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INSTITUT NATIONAL DE RECHERCHE EN INFORMATIQUE ET EN AUTOMATIQUE

*Analytical Solution for Wave Propagation in  
Stratified Acoustic/Porous Media. Part I: the 2D  
Case*

Julien Diaz — Abdelaâziz Ezziani

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## Analytical Solution for Wave Propagation in Stratified Acoustic/Porous Media. Part I: the 2D Case

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**Abstract:** Thanks to the Cagniard-de Hoop we derive the solution to the problem of wave propagation in an infinite bilayered acoustic/poroelastic media, where the poroelastic layer is modelled by the biphasic Biot's model. This first part is dedicated to solution to the two dimensional problem. We illustrate the interest of the solution by using it to validate a numerical code.

**Key-words:** Biot's model, poroelastic waves, acoustic waves, acoustic/poroelastic coupling, analytical solution, Cagniard-De Hoop's technique.

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## **Solution analytique pour la propagation d'ondes en milieu stratifié hétérogène acoustique/poroélastique. Partie I : en dimension 2**

**Résumé :** Nous nous intéressons à la modélisation de la propagation d'ondes dans les milieux infinis bicouche acoustique/poroélastique. Nous considérons le modèle bi-phasique de Biot dans la couche poroélastique. Cette première partie est consacrée au calcul de la solution analytique en dimension deux à l'aide de la technique de Cagniard-De Hoop. Nous mettons en évidence l'intérêt de la solution analytique en l'utilisant pour valider un code de calcul.

**Mots-clés :** Modèle de Biot, ondes poroélastiques, ondes acoustiques, couplage acoustique/poroélastique, solution analytique, technique de Cagniard de Hoop.

## Introduction

The computation of analytical solutions for wave propagation problems is of high importance for the validation of numerical computational codes or for a better understanding of the reflexion/transmission properties of the media. Cagniard-de Hoop method [4, 6] is a useful tool to obtain such solutions and permits to compute each type of waves (P wave, S wave, head wave...) independently. Although it was originally dedicated to the solution to elastodynamic wave propagation, it can be applied to any transient wave propagation problem in stratified medium. However, as far as we know, few works have been dedicated to the application of this method to poroelastic medium. In [10] the analytical solution to poroelastic wave propagation in an homogeneous 2D medium is provided and in [11] the authors compute the analytical expression of the reflected wave at the interface between an acoustic and a poroelastic layer in two dimension but they do not explicit the expression of the transmitted waves.

In order to validate computational codes of wave propagation in poroelastic media, we have implemented the codes Gar6more 2D [8] and Gar6more 3D [9] which provide the complete solution (reflected and transmitted waves) of the propagation of wave in stratified 2D or 3D media composed of acoustic/acoustic, acoustic/elastic, acoustic/poroelastic or poroelastic/poroelastic layers. The codes are freely downloadable at

<http://www.spice-rtn.org/library/software/Gar6more2D>

and

<http://www.spice-rtn.org/library/software/Gar6more3D>.

We will focus here on the 2D acoustic/poroelastic case, the three dimensional and the poroelastic/poroelastic cases will be the object of forthcoming papers. The outline of the paper is as follows: we first present the model problem we want to solve and derive the Green problem from it (section 1). Then we present the analytical solution to the wave propagation problem in a stratified 2D medium composed of an acoustic and a poroelastic layer (section 2) and we detail the computation of the solution (section 3). Finally we show how the analytical solution can be used to validate a numerical code (section 4).

## 1 The model problem

We consider an infinite two dimensional medium ( $\Omega = \mathbf{R}^2$ ) composed of an homogeneous acoustic layer  $\Omega^+ = \mathbf{R} \times ]-\infty, 0]$  and an homogeneous poroelastic layer  $\Omega^- = \mathbf{R} \times [0, +\infty[$  separated by an horizontal interface  $\Gamma$  (see Fig. 1). We first describe the equations in the two layers (§1.1 and §1.2) and the transmission conditions on the interface  $\Gamma$  (§1.3), then we present the Green problem from which we compute the analytical solution (§1.4).

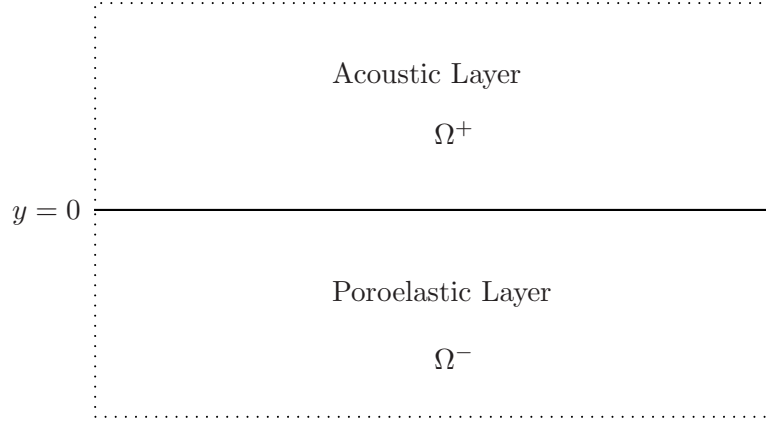


Figure 1: Configuration of the study

### 1.1 The equation of acoustics

In the acoustic layer we consider the second-order formulation of the wave equation with a point source in space, a regular source function  $f$  in time and zero initial conditions:

$$\left\{ \begin{array}{ll} \ddot{P}^+ - V^{+2} \Delta P^+ = \delta_x \delta_{y-h} f(t), & \text{in } \Omega^+ \times ]0, T], \\ \ddot{\mathbf{U}}^+ = -\frac{1}{\rho^+} \nabla P^+, & \text{in } \Omega^+ \times ]0, T], \\ P^+(x, y, 0) = 0, \dot{P}^+(x, y, 0) = 0, & \text{in } \Omega^+ \\ \mathbf{U}^+(x, y, 0) = 0, \dot{\mathbf{U}}^+(x, y, 0) = 0, & \text{in } \Omega^+ \end{array} \right. \quad (1)$$

where

- $P^+$  is the pressure;
- $\mathbf{U}^+$  is the displacement field;
- $V^+$  is the celerity of the wave;
- $\rho^+$  is the density of the fluid.

## 1.2 Biot's Model

In the second layer we consider the second order formulation of the poroelastic equations [1, 2, 3]

$$\left\{ \begin{array}{ll} \rho^- \ddot{\mathbf{U}}_s^- + \rho_f^- \ddot{\mathbf{W}}^- - \nabla \cdot \Sigma^- = 0, & \text{in } \Omega^- \times ]0, T], \\ \rho_f^- \ddot{\mathbf{U}}_s^- + \rho_w^- \ddot{\mathbf{W}}^- + \frac{1}{\mathcal{K}^-} \dot{\mathbf{W}}^- + \nabla P^- = 0, & \text{in } \Omega^- \times ]0, T], \\ \Sigma^- = \lambda^- \nabla \cdot \mathbf{U}_s^- \mathbf{I}_2 + 2\mu^- \varepsilon(\mathbf{U}_s^-) - \beta^- P^- \mathbf{I}_2, & \text{in } \Omega^- \times ]0, T], \\ \frac{1}{m^-} P^- + \beta^- \nabla \cdot \mathbf{U}_s^- + \nabla \cdot \mathbf{W}^- = 0, & \text{in } \Omega^- \times ]0, T], \\ \mathbf{U}_s^-(x, 0) = 0, \mathbf{W}^-(x, 0) = 0, & \text{in } \Omega^-, \\ \dot{\mathbf{U}}_s^-(x, 0) = 0, \dot{\mathbf{W}}^-(x, 0) = 0, & \text{in } \Omega^-, \end{array} \right. \quad (2)$$

with

$$(\nabla \cdot \Sigma^-)_i = \sum_{j=1}^2 \frac{\partial \Sigma_{ij}^-}{\partial x_j} \quad \forall i = 1, 2. \quad \text{As usual } \mathbf{I}_2 \text{ is the identity matrix of } \mathcal{M}_2(\mathbb{R})$$

and  $\varepsilon(\mathbf{U}_s^-)$  is the solid strain tensor defined by:

$$\varepsilon_{ij}(\mathbf{U}) = \frac{1}{2} \left( \frac{\partial U_i}{\partial x_j} + \frac{\partial U_j}{\partial x_i} \right).$$

In (2), the unknowns are:

- $\mathbf{U}_s^-$  the displacement field of solid particles;
- $\mathbf{W}^- = \phi^-(\mathbf{U}_f^- - \mathbf{U}_s^-)$ , the relative displacement,  $\mathbf{U}_f^-$  being the displacement field of fluid particle and  $\phi^-$  the porosity;
- $P^-$ , the fluid pressure;
- $\Sigma^-$ , the solid stress tensor.

The parameters describing the physical properties of the medium are given by:

- $\rho^- = \phi^- \rho_f^- + (1 - \phi^-) \rho_s^-$  is the overall density of the saturated medium, with  $\rho_s^-$  the density of the solid and  $\rho_f^-$  the density of the fluid;
- $\rho_w^- = a^- \rho_f^- / \phi^-$ , where  $a^-$  is the tortuosity of the solid matrix;



- $\mathcal{K}^- = \kappa^-/\eta^-$ , where  $\kappa^-$  is the permeability of the solid matrix and  $\eta$  is the viscosity of the fluid;
- $m^-$  and  $\beta^-$  are positive physical coefficients:  $\beta^- = 1 - K_b^-/K_s^-$  and  $m^- = \left[ \phi^-/K_f^- + (\beta^- - \phi^-)/K_s^- \right]^{-1}$ , where  $K_s^-$  is the bulk modulus of the solid,  $K_f^-$  is the bulk modulus of the fluid and  $K_b^-$  is the frame bulk modulus;
- $\mu^-$  is the frame shear modulus, and  $\lambda^- = K_b^- - 2\mu^-/3$  is the Lamé constant.

