetosonic waves are roughly of the same order of magnitude.

4 Concluding remarks

This work has shown that the derivation of reduced MHD models for fusion plasma can be formulated in the general framework of the singular limit of hyperbolic system of PDEs with large operator. This allows to use the results of this theory and to prove rigorously the validity of these approximations. In particular, it is proven, that the solutions of the full MHD system converge to the solutions of the reduced model displayed in section 3.2.3.

This work can be extended in several different directions.

First, the reduced MHD model considered in this paper is the simplest of a whole hierarchy of models of increasing complexity. The model used in the present work has at least two important weaknesses :

- a) It uses the straight tokamak model and therefore curvature terms are absent from the resulting equations. More elaborated models [3, 12] retaining curvature effects and high order terms in ε are available and can be possibly analyzed within the present framework.
- b) Another weakness of the model is that it uses as small parameter the ratio a/R_0 that cannot be considered as small in a large number of today's machines. More elaborated models denoted in several references as "generalized reduced MHD models" [11, 17, 30, 26] have been derived. These models do not make use of the small aspect ratio hypothesis and thus are in principle applicable with no restriction on the geometry. However, even from the point of view of formal asymptotics, these models are not always easy to understand and contains ad-hoc assumptions that are difficult to justify rigorously. It would be extremely valuable to study the possibility to formulate these "generalized reduced" MHD models along the lines exposed in this work.

In the terminology of [25], the present work has examined the slow singular limit of the MHD equations. A second possible and interesting sequel of this work would be to examine the fast singular limit where no assumption is made on the boundedness of the initial time derivatives. On physical grounds, the assumption underlying the use of reduced MHD models is that fast transverse magnetosonic waves do not affect the dynamics on the long time scale in the same way as in fluid dynamics, the propagation of acoustic waves do not modify the average incompressible background. For the Euler (or Navier-Stokes) equations this can be proven for certain cases e.g [25, 1]. Such a result however appears significantly more difficult to obtain for the MHD equations since their degree of non-linearity is higher than in the fluid dynamics case. Note however, that the formal asymptotic expansion used in [17] can be considered as a first step in this direction.

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A Annex 1

In this section, we give a direct obtention of Equation (22). Since \mathbf{B} is a divergence free vector field, there exists a vector potential \mathbf{A} such that $\nabla \times \mathbf{A} = \mathbf{B}$. From the expression (9.3) of the curl operator and the expression of the magnetic field, it is seen that ψ is the toroidal component of this vector potential. In term of vector potential \mathbf{A} , Faraday's law writes :

$$\frac{\partial}{\partial t} \mathbf{A} + \mathbf{E} = \nabla \phi$$

where \mathbf{E} is the electric field and ϕ is the electric potential²
Taking the scalar product of this equation by \mathbf{e}_z , one has

$$\frac{\partial}{\partial t} \psi + \mathbf{e}_z \cdot \mathbf{E} - \partial_z \phi = 0$$

Now, using Ohm's law $\mathbf{E} + \mathbf{v} \times \mathbf{B} = 0$ and the identity

$$-\mathbf{e}_z \cdot (\mathbf{v} \times \mathbf{B}) = \mathbf{v} \cdot (\mathbf{e}_z \times \mathbf{B})$$

one obtains (22) :

$$\frac{\partial}{\partial \tau} \psi + \mathbf{v}_\perp \cdot \nabla_\perp \psi - \frac{\partial}{\partial z} \phi = 0$$

Note that since $\mathbf{v}_\perp \cdot \nabla_\perp \psi = -\mathcal{B}_\perp \cdot \nabla_\perp \phi$, this equation can also be written

$$\frac{\partial}{\partial \tau} \psi - \nabla_{//} \phi = 0$$

From a physical point of view, this interpretation shows that the velocity defined by (18.1) is the so-called electric drift $\vec{v}_E = \mathbf{E} \times \mathbf{B} / |\mathbf{B}|^2$. Indeed it can be shown (see [28] for instance) that the reduced MHD approximation implies that the transverse electric field is electrostatic :

$$\mathbf{E}_\perp = \nabla_\perp \phi$$

from which one can deduce by taking the cross product of Ohm's law by \mathbf{B} the expression (18.2) since in the small aspect ratio theory, the parallel and toroidal direction are identical up to terms of order ε .

²Note that the sign convention to define the electric field can be the opposite depending on the authors

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