### 1.3 Transmission conditions

Let  $\mathbf{n}$  be the unitary normal vector of  $\Gamma$  outwardly directed to  $\Omega^-$ . The transmission conditions on the interface between the acoustic and porous medium are [5]:

$$\begin{cases} \mathbf{W}^- \cdot \mathbf{n} = (\mathbf{U}^+ - \mathbf{U}_s^-) \cdot \mathbf{n}, \\ P^- = P^+, \\ \Sigma^- \mathbf{n} = -P^+ \mathbf{n}. \end{cases} \quad (3)$$

### 1.4 The Green problem

We won't compute directly the solution to (1-2-3) but the solution to the following Green problem:

$$\ddot{p}^+ - V^{+2} \Delta p^+ = \delta_x \delta_{y-h} \delta_t, \quad \text{in } \Omega^+ \times ]0, T], \quad (4a)$$

$$\ddot{\mathbf{u}}^+ = -\frac{1}{\rho^+} \nabla p^+, \quad \text{in } \Omega^+ \times ]0, T], \quad (4b)$$

$$\rho^- \ddot{\mathbf{u}}_s^- + \rho_f^- \ddot{\mathbf{w}}^- - \nabla \cdot \boldsymbol{\sigma}^- = 0, \quad \text{in } \Omega^- \times ]0, T], \quad (5a)$$

$$\rho_f^- \ddot{\mathbf{u}}_s^- + \rho_w^- \ddot{\mathbf{w}}^- + \frac{1}{\mathcal{K}^-} \dot{\mathbf{w}}^- + \nabla p^- = 0, \quad \text{in } \Omega^- \times ]0, T], \quad (5b)$$

$$\boldsymbol{\sigma}^- = \lambda^- \nabla \cdot \mathbf{u}_s^- \mathbf{I}_2 + 2\mu^- \varepsilon(\mathbf{u}_s^-) - \beta^- p^- \mathbf{I}_2, \quad \text{in } \Omega^- \times ]0, T], \quad (5c)$$

$$\frac{1}{m^-} p^- + \beta^- \nabla \cdot \mathbf{u}_s^- + \nabla \cdot \mathbf{w}^- = 0, \quad \text{in } \Omega^- \times ]0, T], \quad (5d)$$

$$\mathbf{w}^- \cdot \mathbf{n} = (\mathbf{u}^+ - \mathbf{u}_s^-) \cdot \mathbf{n}, \quad \text{on } \Gamma \times ]0, T] \quad (6a)$$

$$p^- = p^+, \quad \text{on } \Gamma \times ]0, T] \quad (6b)$$

$$\boldsymbol{\sigma}^- \mathbf{n} = -p^+ \mathbf{n}. \quad \text{on } \Gamma \times ]0, T] \quad (6c)$$

The solution to (1-2-3) is then computed from the solution to the Green Problem thanks to a convolution by the source function. For instance we have:

$$P^+(x, y, t) = p^+(x, y, \cdot) * f(\cdot) = \int_0^t p^+(x, y, \tau) f(t - \tau) d\tau$$

(we have similar relations for the other unknowns). We also suppose that the poroelastic medium is non dissipative, i.e the viscosity  $\eta^- = 0$ . Using the equations (5c, 5d) we can eliminate  $\sigma^-$  and  $p^-$  in (5) and we obtain the equivalent system:

$$\begin{cases} \rho^- \ddot{\mathbf{u}}_s^- + \rho_f^- \ddot{\mathbf{w}}^- - \alpha^- \nabla(\nabla \cdot \mathbf{u}_s^-) + \mu^- \nabla \times (\nabla \times \mathbf{u}_s^-) - m^- \beta^- \nabla(\nabla \cdot \mathbf{w}^-) = 0, \\ \rho_f^- \ddot{\mathbf{u}}_s^- + \rho_w^- \ddot{\mathbf{w}}^- - m^- \beta^- \nabla(\nabla \cdot \mathbf{u}_s^-) - m^- \nabla(\nabla \cdot \mathbf{w}^-) = 0, \end{cases} \quad (7)$$

with  $\alpha^- = \lambda^- + 2\mu^- + m^- \beta^{-2}$ .

And using the equation (4b) the transmission conditions (6) are rewritten as:

$$\begin{cases} \ddot{u}_{sy}^- + \ddot{w}_y^- = -\frac{1}{\rho^+} \partial_y p^+, \\ -m^- \beta^- \nabla \cdot \mathbf{u}_s^- - m^- \nabla \cdot \mathbf{w}^- = p^+, \\ \partial_y u_{sx}^- + \partial_x u_{sy}^- = 0, \\ (\lambda^- + m^- \beta^{-2}) \nabla \cdot \mathbf{u}_s^- + 2\mu^- \partial_y u_{sy}^- + m^- \beta^- \nabla \cdot \mathbf{w}^- = -p^+. \end{cases} \quad (8)$$

We split the displacement fields  $\mathbf{u}_s^-$  and  $\mathbf{u}_f^-$  into irrotational and isovolumic fields (P-wave and S-wave):

$$\mathbf{u}_s^- = \nabla \Theta_u^- + \nabla \times \Psi_u^- ; \quad \mathbf{w}^- = \nabla \Theta_w^- + \nabla \times \Psi_w^- . \quad (9)$$

We can then rewrite system (7) in the following form:

$$\begin{cases} A^- \ddot{\Theta}^- - B^- \Delta \Theta^- = 0, & y < 0 \\ \ddot{\Psi}_u^- - V_S^{-2} \Delta \Psi_u^- = 0, & y < 0 \\ \ddot{\Psi}_w^- = -\frac{\rho_f^-}{\rho_w^-} \ddot{\Psi}_u^-, & y < 0 \end{cases} \quad (10)$$

where  $\Theta^- = (\Theta_u^-, \Theta_w^-)^t$ ,  $A^-$  and  $B^-$  are  $2 \times 2$  symmetric matrices:

$$A^- = \begin{pmatrix} \rho^- & \rho_f^- \\ \rho_f^- & \rho_w^- \end{pmatrix} ; \quad B^- = \begin{pmatrix} \lambda^- + 2\mu^- + m^- (\beta^-)^2 & m^- \beta^- \\ m^- \beta^- & m^- \end{pmatrix},$$

and

$$V_S^- = \sqrt{\frac{\mu \rho_w^-}{\rho^- \rho_w^- - \rho_f^{-2}}}$$

is the S-wave velocity.

We multiply the first equation of system (10) by the inverse of  $A$ . The matrix  $A^{-1}B$  is diagonalizable:  $A^{-1}B = \mathcal{P}D\mathcal{P}^{-1}$ , where  $\mathcal{P}$  is the change-of-coordinates matrix,  $D = \text{diag}(V_{P_f}^{-2}, V_{P_s}^{-2})$  is the diagonal matrix similar to  $A^{-1}B$ ,  $V_{P_f}^-$  and  $V_{P_s}^-$  are respectively the fast P-wave velocity and the slow P-wave velocity ( $V_{P_s}^- < V_{P_f}^-$ ).

Using the change of variables  $\Phi = (\Phi_{Pf}, \Phi_{Ps})^t = \mathcal{P}^{-1}\Theta$ , we obtain the uncoupled system on fast P-waves, slow P-waves and S-waves:

$$\begin{cases} \ddot{\Phi} - D\Delta\Phi = 0, & y < 0 \\ \ddot{\Psi}_u - V_S^{-2}\Delta\Psi_u = 0, & y < 0 \\ \Psi_w = -\frac{\rho_f^-}{\rho_w}\Psi_u, & y < 0 \end{cases} \quad (11)$$

Finally, we obtain the Green problem equivalent to (4,5,6):

$$\begin{cases} \ddot{p}^+ - V^{+2}\Delta p^+ = \delta_x\delta_{y-h}\delta_t, & y > 0 \\ \ddot{\Phi}_i^- - V_i^{-2}\Delta\Phi_i^- = 0, \quad i \in \{Pf, Ps, S\} & y < 0 \\ \mathcal{B}(p^+, \Phi_{Pf}^-, \Phi_{Ps}^-, \Phi_S^-) = 0, & y = 0 \end{cases} \quad (12)$$

where we have set  $\Phi_S = \Psi_u$  in order to have similar notations for the  $Pf$ ,  $Ps$  and  $S$  waves. The operator  $\mathcal{B}$  represents the transmission conditions on  $\Gamma$ :

$$\mathcal{B} \begin{pmatrix} p^+ \\ \Phi_{Pf}^- \\ \Phi_{Ps}^- \\ \Phi_S^- \end{pmatrix} = \begin{bmatrix} \frac{1}{\rho^+}\partial_y & (\mathcal{P}_{11} + \mathcal{P}_{21})\partial_{ytt}^3 & (\mathcal{P}_{12} + \mathcal{P}_{22})\partial_{ytt}^3 & (\frac{\rho_f^-}{\rho_w} - 1)\partial_{xtt}^3 \\ 1 & \frac{m^-(\beta^-\mathcal{P}_{11} + \mathcal{P}_{21})}{V_{Pf}^2}\partial_{tt}^2 & \frac{m^-(\beta^-\mathcal{P}_{12} + \mathcal{P}_{22})}{V_{Ps}^2}\partial_{tt}^2 & 0 \\ 0 & 2\mathcal{P}_{11}\partial_{xy}^2 & 2\mathcal{P}_{12}\partial_{xy}^2 & \partial_{yy}^2 - \partial_{xx}^2 \\ 1 & \mathcal{B}_{42} & \mathcal{B}_{43} & -2\mu^-\partial_{xy}^2 \end{bmatrix} \begin{bmatrix} p^+ \\ \Phi_{Pf}^- \\ \Phi_{Ps}^- \\ \Phi_S^- \end{bmatrix}$$

where  $\mathcal{P}_{i,j}$ ,  $i, j = 1, 2$  are the components of the change-of-coordinates matrix  $\mathcal{P}$ ,  $\mathcal{B}_{41}$  and  $\mathcal{B}_{43}$  are given by:

$$\mathcal{B}_{42} = \frac{(\lambda^- + m^-\beta^{-2})\mathcal{P}_{11} + m^-\beta^-\mathcal{P}_{21}}{V_{Pf}^{-2}}\partial_{tt}^2 + 2\mu^-\mathcal{P}_{11}\partial_{yy}^2,$$

$$\mathcal{B}_{43} = \frac{(\lambda^- + m^-\beta^{-2})\mathcal{P}_{12} + m^-\beta^-\mathcal{P}_{22}}{V_{Ps}^{-2}}\partial_{tt}^2 + 2\mu^-\mathcal{P}_{12}\partial_{yy}^2.$$

To obtain this operator we have used the transmission conditions (8), the change of variables (9) and the uncoupled system (11).

Moreover, we can determine the solid displacement  $\mathbf{u}_s^-$  by using the change of variables (9) and the fluid displacement  $\mathbf{u}^+$  by using (4b).

## 2 Expression of the analytical solution

To state our results, we need the following notations and definitions:

1. **Definition of the complex square root.** For  $q \in \mathbb{C} \setminus \mathbb{R}^-$ , we use the following definition of the square root  $g(q) = q^{1/2}$ :

$$g(q)^2 = q \quad \text{and} \quad \Re[g(q)] > 0.$$

The branch cut of  $g(q)$  in the complex plane will thus be the half-line defined by  $\{q \in \mathbb{R}^-\}$  (see Fig. 2). In the following, we use the abuse of notation  $g(q) = i\sqrt{-q}$  for  $q \in \mathbb{R}^-$ .

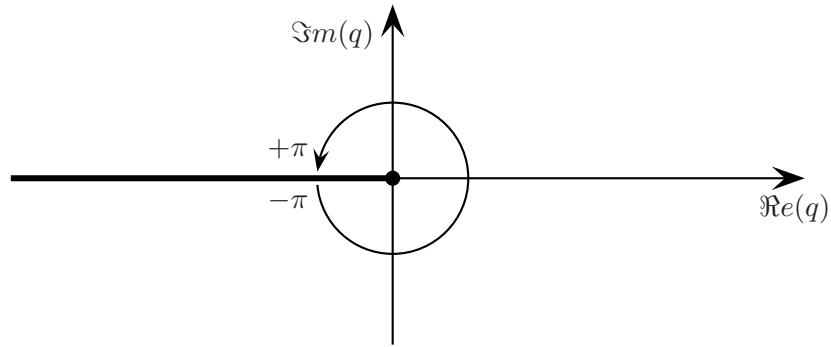


Figure 2: Definition of the function  $x \mapsto (x)^{1/2}$

2. **Definition of the functions  $\kappa^+$  and  $\kappa_i^-$ .** For  $i \in \{Pf, Ps, S\}$  and  $q \in \mathbb{C}$ , we define the functions

$$\kappa^+ := \kappa^+(q) = \left( \frac{1}{V^{+2}} + q^2 \right)^{1/2} \quad \text{and} \quad \kappa_i^- := \kappa_i^-(q) = \left( \frac{1}{V_i^{-2}} + q^2 \right)^{1/2}.$$

3. **Definition of the reflection and transmission coefficients.** For a given  $q \in \mathbb{C}$ , we denote by  $\mathcal{R}(q)$ ,  $\mathcal{T}_{Pf}(q)$ ,  $\mathcal{T}_{Ps}(q)$  and  $\mathcal{T}_S(q)$  the solution to the linear system

$$\mathcal{A}(q) \begin{bmatrix} \mathcal{R}(q) \\ \mathcal{T}_{Pf}(q) \\ \mathcal{T}_{Ps}(q) \\ \mathcal{T}_S(q) \end{bmatrix} = -\frac{1}{2\kappa^+ V^{+2}} \begin{bmatrix} \frac{\kappa^+(q)}{\rho^+} \\ 1 \\ 0 \\ 1 \end{bmatrix}, \quad (13)$$

where the matrix  $\mathcal{A}(q)$  is defined for  $q \in \mathbb{C}$  by:

$$\mathcal{A}(q) = \begin{bmatrix} -\frac{\kappa^+(q)}{\rho^+} & \kappa_{Pf}^-(q)(\mathcal{P}_{11} + \mathcal{P}_{21}) & \kappa_{Ps}^-(q)(\mathcal{P}_{12} + \mathcal{P}_{22}) & iq \left( 1 - \frac{\rho_f^-}{\rho_w} \right) \\ 1 & \frac{m^-}{V_{Pf}^{-2}} (\beta^- \mathcal{P}_{11} + \mathcal{P}_{21}) & \frac{m^-}{V_{Ps}^{-2}} (\beta^- \mathcal{P}_{12} + \mathcal{P}_{22}) & 0 \\ 0 & -2iq \kappa_{Pf}^-(q) \mathcal{P}_{11} & -2iq \kappa_{Ps}^-(q) \mathcal{P}_{12} & (\kappa_S^{-2}(q) + q^2) \\ 1 & \mathcal{A}_{4,2}(q) & \mathcal{A}_{4,3}(q) & 2iq \mu^- \kappa_S^-(q) \end{bmatrix},$$

RR n° 6509

with

$$A_{4,2}(q) = \frac{(\lambda^- + m^- \beta^{-2}) \mathcal{P}_{11} + m^- \beta^- \mathcal{P}_{21}}{V_{Pf}^{-2}} + 2\mu^- \kappa_{Pf}^-(q)^2 \mathcal{P}_{11},$$

$$A_{4,3}(q) = \frac{(\lambda^- + m^- \beta^{-2}) \mathcal{P}_{12} + m^- \beta^- \mathcal{P}_{22}}{V_{Ps}^{-2}} + 2\mu^- \kappa_{Ps}^-(q)^2 \mathcal{P}_{12},$$

We also denote by  $V_{\max}$  the greatest velocity in the two media:  $V_{\max} = \max(V^+, V_{Pf}, V_{Ps}, V_S)$ .

We can now present the expression of the solution to the Green Problem:

**Theorem 2.1.** *The pressure and the displacement in the top medium are given by*

$$p^+(x, y, t) = p_{inc}^+(x, y, t) + p_{ref}^+(x, y, t) \text{ and } \mathbf{u}^+(x, y, t) = \int_0^t \nu_{inc}^+(x, y, \tau) d\tau + \int_0^t \nu_{ref}^+(x, y, \tau) d\tau,$$

and the displacement in the bottom medium is given by

$$\mathbf{u}_s^- = \int_0^t \nu^-(x, y, \tau) d\tau \text{ with } \nu^- = \nu_{Pf}^- + \nu_{Ps}^- + \nu_S^-,$$

where

- $p_{inc}^+$  and  $\nu_{inc}^+$  are respectively the pressure and the velocity of the incident wave and satisfy:

$$\begin{cases} p_{inc}^+(x, y, t) &= \frac{1}{2\pi V^{+2} \sqrt{t^2 - t_0^2}}, \\ \nu_{inc,x}^+(x, y, t) &= \frac{tx}{2\pi V^{+2} \rho^{+r} \sqrt{t^2 - t_0^2}}, \\ \nu_{inc,y}^+(x, y, t) &= \frac{t(y-h)}{2\pi V^{+2} \rho^{+r} \sqrt{t^2 - t_0^2}}, \end{cases} \text{ if } t > t_0$$

$$p_{inc}(x, y, t) = 0 \text{ and } \nu_{inc}(x, y, t) = 0, \quad \text{else.}$$

We set here  $r = (x^2 + (y-h)^2)^{1/2}$  and  $t_0 = r/V^+$  denotes the arrival time of the incident wave.

- $p_{ref}^+$  and  $\nu_{ref}^+$  are respectively the pressure and the velocity of the reflected wave and satisfy:

$$\left\{ \begin{array}{l} p_{ref}^+(x, y, t) = -\frac{\Im m [\kappa^+(v(t))\mathcal{R}(v(t))]}{\pi\sqrt{t_0^2 - t^2}}, \\ \nu_{ref,x}^+(x, y, t) = -\frac{\Im m [i v(t)\kappa^+(v(t))\mathcal{R}(v(t))]}{\pi\rho^+\sqrt{t_0^2 - t^2}}, \\ \nu_{ref,y}^+(x, y, t) = -\frac{\Im m [\kappa^{+2}(v(t))\mathcal{R}(v(t))]}{\pi\rho^+\sqrt{t_0^2 - t^2}}, \end{array} \right. \quad \text{if } t_h < t \leq t_0 \text{ and } \frac{x}{r} > \frac{V^+}{V_{\max}},$$

$$\left\{ \begin{array}{l} p_{ref}^+(x, y, t) = \frac{\Re e [\kappa^+(\gamma(t))\mathcal{R}(\gamma(t))]}{\pi\sqrt{t_0^2 - t^2}}, \\ \nu_{ref,x}^+(x, y, t) = \frac{\Re e [i \gamma(t)\kappa^+(\gamma(t))\mathcal{R}(\gamma(t))]}{\pi\rho^+\sqrt{t_0^2 - t^2}}, \\ \nu_{ref,y}^+(x, y, t) = \frac{\Re e [\kappa^{+2}(\gamma(t))\mathcal{R}(\gamma(t))]}{\pi\rho^+\sqrt{t^2 - t_0^2}}, \end{array} \right. \quad \text{if } t > t_0,$$

$$p_{ref}(x, y, t) = 0 \text{ and } \nu_{ref}(x, y, t) = 0, \quad \text{else.}$$

We set here  $r = (x^2 + (y + h)^2)^{1/2}$ ,  $t_0 = r/V^+$  denotes the arrival time of the reflected volume wave,

$$t_h = (y + h) \sqrt{\frac{1}{V^{+2}} - \frac{1}{V_{\max}^2}} + \frac{|x|}{V_{\max}},$$

denotes the arrival time of the reflected head wave and the complex functions  $v := v(t)$  and  $\gamma := \gamma(t)$  are defined by

$$\left\{ \begin{array}{l} v(t) = -i \left( \frac{y + h}{r} \sqrt{\frac{1}{V^{+2}} - \frac{t^2}{r^2}} + \frac{xt}{r^2} \right) \quad \text{for } t_h < t \leq t_0 \text{ and } x < 0, \\ v(t) = i \left( \frac{y + h}{r} \sqrt{\frac{1}{V^{+2}} - \frac{t^2}{r^2}} - \frac{xt}{r^2} \right) \quad \text{for } t_h < t \leq t_0 \text{ and } x \geq 0, \end{array} \right.$$

and

$$\gamma(t) = -i \frac{x}{r^2} t + \frac{y + h}{r} \sqrt{\frac{t^2}{r^2} - \frac{1}{V^{+2}}} \quad \text{for } t > t_0.$$

- $\nu_{Pf}^-$  is the velocity of the transmitted Pf wave and satisfies:

$$\left\{ \begin{array}{l} \nu_{Pf,x}^-(x, y, t) = -\frac{\mathcal{P}_{11}}{\pi} \Re e \left[ i v(t) \mathcal{T}_{Pf}(v(t)) \frac{dv}{dt}(t) \right], \\ \nu_{Pf,y}^-(x, y, t) = \frac{\mathcal{P}_{11}}{\pi} \Re e \left[ \kappa_{Pf}^-(v(t)) \mathcal{T}_{Pf}(v(t)) \frac{dv}{dt}(t) \right], \end{array} \right. \quad \begin{array}{l} \text{if } t_h < t \leq t_0 \\ \text{and } |\Im m(v(t_0))| > \frac{1}{V_{\max}} \end{array}$$

$$\left\{ \begin{array}{l} \nu_{Pf,x}^-(x, y, t) = -\frac{\mathcal{P}_{11}}{\pi} \Re e \left[ i \gamma(t) \mathcal{T}_{Pf}(\gamma(t)) \frac{d\gamma}{dt}(t) \right], \\ \nu_{Pf,y}^-(x, y, t) = \frac{\mathcal{P}_{11}}{\pi} \Re e \left[ \kappa_{Pf}^-(\gamma(t)) \mathcal{T}_{Pf}(\gamma(t)) \frac{d\gamma}{dt}(t) \right], \end{array} \right. \quad \text{if } t > t_0$$

$$\nu_{Pf}^-(x, y, t) = 0, \quad \text{else.}$$

Here  $t_0$  denotes the arrival time of the Pf wave (its calculation is detailed in appendix) and  $t_h$  is the arrival time of the Pf head wave:

$$t_h = -y \sqrt{\frac{1}{V_{Pf}^{-2}} - \frac{1}{V_{\max}^2}} + h \sqrt{\frac{1}{V^{+2}} - \frac{1}{V_{\max}^2}} + \frac{|x|}{V_{\max}}.$$

For  $t_h < t \leq t_0$ , the function  $v := v(t)$  is defined as the only root of

$$q \in \mathbb{C} \mapsto \mathcal{F}(q, t) = -y \left( \frac{1}{V_{Pf}^{-2}} + q^2 \right)^{1/2} + h \left( \frac{1}{V^{+2}} + q^2 \right)^{1/2} + iqx - t,$$

such that  $\Im m \left( x \frac{dv(t)}{dt} \right) \leq 0$ . For  $t > t_0$ , the function  $\gamma := \gamma(t)$  is defined as the only root of  $q \in \mathbb{C} \mapsto \mathcal{F}(q, t)$  whose real part is positive.

- $\nu_{Ps}^-$  is the velocity of the transmitted Ps wave and satisfies:

$$\left\{ \begin{array}{l} \nu_{Ps,x}^-(x, y, t) = -\frac{\mathcal{P}_{12}}{\pi} \Re e \left[ i v(t) \mathcal{T}_{Ps}(v(t)) \frac{dv}{dt}(t) \right], \\ \nu_{Ps,y}^-(x, y, t) = \frac{\mathcal{P}_{12}}{\pi} \Re e \left[ \kappa_{Ps}^-(v(t)) \mathcal{T}_{Ps}(v(t)) \frac{dv}{dt}(t) \right], \end{array} \right. \quad \begin{array}{l} t_h < t \leq t_0 \\ \text{and } |\Im m(v(t_0))| > \frac{1}{V_{\max}}, \end{array}$$

$$\left\{ \begin{array}{l} \nu_{Ps,x}^-(x, y, t) = -\frac{\mathcal{P}_{12}}{\pi} \Re e \left[ i \gamma(t) \mathcal{T}_{Ps}(\gamma(t)) \frac{d\gamma}{dt}(t) \right], \\ \nu_{Ps,y}^-(x, y, t) = \frac{\mathcal{P}_{12}}{\pi} \Re e \left[ \kappa_{Ps}^-(\gamma(t)) \mathcal{T}_{Ps}(\gamma(t)) \frac{d\gamma}{dt}(t) \right], \end{array} \right. \quad \text{if } t > t_0,$$

$$\nu_{Ps}^-(x, y, t) = 0, \quad \text{else.}$$

Here  $t_0$  denotes the arrival time of the Ps wave and  $t_h$  is the arrival time of the Ps head wave:

$$t_h = -y \sqrt{\frac{1}{V_{Ps}^{-2}} - \frac{1}{V_{\max}^2}} + h \sqrt{\frac{1}{V^{+2}} - \frac{1}{V_{\max}^2}} + \frac{|x|}{V_{\max}}.$$

For  $t_h < t \leq t_0$ , the function  $v := v(t)$  is defined as the only root of

$$q \in \mathbb{C} \mapsto \mathcal{F}(q, t) = -y \left( \frac{1}{V_{Ps}^{-2}} + q^2 \right)^{1/2} + h \left( \frac{1}{V^{+2}} + q^2 \right)^{1/2} + iqx - t,$$

such that  $\Im m \left( x \frac{dv(t)}{dt} \right) \leq 0$ . For  $t > t_0$ , the function  $\gamma := \gamma(t)$  is defined as the only root of  $q \in \mathbb{C} \mapsto \mathcal{F}(q, t)$  whose real part is positive.

- $\nu_S^-$  is the velocity of the transmitted  $S$  wave and satisfies:

$$\begin{cases} \nu_{S,x}^-(x, y, t) = \frac{1}{\pi} \Re e \left[ \kappa_S^-(v(t)) \mathcal{I}_S(v(t)) \frac{dv}{dt}(t) \right], & \text{if } t_h < t \leq t_0 \\ \nu_{S,y}^-(x, y, t) = \frac{1}{\pi} \Re e \left[ i v(t) \mathcal{I}_S(v(t)) \frac{dv}{dt}(t) \right], & \text{and } |\Im m(v(t_0))| > \frac{1}{V_{\max}}, \end{cases}$$

$$\begin{cases} \nu_{S,x}^-(x, y, t) = \frac{1}{\pi} \Re e \left[ \kappa_S^-(\gamma(t)) \mathcal{I}_S(\gamma(t)) \frac{d\gamma}{dt}(t) \right], \\ \nu_{S,y}^-(x, y, t) = \frac{1}{\pi} \Re e \left[ i \gamma(t) \mathcal{I}_S(\gamma(t)) \frac{d\gamma}{dt}(t) \right], \end{cases} \quad \text{if } t > t_0,$$

$$\nu_{S,x}^-(x, y, t) = 0, \quad \text{else.}$$

Here  $t_0$  denotes the arrival time of the  $S$  wave and  $t_h$  is the arrival time of the  $S$  head wave:

$$t_h = -y \sqrt{\frac{1}{V_S^{-2}} - \frac{1}{V_{\max}^2}} + h \sqrt{\frac{1}{V^{+2}} - \frac{1}{V_{\max}^2}} + \frac{|x|}{V_{\max}}.$$

For  $t_h < t \leq t_0$ , the function  $v := v(t)$  is defined as the only root of

$$q \in \mathbb{C} \mapsto \mathcal{F}(q, t) = -y \left( \frac{1}{V_S^{-2}} + q^2 \right)^{1/2} + h \left( \frac{1}{V^{+2}} + q^2 \right)^{1/2} + iqx - t,$$

such that  $\Im m \left( x \frac{dv(t)}{dt} \right) \leq 0$ . For  $t > t_0$ , the function  $\gamma := \gamma(t)$  is defined as the only root of  $q \in \mathbb{C} \mapsto \mathcal{F}(q, t)$  whose real part is positive.

**Remark 2.1.** For the practical computations of the displacement, we won't have to explicitly compute the primitive of the velocities  $\nu$ , which would be rather tedious, since

$$\left( \int_0^t \nu(\tau) d\tau \right) * f = \nu * \left( \int_0^t f(\tau) d\tau \right).$$

Therefore, we'll only have to compute the primitive of the source function  $f$ .



### 3 Proof of the theorem

To prove the theorem, we use the Cagniard-de Hoop method (see [4, 6, 15, 14, 12]), which consists of two steps:

1. We apply a Laplace transform in time,

$$\tilde{u}(x, y, s) = \int_0^{+\infty} u(x, y, t) e^{-st} dt,$$

and a Fourier transform in the  $x$  variable,

$$\hat{u}(k_x, y, s) = \int_{-\infty}^{+\infty} \tilde{u}(x, y, s) e^{ik_x x} dx$$

to (12) in order to obtain an ordinary differential system whose solution  $\hat{\mathcal{G}}(k_x, y, s)$  can be explicitly computed (§ 3.1);

2. we apply an inverse Fourier transform in the  $x$  variable to  $\mathcal{G}$ :

$$\tilde{\mathcal{G}}(x, y, s) = \frac{1}{2\pi} \int_{-\infty}^{+\infty} \hat{\mathcal{G}}(k_x, y, s) e^{-ik_x x} dk_x.$$

and, using tools of complex analysis, we turn this inverse Fourier transform into the Laplace transform of some function  $\mathcal{H}(\S, \dagger, \sqcup)$ :

$$\tilde{\mathcal{G}}(x, y, s) = \frac{1}{2\pi} \int_0^{+\infty} \mathcal{H}(x, y, t) e^{-st} dt.$$

Then, using the injectivity of the Laplace transform, we identify  $\mathcal{G}(x, y, t)$  to  $\mathcal{H}(x, y, t)$  (§ 3.2).

#### 3.1 The solution in the Laplace-Fourier plane

Let us first apply a Laplace transform in time and a Fourier transform in the  $x$  variable to (12) to obtain

$$\left\{ \begin{array}{ll} \left( \frac{s^2}{V^{+2}} + k_x^2 \right) \hat{p}^+ - \frac{\partial^2 \hat{p}^+}{\partial y^2} = \frac{\delta(y-h)}{V^{+2}}, & y > 0, \\ \left( \frac{s^2}{V_i^{-2}} + k_x^2 \right) \hat{\Phi}_i^- - \frac{\partial^2 \hat{\Phi}_i^-}{\partial y^2} = 0, \quad i \in \{Pf, Ps, S\} & y < 0, \\ \hat{\mathcal{B}}(\hat{p}^+, \hat{\Phi}_{Pf}^-, \hat{\Phi}_{Ps}^-, \hat{\Phi}_S^-) = 0 & y = 0, \end{array} \right. \quad (14)$$

where  $\hat{\mathcal{B}}$  is the Laplace-Fourier transform of the operator  $\mathcal{B}$ .

From the two first equations of (14), we deduce that the solution  $(\hat{p}^+, (\hat{\Phi}_i^-)_{i \in \{Pf, Ps, S\}})$  is

such that

$$\left\{ \begin{array}{l} \hat{p}^+ = \hat{p}_{\text{inc}}^+ + \hat{p}_{\text{ref}}^+, \\ \hat{p}_{\text{inc}}^+(k_x, y, s) = \frac{e^{-s|y-h|\left(\frac{1}{V+2} + \frac{k_x^2}{s^2}\right)^{1/2}}}{sV+2 \left(\frac{1}{V+2} + \frac{k_x^2}{s^2}\right)^{1/2}}, \\ \hat{p}_{\text{ref}}^+(k_x, y, s) = R(k_x, s) e^{-sy\left(\frac{1}{V+2} + \frac{k_x^2}{s^2}\right)^{1/2}}, \\ \hat{\Phi}_i^-(k_x, y, s) = T_i(k_x, s) e^{sy\left(\frac{1}{V_i-2} + \frac{k_x^2}{s^2}\right)^{1/2}}, \quad i \in \{Pf, Ps, S\}. \end{array} \right. \quad (15)$$

where the coefficients  $R$  and  $T_i$  are computed by using the last equation of (14):

$$\hat{\mathcal{B}}(\hat{p}_{\text{ref}}^+, \hat{\Phi}_{Pf}^-, \hat{\Phi}_{Ps}^-, \hat{\Phi}_S^-) = -\hat{\mathcal{B}}(\hat{p}_{\text{inc}}^+, 0, 0, 0).$$

Using the expressions of  $\hat{p}_{\text{inc}}^+$ ,  $\hat{p}_{\text{ref}}^+$  and  $\hat{\Phi}_i^-$ , we obtain that  $R(k_x, s)$ ,  $T_{Pf}(k_x, s)$ ,  $T_{Ps}(k_x, s)$ ,  $T_S(k_x, s)$  are solution to

$$\mathcal{A}\left(\frac{k_x}{s}\right) \begin{bmatrix} sR(k_x, s) \\ s^3T_{Pf}(k_x, s) \\ s^3T_{Ps}(k_x, s) \\ s^3T_S(k_x, s) \end{bmatrix} = -\frac{e^{-sh\kappa^+\left(\frac{k_x}{s}\right)}}{2V+2\kappa^+\left(\frac{k_x}{s}\right)} \begin{bmatrix} \kappa^+\left(\frac{k_x}{s}\right) \\ \rho^+ \\ 1 \\ 0 \\ 1 \end{bmatrix}. \quad (16)$$

From the definition of the functions  $\mathcal{R}(q)$ ,  $\mathcal{T}_{Pf}(q)$ ,  $\mathcal{T}_{Ps}(q)$  and  $\mathcal{T}_S(q)$  we deduce that

$$\begin{bmatrix} \mathcal{R}\left(\frac{k_x}{s}\right) \\ \mathcal{T}_{Pf}\left(\frac{k_x}{s}\right) \\ \mathcal{T}_{Ps}\left(\frac{k_x}{s}\right) \\ \mathcal{T}_S\left(\frac{k_x}{s}\right) \end{bmatrix} = \begin{bmatrix} sR(k_x, s) \\ s^3T_{Pf}(k_x, s) \\ s^3T_{Ps}(k_x, s) \\ s^3T_S(k_x, s) \end{bmatrix} e^{sh\kappa^+\left(\frac{k_x}{s}\right)}. \quad (17)$$

Finally, we rewrite  $\hat{p}_{\text{inc}}^+$ ,  $\hat{p}_{\text{ref}}^+$  and  $\hat{\Phi}_i^-$  under the form

$$\left\{ \begin{array}{l} \hat{p}^+ = \hat{p}_{\text{inc}}^+ + \hat{p}_{\text{ref}}^+, \\ \hat{p}_{\text{inc}}^+(k_x, y, s) = \frac{1}{sV+2\kappa^+\left(\frac{k_x}{s}\right)} e^{-s|y-h|\kappa^+\left(\frac{k_x}{s}\right)}, \\ \hat{p}_{\text{ref}}^+(k_x, y, s) = \frac{1}{s}\mathcal{R}\left(\frac{k_x}{s}\right) e^{-s(y+h)\kappa^+\left(\frac{k_x}{s}\right)}, \\ \hat{\Phi}_i^-(k_x, y, s) = \frac{1}{s^3}\mathcal{T}_i\left(\frac{k_x}{s}\right) e^{-s(y\kappa_i^-\left(\frac{k_x}{s}\right)-h\kappa^+\left(\frac{k_x}{s}\right))}, \quad i \in \{Pf, Ps, S\}. \end{array} \right. \quad (18)$$

From (4b) and (9), we deduce the expression of the displacement field:

$$\left\{ \begin{array}{l} \hat{u}^+ = \hat{u}_{\text{inc}}^+ + \hat{u}_{\text{ref}}^+, \\ \hat{u}_{\text{inc},x}^+ = i \frac{k_x}{\rho^+ s^2} \hat{p}_{\text{inc}}^+, \quad \hat{u}_{\text{inc},y}^+ = \text{sign}(h-y) \frac{\kappa^+ \left(\frac{k_x}{s}\right)}{\rho^+ s} \hat{p}_{\text{inc}}^+, \\ \hat{u}_{\text{ref},x}^+ = i \frac{k_x}{\rho^+ s^2} \hat{p}_{\text{ref}}^+, \quad \hat{u}_{\text{ref},y}^+ = \frac{\kappa^+ \left(\frac{k_x}{s}\right)}{\rho^+ s} \hat{p}_{\text{ref}}^+, \\ \hat{u}_{sx}^- = -i k_x \mathcal{P}_{11} \hat{\Phi}_{P_f}^- - i k_x \mathcal{P}_{12} \hat{\Phi}_{P_s}^- + s \kappa_S^- \left(\frac{k_x}{s}\right) \Phi_S^-, \\ \hat{u}_{sy}^- = s \kappa_{P_f}^- \left(\frac{k_x}{s}\right) \mathcal{P}_{11} \hat{\Phi}_{P_f}^- + s \kappa_{P_s}^- \left(\frac{k_x}{s}\right) \mathcal{P}_{12} \hat{\Phi}_{P_s}^- + i k_x \Phi_S^- \end{array} \right. \quad (19)$$

In the following we only detail the computation of  $\hat{u}_{sx,P_s}^- = -i k_x \mathcal{P}_{12} \hat{\Phi}_{P_s}^-$ , since the computation of the other terms is very similar.

### 3.2 The Laplace transform of the solution

Let us now apply an inverse Fourier transform in the  $x$  variable to  $\hat{u}_{sx,P_s}^-$  and set  $k_x = qs$  to obtain

$$\tilde{u}_{sx,P_s}^- = - \int_{-\infty}^{+\infty} \frac{i q \mathcal{P}_{12}}{2s\pi} \mathcal{T}_{P_s}(q) e^{-s(-y\kappa_{P_s}^-(q) + h\kappa^+(q)) + i q x} dq = - \frac{\mathcal{P}_{12}}{2s\pi} \int_{-\infty}^{+\infty} \Xi(q) dq, \quad (20)$$

with  $\Xi(q) = i q \mathcal{T}_{P_s}(q) e^{-s(-y\kappa_{P_s}^-(q) + h\kappa^+(q)) + i q x}$ .

The key point of the Cagniard-de Hoop method is to turn this Fourier integral into a Laplace integral by finding a path  $\Gamma$  in the complex plane such that

$$-y\kappa_{P_s}^-(q) + h\kappa^+(q) + i q x = t \in \mathbb{R}^+, \forall q \in \Gamma.$$

This amounts to compute the roots  $q$  of the function

$$\mathcal{F}(q, t) = -y \left( \frac{1}{V_{P_s}^-} + q^2 \right)^{1/2} + h \left( \frac{1}{V^+} + q^2 \right)^{1/2} + i q x - t,$$

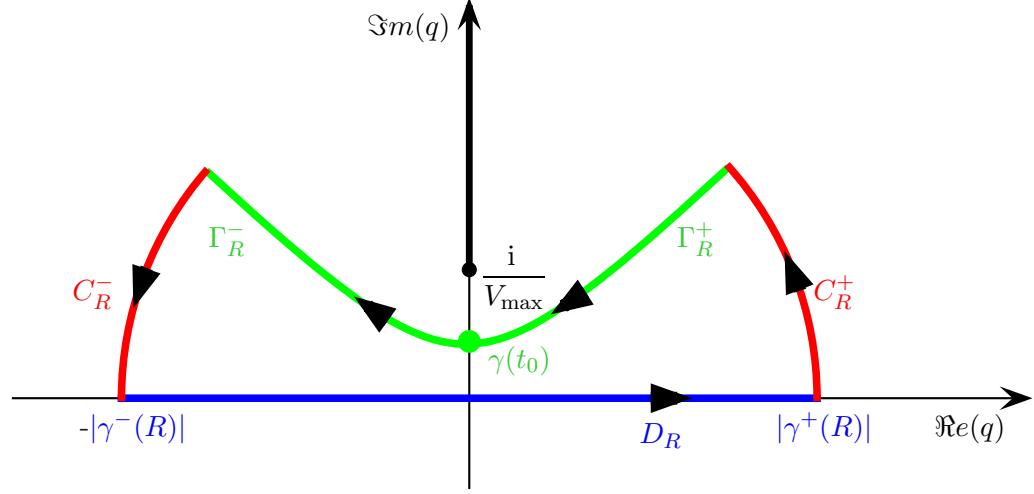
for  $t \in \mathbb{R}^+$ . We recall in appendix A some properties of the function  $\mathcal{F}$ ; from properties A.1, A.3 and A.2 we can define the function  $\gamma(t) \in \mathbb{C}$  for  $t > t_0$  as the only root of  $\mathcal{F}(., t)$  whose real part is positive, where  $t_0$  is the arrival time of the  $P_s$  volume wave (we recall in appendix B the practical computation of  $t_0$ ). Moreover, for a given  $R \in \mathbb{R}^+$ , we define

$$\Gamma_R^+ = \{p = \gamma(t) \mid t_0 < t < R\}, \Gamma_R^- = \{p = -\overline{\gamma(t)} \mid t_0 < t < R\} \text{ and } \Gamma^\pm = \lim_{R \rightarrow \infty} \Gamma_R^\pm.$$

We represent the paths  $\Gamma_R^\pm$  in Fig. 3 in the case  $x < 0$  (for  $x \geq 0$  the path would be similar but in the half plane  $\Im m(q) \leq 0$ ). The shape of  $\Gamma^\pm$  is given by the following property:

**Property 3.1.** *When  $R$  tends to infinity,  $\Gamma_R^\pm$  admits an asymptote of equation*

$$p = \frac{\pm(y-h) - ix}{(y-h)^2 + x^2}.$$

Figure 3: Integration path if  $|\gamma(t_0)| < 1/V_{\max}$ .

We now have to decide whether this path intersects the branch cuts of the functions  $\kappa^+$  and  $\kappa_i^-$ . From the definition of the complex square root, we deduce that the branch cuts of  $\kappa^+$  are the two half lines

$$\{q \in \mathbb{C} \mid \Re(q) = 0 \text{ and } |\Im(q)| \geq \frac{1}{V^+}\}$$

and the branch cuts of  $\kappa_i^-$  are the two half lines

$$\{q \in \mathbb{C} \mid \Re(q) = 0 \text{ and } |\Im(q)| \geq \frac{1}{V_i^-}\}.$$

and, since only  $\gamma(t_0)$  is purely imaginary, the path cross the branch cuts if and only if

$$|\gamma(t_0)| \geq \frac{1}{V_{\max}}.$$

We have then have to consider two possibilities:

- **if  $|\gamma(t_0)| < 1/V_{\max}$ :** then  $\Gamma_R$  does not intersect the branch cuts of the functions  $\kappa_i^-$  or  $\kappa^+$ . We define the segment  $D_R = \{p \in \mathbb{R}, |p| \leq |\gamma(R)|\}$  and we close the path by the two arcs of circle  $C_R^-$  and  $C_R^+$  of radius  $\gamma(R)$  linking  $\Gamma_R^\pm$  and  $D_R$  (see Fig.3). By Cauchy's theorem we have

$$\int_{D_R} \Xi(q) dq + \int_{C_R^+} \Xi(q) dq + \int_{\Gamma_R^-} \Xi(q) dq - \int_{\Gamma_R^+} \Xi(q) dq + \int_{C_R^-} \Xi(q) dq = 0,$$

and, using Jordan's lemma, we obtain:

$$\lim_{R \rightarrow \infty} \int_{C_R^\pm} \Xi(q) dq = 0.$$

so that

$$\int_{-\infty}^{+\infty} \Xi(q) dq = \int_{\Gamma^+} \Xi(q) dq - \int_{\Gamma^-} \Xi(q) dq.$$

Next, using the change of variable  $q = \gamma(t)$  on  $\Gamma^+$  and  $q = -\overline{\gamma(t)}$  on  $\Gamma^-$ , we end up with

$$\int_{-\infty}^{+\infty} \Xi(q) dq = \int_{t_0}^{+\infty} i \gamma(t) \mathcal{T}_{P_s}(\gamma(t)) \frac{d\gamma(t)}{dt} e^{-st} dt - \int_{t_0}^{+\infty} i \overline{\gamma(t)} \mathcal{T}_{P_s}(-\overline{\gamma(t)}) \frac{d\overline{\gamma(t)}}{dt} e^{-st} dt.$$

From the definition of  $\mathcal{T}_{P_s}$ , we check, after some calculation, that  $\mathcal{T}_{P_s}(-\overline{\gamma(t)}) = -\overline{\mathcal{T}_{P_s}(\gamma(t))}$  and

$$i \overline{\gamma(t)} \mathcal{T}_{P_s}(-\overline{\gamma(t)}) \frac{d\overline{\gamma(t)}}{dt} = -i \gamma(t) \mathcal{T}_{P_s}(\gamma(t)) \frac{d\gamma(t)}{dt},$$

so that

$$\begin{aligned} \tilde{u}_{s, P_s}^-(x, y, s) &= - \int_{t_0}^{+\infty} \frac{P_{12}}{s\pi} \Re e \left( i \gamma(t) \mathcal{T}_{P_s}(\gamma(t)) \frac{d\gamma(t)}{dt} \right) e^{-st} dt \\ &= \int_{t_0}^{+\infty} \left[ \int_0^t \nu_{s,x}^-(x, y, \tau) d\tau \right] e^{-st} dt, \end{aligned}$$

We conclude by using the injectivity of the Laplace transform that

$$u_{s, P_s}^-(x, y, t) = \int_0^t \nu_{s,x}^-(x, y, \tau) d\tau, .$$

**Remark 3.1.** *The computation of  $\frac{d\gamma(t)}{dt}$  is easily achieved by using the implicit function theorem:*

$$\frac{d\gamma(t)}{dt} = \frac{1}{-y \frac{\gamma(t)}{\left(\frac{1}{V_{P_s}^-} + \gamma^2(t)\right)^{1/2}} + h \frac{\gamma(t)}{\left(\frac{1}{V_{P_s}^+} + \gamma^2(t)\right)^{1/2}} + i x}$$

Since  $\mathcal{F}(\cdot, t)$  admits a double root at  $t = t_0$ , the function  $\frac{d\gamma(t)}{dt}$  is singular at this point, however this singularity behaves as [7]

$$\frac{\alpha}{\sqrt{t^2 - t_0^2}}$$

and can therefore be integrated.

- if  $|\gamma(t_0)| \leq 1/V_{\max}$ ; in this case, the path does intersect the branch cut and we have to consider an additional path  $\Upsilon$  to bypass the half-lines defined by

$$\left\{ q \in \mathbb{C} \mid \Re e(q) = 0 \text{ and } |\Im m(q)| \geq \frac{1}{V_{\max}} \right\}.$$

This path must obviously satisfy the condition

$$-y\kappa_{P_s}^-(q) + h\kappa_{P_s}^+(q) + iqx = t \in \mathbb{R}^+, \forall q \in \Upsilon.$$

If  $x < 0$ ,  $\Im m(\gamma(t_0)) \geq 0$  (property A.2), so that  $\gamma(t_0)$  lies on the branch cut

$$\left\{ q \in \mathbb{C} \mid \Re e(q) = 0 \text{ and } \Im m(q) > \frac{1}{V_{\max}} \right\}.$$

Therefore, using properties A.4 and A.5, we define  $v(t)$ , for  $t_h \leq t \leq t_0$ , as the only root of  $\mathcal{F}(\cdot, t)$  such that

$$\Im m \left( \frac{dv(t)}{dt} \right) = \Im m \left( -y \frac{v(t)}{\left( \frac{1}{V_{Ps}^{-2}} + v^2(t) \right)^{1/2}} + h \frac{v(t)}{\left( \frac{1}{V^{+2}} + v^2(t) \right)^{1/2}} + i x \right) > 0,$$

where

$$t_h = -y \sqrt{\frac{1}{V_{Ps}^{-2}} - \frac{1}{V_{\max}^2}} + h \sqrt{\frac{1}{V^{+2}} - \frac{1}{V_{\max}^2}} + \frac{|x|}{V_{\max}}.$$

If  $x > 0$ , we define  $v(t)$ , for  $t_h \leq t \leq t_0$ , as the only root of  $\mathcal{F}(\cdot, t)$  such that

$$\Im m \left( \frac{dv(t)}{dt} \right) = \Im m \left( -y \frac{v(t)}{\left( \frac{1}{V_{Ps}^{-2}} + v^2(t) \right)^{1/2}} + h \frac{v(t)}{\left( \frac{1}{V^{+2}} + v^2(t) \right)^{1/2}} + i x \right) < 0.$$

We are now able to define the paths  $\Upsilon_R^\pm$  and  $\Upsilon^\pm$  by:

$$\Upsilon_R^\pm = \left\{ v(t) \pm \frac{1}{R} \mid t_h < t < t_0 \right\} \text{ and } \Upsilon^\pm = \lim_{R \rightarrow +\infty} \Upsilon_R^\pm$$

We represent the paths  $\Gamma_R^\pm$  and  $\Upsilon_R^\pm$  in Fig. 4 in the case  $x < 0$  (for  $x \geq 0$  the path would be similar but in the half plane  $\Im m(q) \leq 0$ ). We define the segment

$$D_R = \{p \in \mathbb{R}, \mid |p| \leq |\gamma(R)|\}$$

and we close the path by the two arcs of circle  $C_R^-$  and  $C_R^+$  of radius  $\gamma(R)$  linking  $\Gamma_R^\pm$  and  $D_R$  and the half circle  $c_R$  linking  $\Upsilon_R^+$  to  $\Upsilon_R^-$  (see Fig.4). By Cauchy's theorem:

$$\begin{aligned} & \int_{D_R} \Xi(q) dq + \int_{C_R^+} \Xi(q) dq - \int_{\Gamma_R^+} \Xi(q) dq + \int_{\Gamma_R^-} \Xi(q) dq \\ & - \int_{\Upsilon_R^+} \Xi(q) dq + \int_{\Upsilon_R^-} \Xi(q) dq + \int_{C_R^-} \Xi(q) dq + \int_{c_R} \Xi(q) dq = 0. \end{aligned}$$

Using once again Jordan's Lemma, we prove that the integrals over  $C_R^-$ ,  $C_R^+$  and  $c_R$  vanish when  $R$  tends to infinity and that

$$\int_{-\infty}^{+\infty} \Xi(q) dq = \int_{\Gamma^+} \Xi(q) dq - \int_{\Gamma^-} \Xi(q) dq + \int_{\Upsilon^+} \Xi(q) dq - \int_{\Upsilon^-} \Xi(q) dq.$$

The calculation of the integral over  $\Gamma^\pm$  is done as in the first case and we only focus on the calculation over  $\Upsilon^\pm$ . Let us now use the change of variable  $q = v_{Ps}^-(t) - 1/R$  on  $\Upsilon_R^-$  and  $q = v_{Ps}^-(t) + 1/R$  on  $\Upsilon_R^+$  to obtain:

$$\begin{aligned} \int_{\Upsilon_R^-} \Xi(q) dq &= \int_{t_h}^{t_0} i \left( v(t) - \frac{1}{R} \right) \mathcal{T}_{Ps} \left( v(t) - \frac{1}{R} \right) \frac{dv(t)}{dt} e^{-st} dt \\ \int_{\Upsilon_R^+} \Xi(q) dq &= \int_{t_h}^{t_0} i \left( v(t) + \frac{1}{R} \right) \mathcal{T}_{Ps} \left( v(t) + \frac{1}{R} \right) \frac{dv(t)}{dt} e^{-st} dt. \end{aligned}$$

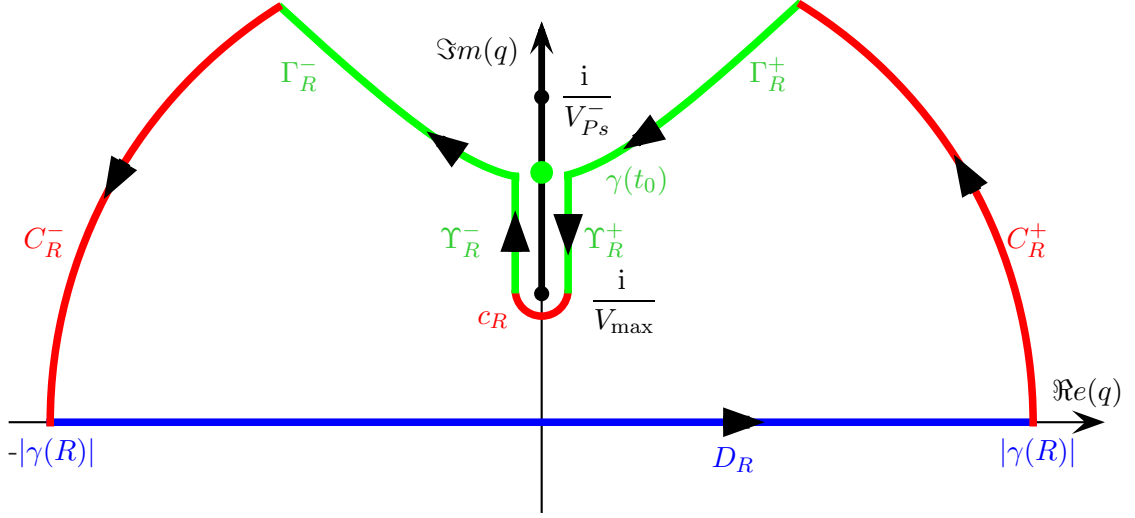


Figure 4: Integration path if  $|\gamma(t_0)| > 1/V_{\max}$ .

Because of the branch cut, it is clear that

$$\lim_{R \rightarrow +\infty} \mathcal{T}_{P_s}(v(t) + 1/R) \neq \lim_{R \rightarrow +\infty} \mathcal{T}_{P_s}(v(t) - 1/R),$$

however, as  $v(t)$  is imaginary,

$$v(t) - 1/R = -\overline{v(t) + 1/R} \text{ and } \mathcal{T}_{P_s}(v(t) - 1/R) = \overline{\mathcal{T}_{P_s}(v(t) + 1/R)},$$

so that

$$\int_{\Upsilon^+} \Xi(q) dq - \int_{\Upsilon^-} \Xi(q) dq = - \int_{t_h}^{t_0} 2v(t) \Im m(\mathcal{T}_{P_s}(v(t))) \frac{dv(t)}{dt} e^{-st} dt. \quad (21)$$

**Remark 3.2.** Following the definition of the square root of a negative number, we made the abuse of notation

$$\lim_{R \rightarrow +\infty} \mathcal{T}_{P_s}(v(t) + 1/R) = \mathcal{T}_{P_s}(v(t)).$$

Since  $v_{P_s}^-(t)$  and  $\frac{dv_{P_s}^-(t)}{dt}$  are purely imaginary, (21) can be rewritten under the form

$$\int_{\Upsilon^+} \Xi(q) dq - \int_{\Upsilon^-} \Xi(q) dq = \int_{t_h}^{t_0} 2\Re e \left( i v(t) \mathcal{T}_{P_s}(v(t)) \frac{dv(t)}{dt} \right) e^{-st} dt.$$

Finally we have

$$\begin{aligned} \tilde{u}_{s, P_s}^-(x, y, s) &= - \int_{t_h}^{t_0} \frac{\mathcal{P}_{12}}{s\pi} \Re e \left( i v(t) \mathcal{T}_{P_s}(v(t)) \frac{dv(t)}{dt} \right) e^{-st} dt \\ &\quad - \int_{t_0}^{+\infty} \frac{\mathcal{P}_{12}}{s\pi} \Re e \left( i \gamma(t) \mathcal{T}_{P_s}(\gamma(t)) \frac{d\gamma(t)}{dt} \right) e^{-st} dt \\ &= \int_{t_h}^{+\infty} \left[ \int_0^t \nu_{P_s, x}^-(x, y, \tau) d\tau \right] e^{-st} dt \end{aligned}$$

and we conclude by using the injectivity of the Laplace transform that

$$u_{sx,Ps}^-(x, y, t) = \int_0^t \nu_{Ps,x}^-(x, y, \tau) d\tau.$$

## 4 Numerical illustration

To illustrate the use our results, we have compared our analytical solution to a numerical one obtained by C. Morency and J. Tromp [13]. We consider an acoustic layer with a density  $\rho^+ = 1020 \text{ kg/m}^3$  and a celerity  $V^+ = 1500 \text{ m/s}$  on top of a poroelastic layer whose characteristic coefficients are:

- the solid density  $\rho_s^- = 2500 \text{ kg/m}^3$ ;
- the fluid density  $\rho_f^- = 1020 \text{ kg/m}^3$ ;
- the porosity  $\phi^- = 0.4$ ;
- the tortuosity  $a^- = 2$ ;
- the solid bulk modulus  $K_s^- = 16.0554 \text{ GPa}$ ;
- the fluid bulk modulus  $K_f^- = 2.295 \text{ GPa}$ ;
- the frame bulk modulus  $K_b^- = 10 \text{ GPa}$ ;
- the frame shear modulus  $\mu^- = 9.63342 \text{ GPa}$ ;

so that the celerity of the waves in the poroelastic medium are:

- for the fast P wave,  $V_{Pf}^- = 3677 \text{ m/s}$
- for the slow P wave,  $V_{Ps}^- = 1060 \text{ m/s}$
- for the  $\psi$  wave,  $V_{\psi}^- = 2378 \text{ m/s}$ .

The source is located in the acoustic layer, at 500 m from the interface. It is a point source in space and a fifth derivative of a Gaussian of dominant frequency  $f_0 = 15 \text{ Hz}$ :

$$f(t) = 4.10^{10} \frac{\pi^2}{f_0^2} \left[ 9 \left( t - \frac{1}{f_0} \right) + 4 \frac{\pi^2}{f_0^2} \left( t - \frac{1}{f_0} \right)^3 - 4 \frac{\pi^4}{f_0^4} \left( t - \frac{1}{f_0} \right)^5 \right] e^{-\frac{\pi^2}{f_0^2} \left( t - \frac{1}{f_0} \right)^2}.$$

We compute the solution at two receivers, the first one is in the acoustic layer, at 533 m from the interface; the second one is in the poroelastic layer, at 533 m from the interface; both are located on a vertical line at 400 m from the source (see Fig. 5). We represent the  $y$  component of the displacement from  $t = 0$  to  $t = 1 \text{ s}$ . on Fig 6. The left picture represents the solution at receiver 1 while the right picture represents the solution at receiver 2. On both pictures the blue solid curve is the analytical solution and the red dashed curve is the numerical solution.

Both pictures show a good agreement between the two solutions, which validates the numerical code.



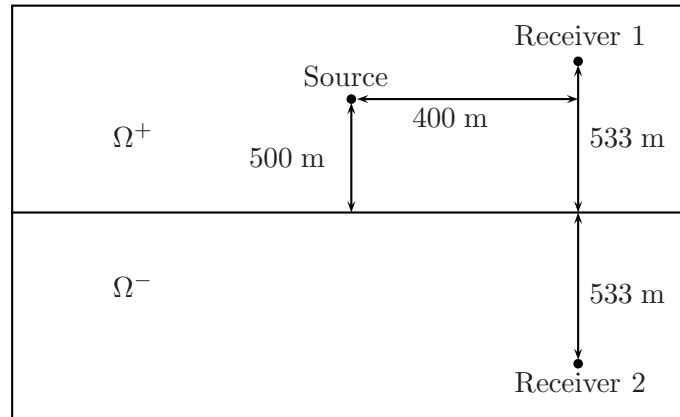
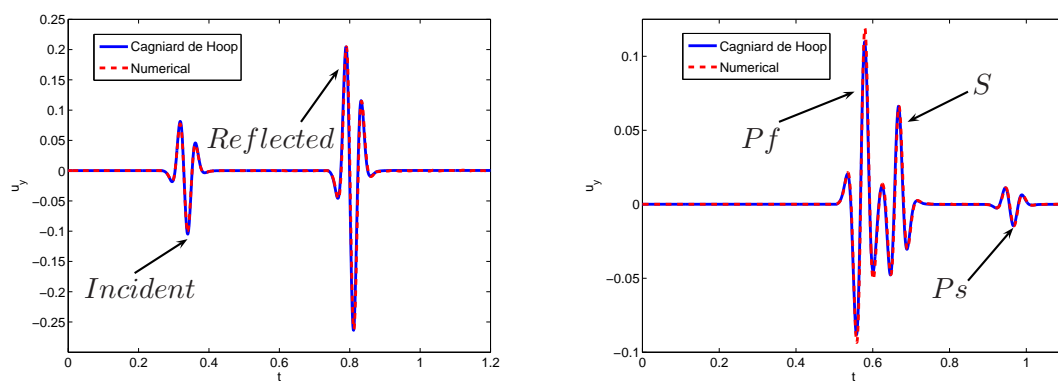


Figure 5: Configuration of the experiment

Figure 6: The  $y$  component of the displacement at receiver 1 (left picture) and 2 (right picture). The blue solid curve is the analytical solution computed by the Cagniard-de Hoop method, the red dashed curve is the numerical solution.

## 5 Conclusion

We provided the complete solution (reflected and transmitted wave) of the propagation of wave in a stratified 2D medium composed of an acoustic and a poroelastic layer and we used it to validate a numerical code. In a forthcoming paper we will use this solution as a basis to derive the solution in a three dimensional medium. We will also extend the method to the propagation of waves in heterogeneous poroelastic medium in two and three dimensions.

## Acknowledgments

We thanks Christina Morency who provided us the numerical solutions we have used to validate our analytical solution.

## A Properties of the function $\mathcal{F}(q, t)$

We recall in this section some properties of the function (see [4, 15, 7]):

$$\mathcal{F} := \mathcal{F}(q, t) = -y \left( \frac{1}{V_{Ps}^{-2}} + q^2 \right)^{1/2} + h \left( \frac{1}{V^{+2}} + q^2 \right)^{1/2} + iqx - t,$$

**Property A.1.** For each  $t \in \mathbb{R}^+$ ,  $\mathcal{F}(\cdot, t)$  admits at most two roots.

**Property A.2.** There is one and only one  $t_0 \in \mathbb{R}^+$  such that  $\mathcal{F}(\cdot, t_0)$  admits a double root  $q_0$ . This root is purely imaginary and  $t_0$  corresponds to the physical arrival time of the wave. Moreover  $\Im m(q_0) \leq 0$  if  $x \geq 0$  and  $\Im m(q_0) > 0$  if  $x < 0$ .

**Property A.3.** For  $t > t_0$ ,  $\mathcal{F}(\cdot, t)$  admits exactly two roots, which have the same imaginary part, positive if  $x < 0$  and negative else, and an opposite non-zero real part.

**Property A.4.** If  $|\gamma(t_0)| \leq 1/V_{\max}$ , there exists a time  $t_h \leq t_0$ , such that for  $t_h \leq t \leq t_0$ , the function  $\mathcal{F}(\cdot, t)$  admits exactly two imaginary roots  $q_1(t)$  and  $q_2(t)$ . The time  $t_h$  is such that

$$\gamma(t_h) = \begin{cases} \frac{i}{V_{\max}}, & \text{if } x < 0 \\ -\frac{i}{V_{\max}}, & \text{if } x \geq 0 \end{cases}$$

and corresponds to the physical arrival time of the head wave. It can be computed by using the relation  $\mathcal{F}(i/V_{\max}, t_h) = 0$  (if  $x < 0$ ) or  $\mathcal{F}(-i/V_{\max}, t_h) = 0$  (if  $x \geq 0$ ):

$$t_h = -y \sqrt{\frac{1}{V_{Ps}^{-2}} - \frac{1}{V_{\max}^2}} + h \sqrt{\frac{1}{V^{+2}} - \frac{1}{V_{\max}^2}} + \frac{|x|}{V_{\max}}.$$

**Property A.5.** The roots  $q_1(t)$  and  $q_2(t)$  satisfy

$$\Im m(q_1(t)) \in [1/V_{\max}, \Im m(\gamma(t_0))] \text{ and } \Im m(\partial_t q_1(t)) > 0$$

$$\Im m(q_2(t)) \in [\Im m(\gamma(t_0)), -1/V_{\max}] \text{ and } \Im m(\partial_t q_2(t)) < 0$$

## B Definition of the arrival time of the transmitted waves.

We detail in this section the computation of the arrival time of the transmitted  $Ps$  wave at point  $(x, y)$ . We first have to determine the fastest path from the source to the point  $(x, y)$ : we search a point  $\xi_0$  on the interface between the two media which minimizes the function

$$t(\xi) = \frac{\sqrt{\xi^2 + h^2}}{V^+} + \frac{\sqrt{(x - \xi)^2 + y^2}}{V_{Ps}^-}$$

(see Fig. 7). This leads us to find  $\xi_0$  such that

$$t'(\xi_0) = \frac{\xi_0}{V^+ \sqrt{\xi_0^2 + h^2}} + \frac{\xi_0 - x}{V_{Ps}^- \sqrt{(x - \xi_0)^2 + y^2}} = 0. \quad (22)$$

From a numerical point of view, the solution to this equation is done by computing the roots of the following fourth degree polynomial

$$\left( \frac{1}{V^{+2}} - \frac{1}{V_{Ps}^{-2}} \right) X^4 + 2x \left( \frac{1}{V_{Ps}^{-2}} - \frac{1}{V^{+2}} \right) X^3 + \left( \frac{x^2 + y^2}{V^{+2}} - \frac{x^2 + h^2}{V_{Ps}^{-2}} \right) X^2 + \frac{xh^2}{V_{Ps}^{-2}} X + \frac{x^2 h^2}{V_{Ps}^{-2}},$$

$\xi_0$  is thus the only real root of this polynomial located between 0 and  $x$  which is also solution to (22). Once  $\xi_0$  is computed, we can define

$$t_0 = \frac{\sqrt{\xi_0^2 + h^2}}{V^+} + \frac{\sqrt{(x - \xi_0)^2 + y^2}}{V_{Ps}^-}$$

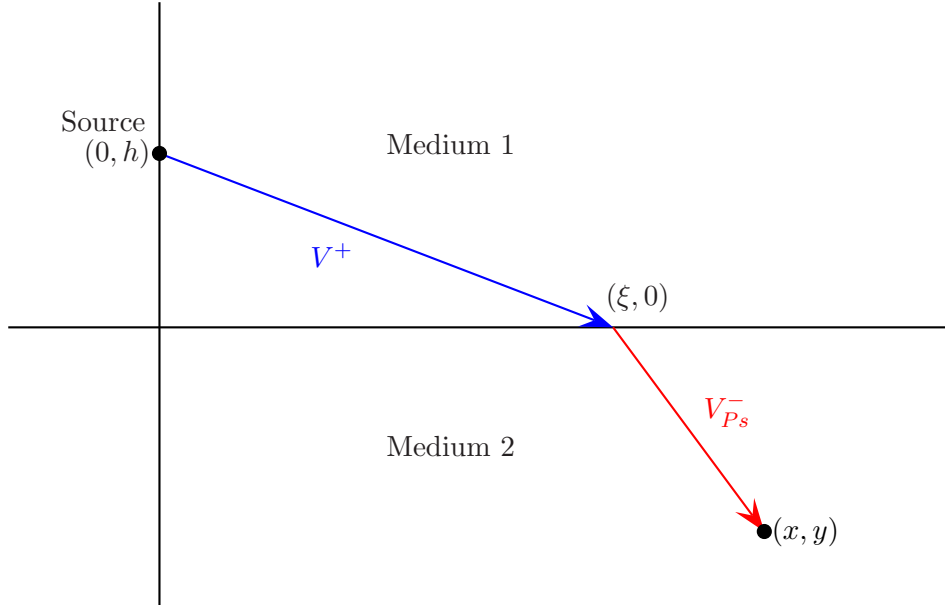


Figure 7: Path of the transmitted  $i$  wave

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## Contents

<b>1</b>	<b>The model problem</b>	<b>3</b>
1.1	The equation of acoustics . . . . .	4
1.2	Biot's Model . . . . .	5
1.3	Transmission conditions . . . . .	6
1.4	The Green problem . . . . .	6
<b>2</b>	<b>Expression of the analytical solution</b>	<b>8</b>
<b>3</b>	<b>Proof of the theorem</b>	<b>14</b>
3.1	The solution in the Laplace-Fourier plane . . . . .	14
3.2	The Laplace transform of the solution . . . . .	16
<b>4</b>	<b>Numerical illustration</b>	<b>21</b>
<b>5</b>	<b>Conclusion</b>	<b>23</b>
<b>A</b>	<b>Properties of the function <math>\mathcal{F}(q, t)</math></b>	<b>23</b>
<b>B</b>	<b>Definition of the arrival time of the transmitted waves.</b>	<b>24</b>



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